

Solving Complex Feeder Protection Challenges and Reducing Wildfire Risks With Remote Measurements

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Distribution feeders become more complex





- Complex topology, multiple sections and branches
- Looped circuits, reclosers, and bidirectional short-circuit current flow
- Increasing load (EVs, heating)
- Distributed energy resources (DERs)
- Microgrid protection issues, islanded operation concerns

Powerline-caused wildfires become concerns

- Long fault clearing time and high energy released at the fault point
- Tree contacts last for a long time before high current follows
- "HiZ" and downed-conductor protection methods are too slow
- Low protection sensitivity for
 - High-impedance faults
 - Downed conductors



Powerline-caused wildfires

Mitigation is expensive

- Rigorous right-of-way vegetation management (mineral soil, gravel)
- Undergrounding overhead feeders
- Insulated overhead conductors
- Converting distribution networks to compensated ungrounded networks
- Experimental protection technologies



TOC protection becomes inadequate

- Historically, TOC feeder protection was
 - Technically adequate
 - Economically cost-efficient
- Today's feeders resemble scaled-down portions of a transmission system
- The industry desperately tries to "make the TOC protection work"
- We do have transmission-grade methods to protect complex feeders



Transmission-grade feeder protection Obstacles

- A "microsubstation on a pole"
 - Devices to measure and communicate
 - Low-latency dependable communications
 - Control power to run the devices
 - Housing to host the equipment
 - Crew access for maintenance
 - Physical and cybersecurity
- A solution exists but is dismissed because of cost and complexity



Powerline-caused wildfire mitigation

Feeder maintenance

- Managing vegetation to high standards
- Installing spacers to eliminate midspan phase faults
- Fault energy reduction
 - Tripping instantaneously for all fault locations
 - Tripping before a downed conductor hits the ground
 - Tripping instantaneously for tree-contact faults
- Multizone feeder differential protection can deliver the required protection speed and sensitivity



Multizone feeder differential protection

- Protection zones in general
 - Protection tripping zone defined by current interrupting devices
 - Fault detection zone defined by current measurement points
 - Ideally, the two zones overlap to maximize return on investment
- Feeder applications
 - Large protection tripping zones (necessity)
 - Small fault detection zones (objective)



Currents measured throughout the feeder

- Dramatically improve primary protection
 - Multizone differential protection
 - Sensitivity and speed for tree-contact faults
 - Speed for midspan phase faults
 - Downed-conductor detection
 - Dependable operation despite DERs
- Improve feeder, load, and DER backup protection
- Allow impedance-based fault locating
- Improve selectivity of autoreclosing
- Simplify settings
- Enable microgrid applications



Enabling technologies Distributed Electrical Sensing (DES)

- Remote CTs/VTs interrogated via fiber
- Passive No active electronics or control power outside the fence
- Weatherproof No housing required
- Distributed Many CTs/VTs share the same fiber
- Coherent No need for time synchronization
- Concentrated All current and voltage signals available in the substation





Enabling technologies

All-dielectric self-supporting fiber cables

- Relatively inexpensive
- Easy to install
- Some utilities already use ADSS on lower-voltage circuits
- Used in third-party networks on utility poles
- Allows Ethernet network to reach reclosers, DERs, and remote substations



Simplified system architecture

- ADSS fiber daisy-chains CTs
- Interrogator located in the substation provides the measurements
- Relays provide protection and other functions
- Tripping of reclosers and remote breaker via ADSSbased Ethernet feeder LAN



Distributed Electrical Sensing

Multiplexed passive sensing of current or voltage

- Passive sensing allows remote measurements outside the substation fence
 - Use conventional CTs
 - Up to 30 single-phase measurements per fiber, up to 60 km (37 mi)
 - Measurements are inherently synchronized no time source needed
 - No electronics or control power required
- Electronics and digitization of measurements are kept within substation
 - No cyber assets outside the substation fence
 - All sensors sampled synchronously, centrally

Passive Converter and CT



ADSS



Fiber Bragg grating principle and application

- A source shines a widespectrum light
- Reflected light encodes periodicity (notch spacing)
- Measured quantity affects periodicity (stretching or contracting)
- Reflected light encodes measured quantity



Optical measurement and multiplexing

- Wavelength also permits serial multiplexing each sensor is placed at a unique nominal wavelength
- Sensors are interrogated from a suitable central measurement point

Passively Reflected Light Encodes Measurements



All Sensors Illuminated Simultaneously

Electrical measurement technique

- CT and precision resistor are used to convert primary current to voltage
- Piezoelectric device converts voltage to strain, measurable by FBG
- Expansion or compression of the FBG causes a detectable shift in the reflected wavelength



And optional mechanical measurements

- CT and precision resistor are used to convert primary current to voltage
- Piezoelectric device converts voltage to strain, measurable by FBG
- Expansion or compression of the FBG causes a detectable shift in the reflected wavelength

OR remove piezo to directly measure strain, vibration, temperature





Measurement processing

$$V_{2} = xV_{1}$$

$$\lambda(nm) = A_{0} + A_{1}pix + A_{2}pix^{2} \dots + A_{5}pix^{5}$$

$$Peak pixel number$$

$$Peak wavelength$$

$$Electrical measurand$$

$$Electrical measurand$$

$$I = B_{0} + B_{1}\lambda_{inst}\lambda_{pp} + B_{2}\lambda_{inst}\lambda_{pp}^{2} + B_{3}\lambda_{inst}^{2}\lambda_{pp} \dots + B_{28}\lambda_{inst}^{6}\lambda_{pp}^{6}$$

- Measurement chain (CT to SV) is 5P class and compliant with IEC 60044-8 / IEC 61869-10
- Synchronization and latency comply with IEC 61850-9-2 / IEC 61869-9

Centralized measurement platform

- Wavelength-based sensing enables simple multiplexing and environmental resilience
- Mechanical and electrical measurements are synchronized on one platform
- Measurement system installation is fast and safe because of minimal wiring and power



- Every sensor is sampled centrally at up to 288 s/c
- Produces synchronized waveforms from each measurement point
- Supports multiple functions from one data source

Enabled topology

- Deploy conventional CTs at multiple remote locations
- Data published centrally, synchronously





Deployment with SSE Transmission, UK

Facilitating new grid connections from renewables in remote locations

- Overcame limitations of distance protection
- Achieved multi-ended differential fre single end
- Enabled wide-area, fully digital, ur protection scheme
- Avoided major civil works and tel upgrades for older remote subst
- Proved IEC 61850 operability with three relay brands
 https://www



Benefits and Conclusions

Protection benefits

- Scalable Differential protection for a single feeder section or many/all sections of a complex feeder
- Ultra-sensitive Protection for tree-contact faults and downed conductors
- Instantaneous Reduced fault energy, protection for galloping conductor faults
- Dependable Breaker failure and recloser failure protection, faster backup protection, not affected by DERs
- Future-ready Anti-islanding protection, microgrid monitoring, easier DER ride through





Passive current sensing + Costeffective ADSS fiber

"See" beyond the substation fence



Radical reframing of how to protect distribution feeders

Transmission-grade protection for complex distribution feeders

Fast, sensitive, granular unit protection

Addresses needs of high-risk wildfire areas