

# American Electric Power's Experience with Protection System Misoperations and Improvements

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75<sup>th</sup> Annual Conference for Protective Relay Engineers

Texas A&M University

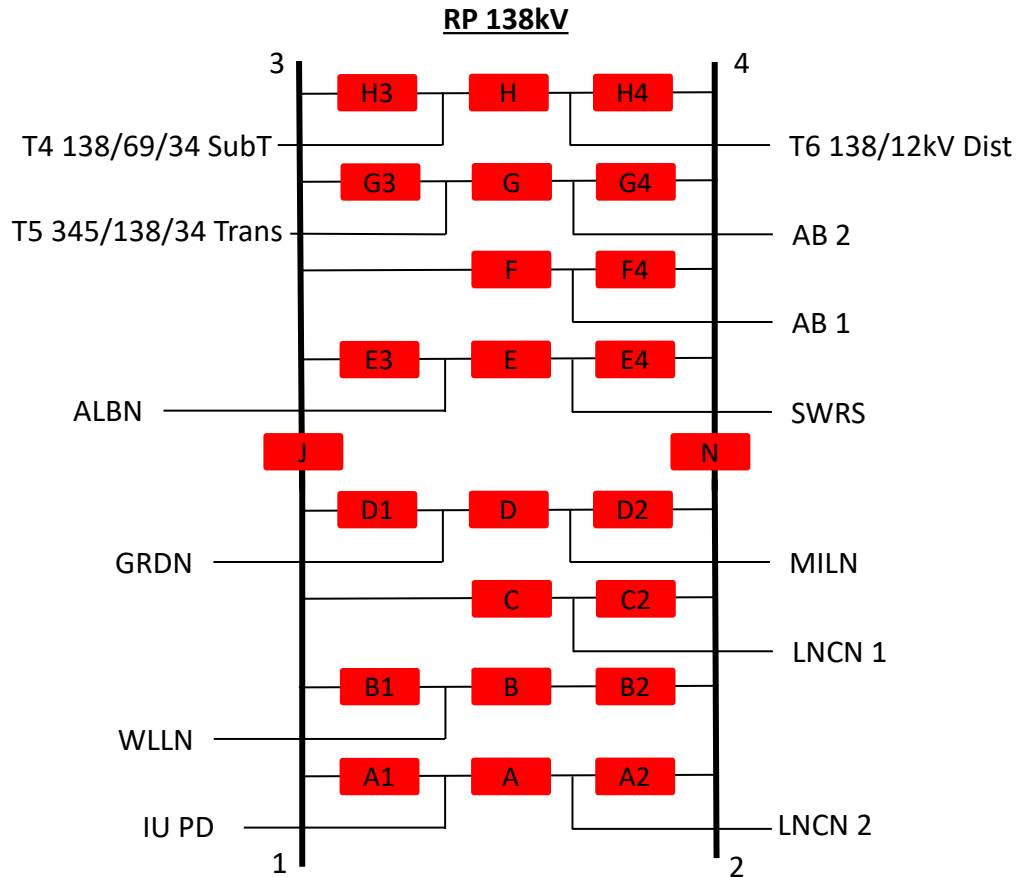
March 28 - March 31, 2022

## AEP Misop Event of 1/26/2022

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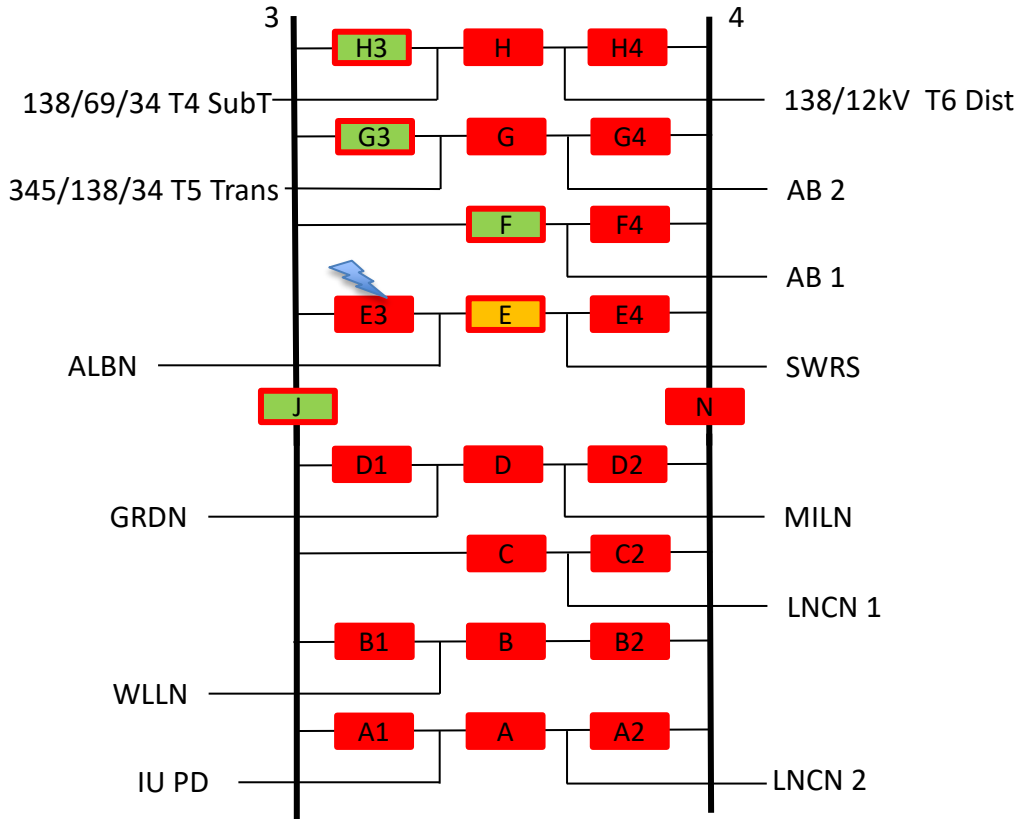
- 138kV CB – E3 Internal Fault
  - Multiple stages to this event, but there was only a single permanent fault. CG fault inside CB-E3.
  - During Stage 2 of the event, 2 – 138kV Circuits and 345/138/34.5 kV T5 lowside lead differential misoperate.

# Pre-fault Configuration



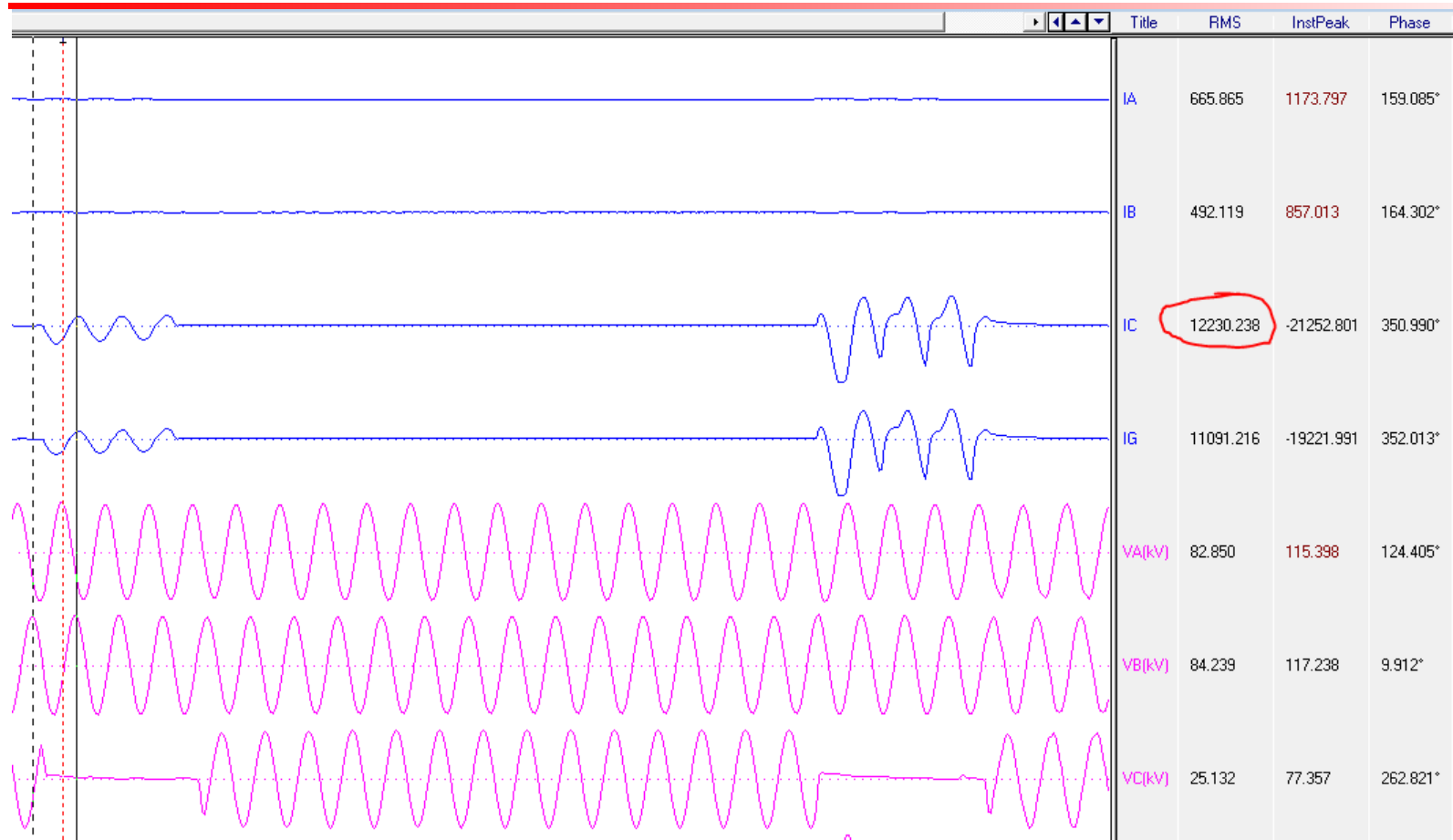
- 138kV RP Station
- System Normal
- CB-E3 is the fault location
- 5 – 345kV circuits on highside of T5
- 10 – 138kV circuits
- 4 – 138kV Bus zones
- Transformers
  - Trans = Transmission Auto
  - Dist = Distribution 2-Winding
  - SubT = Sub-Transmission Auto

# Fault Stage 1 – Initial Operation

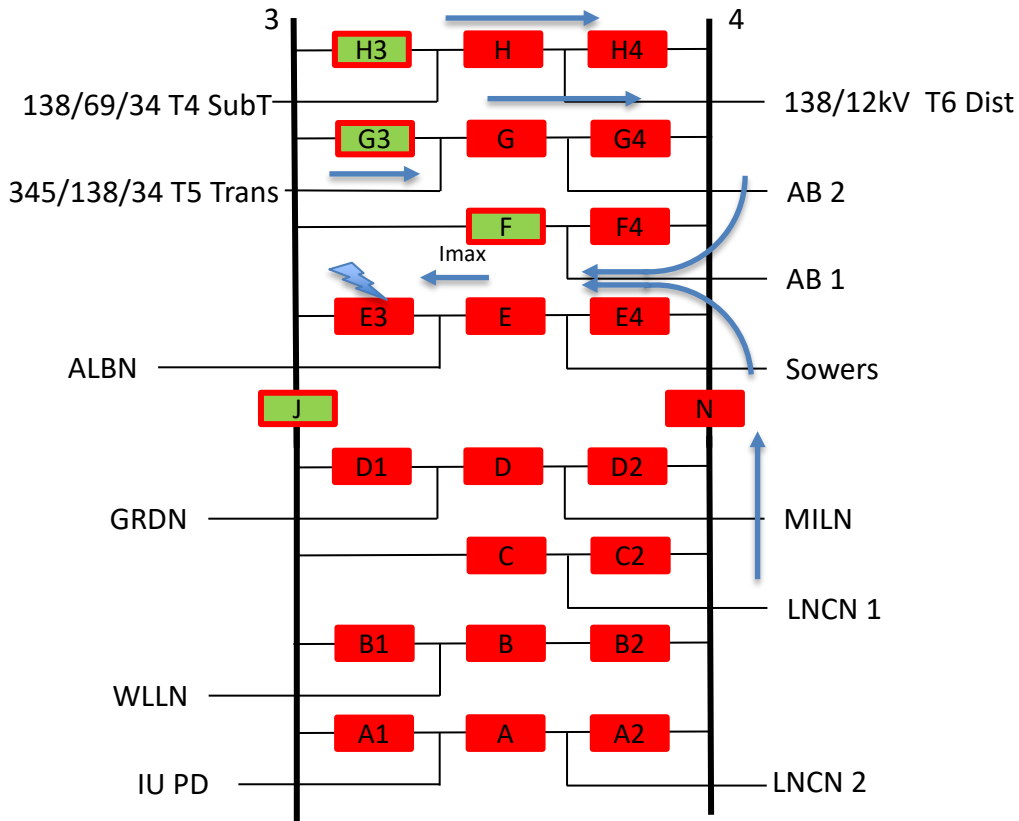


- Internal CB-E3 fault
  - Fault is located between ALBN Line zone and 138kV Bus #3.
  - Both zones operate correctly, with CB's H3, G3, F, and J tripping and locking out from the 87 Bus protection.
  - CB-E trips from line protection zone 1 and is set to reclose highspeed ~18 cycles after initial trip.
  - CB-E sees ~12 kA fault current

# Fault Stage 1 – Initial Operation CB-E (SEL-351S 79/551E)

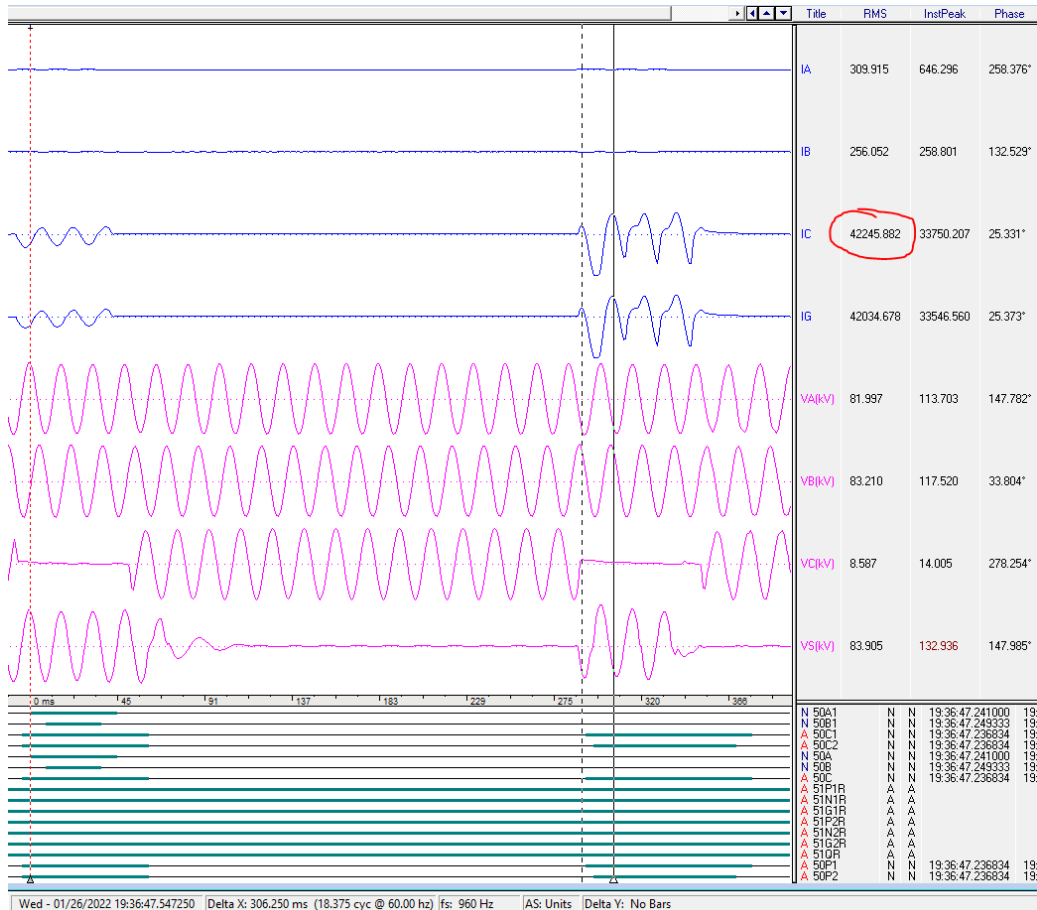


# Fault Stage 2- CB-E Reclose



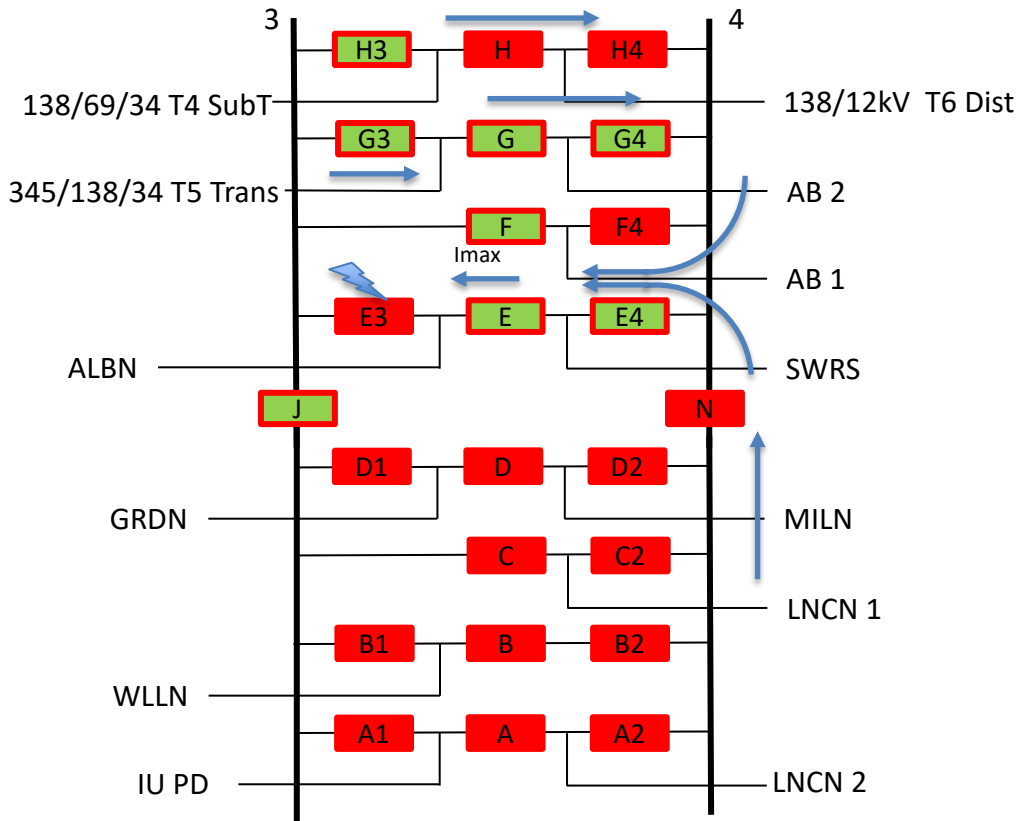
- CG fault is permanent
  - CB-E recloses back into the permanent fault.
  - $I_{max} = 42$  kA with a large contribution from T5
- Notice the new path of fault current due to 138kV Bus #3 being locked out.

# Fault Stage 2 – CB-E Reclose (SEL-351S 79/551E)



- ~18cyc between cursors verifying CB-E HS reclose time.
- IC RMS magnitude much larger then Stage 1.

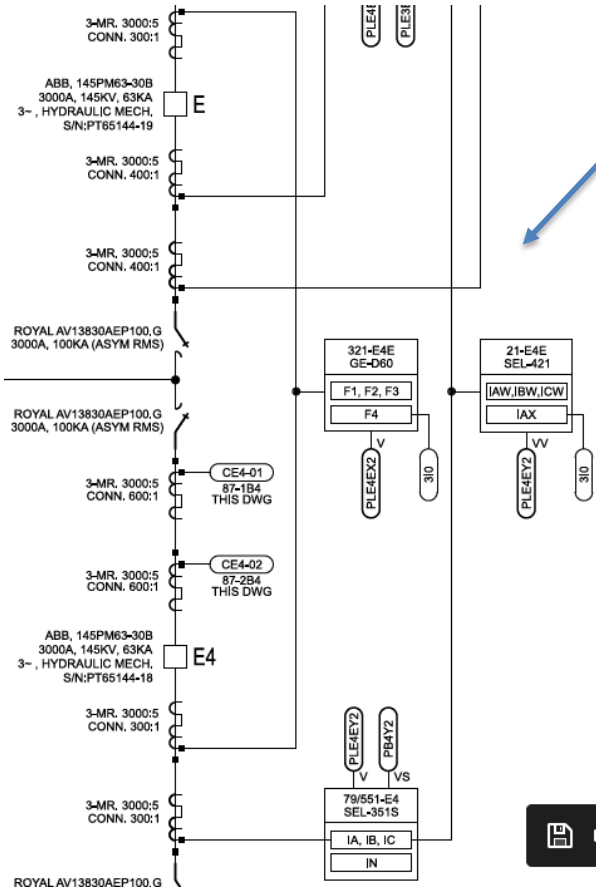
# Fault Stage 2- CB-E Reclose & Misoperation



- CG fault is permanent (same phase as slide 6).
  - CB-E recloses back into the permanent fault.
  - $I_{max} = 42$  kA with a large contribution from T5
- CB's E, E4, G, and G4 misoperate operate for a close-in 1LG fault.
- T5 trips and locks out due to lowside lead differential L90 misoperation.

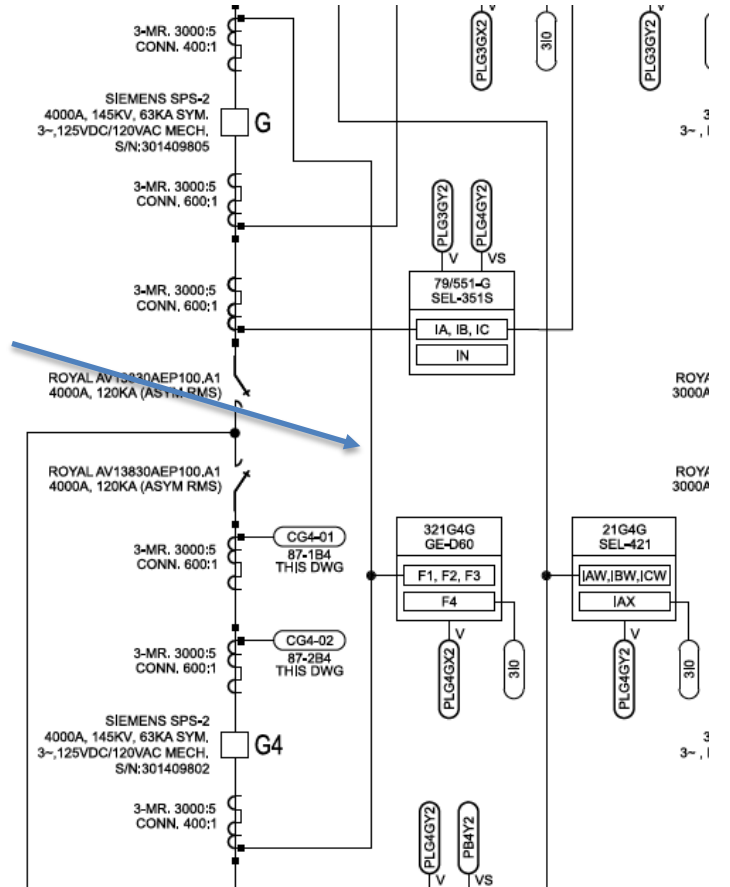


# Misoperated 138kV Line Protection

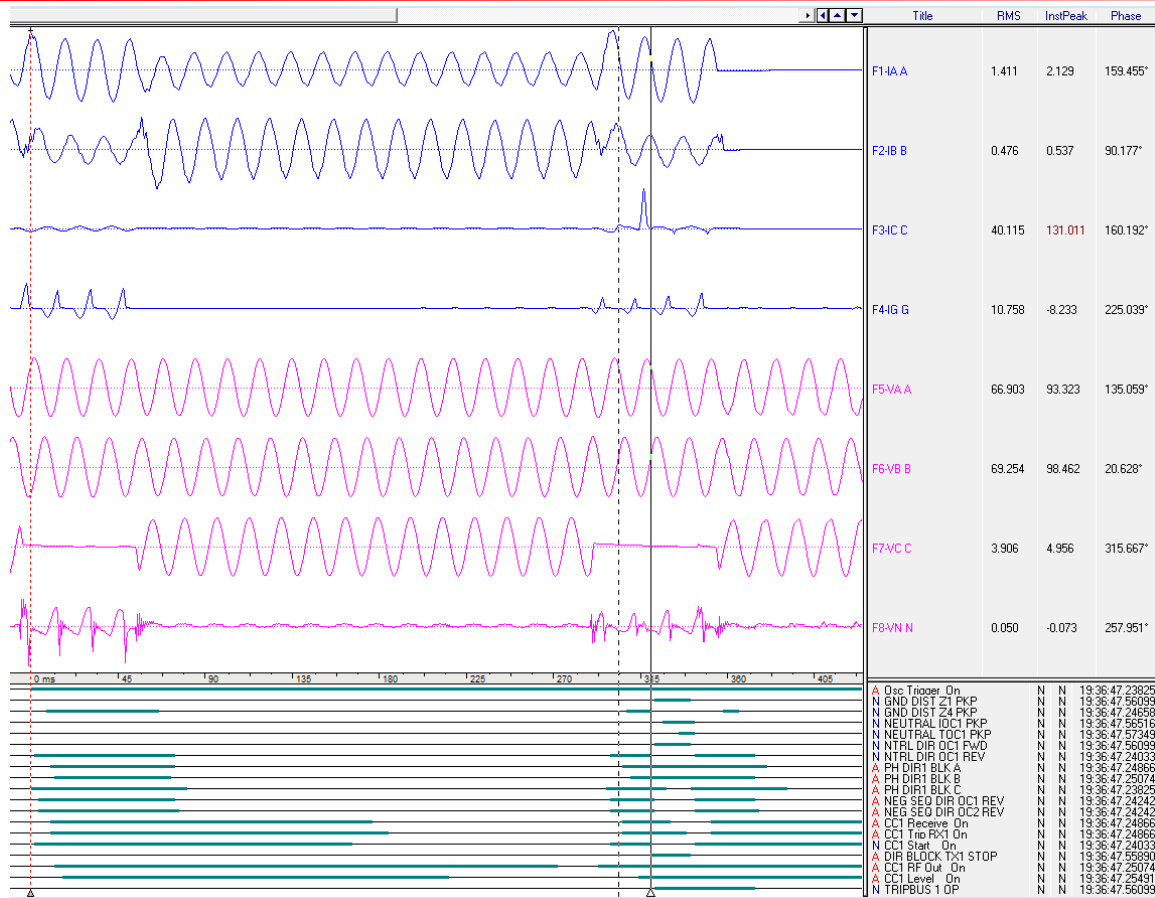


SWRS Line  
321-E4E DCB  
21-E4E SD

AB 2 Line  
321-E4E DCB  
21-E4E SD

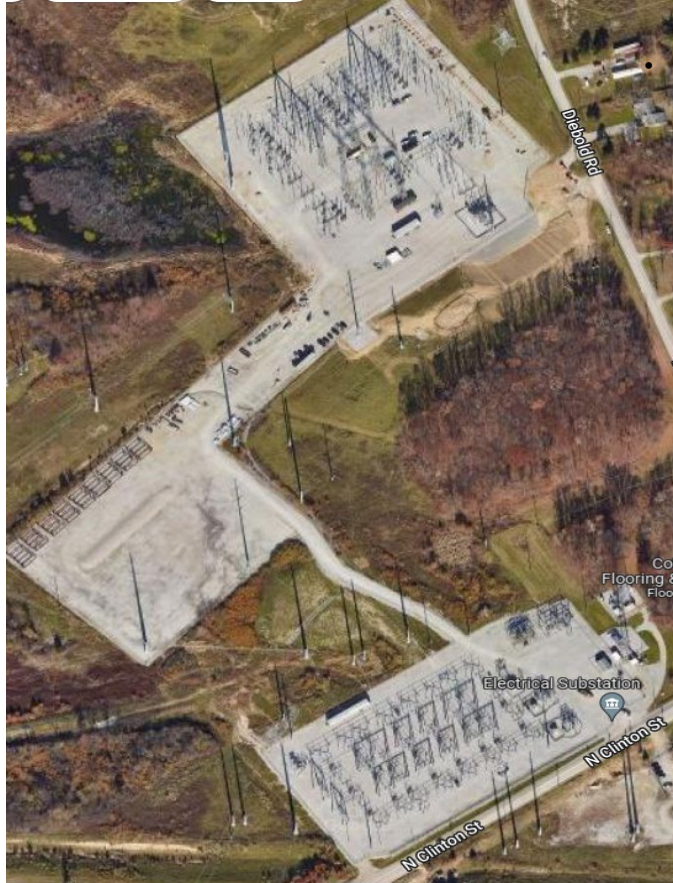


# Misoperated 138kV Line Protection (GE-D60 321-E4E)

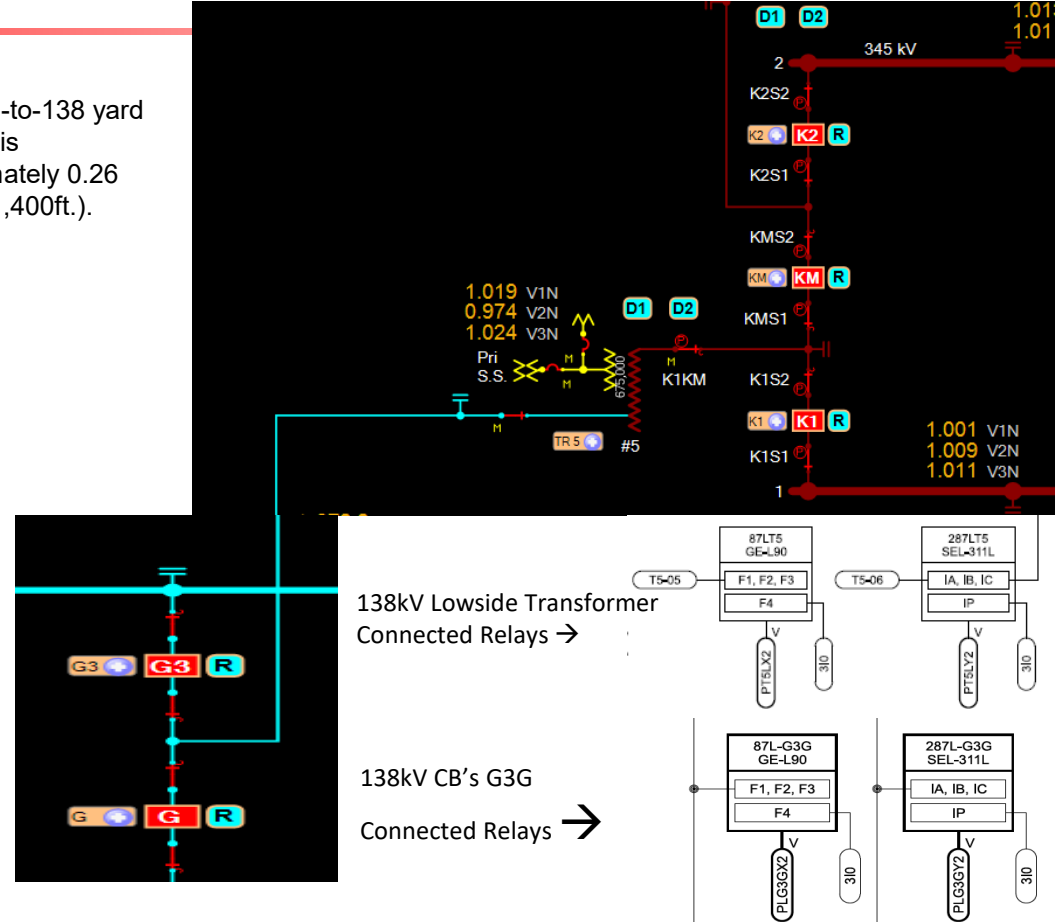


- $40 * 300 = 12\text{kA}$

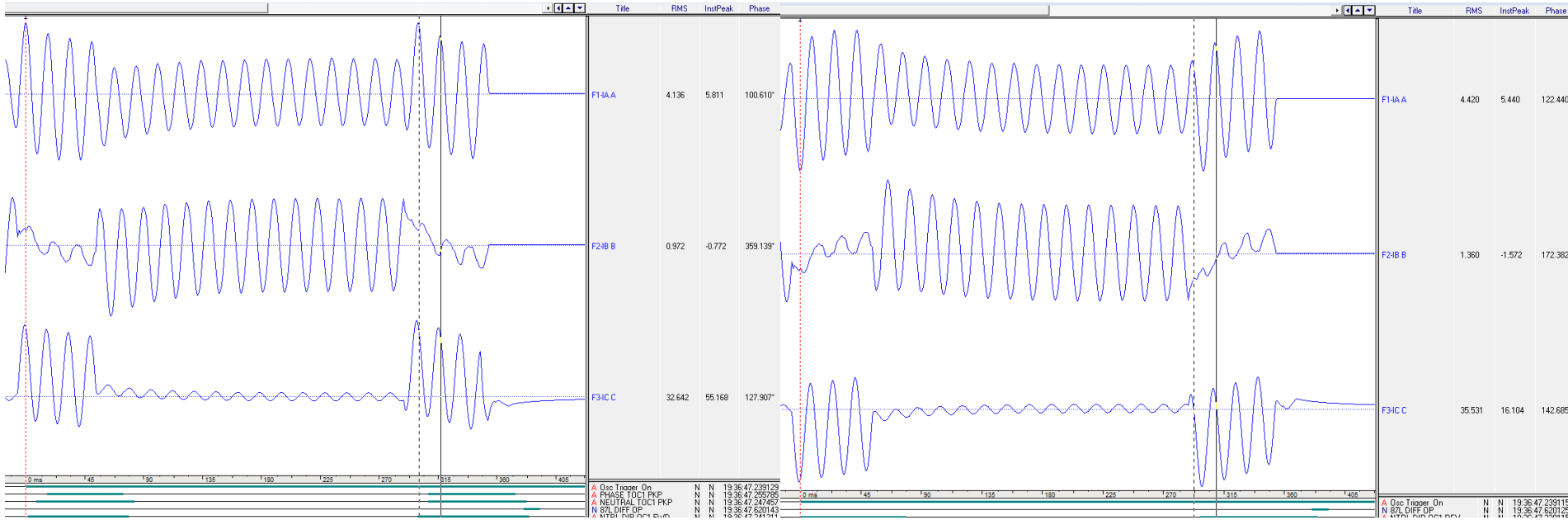
# RP T5 Layout



345 Yard-to-138 yard distance is approximately 0.26 miles (~1,400ft.).



# RP T5 Lowside Lead Differential



L90 – 87T5 (Lowside T5 CT)

L90 – 87L-G3G (138kV Yard BCTs)

# Corrective Action Plans

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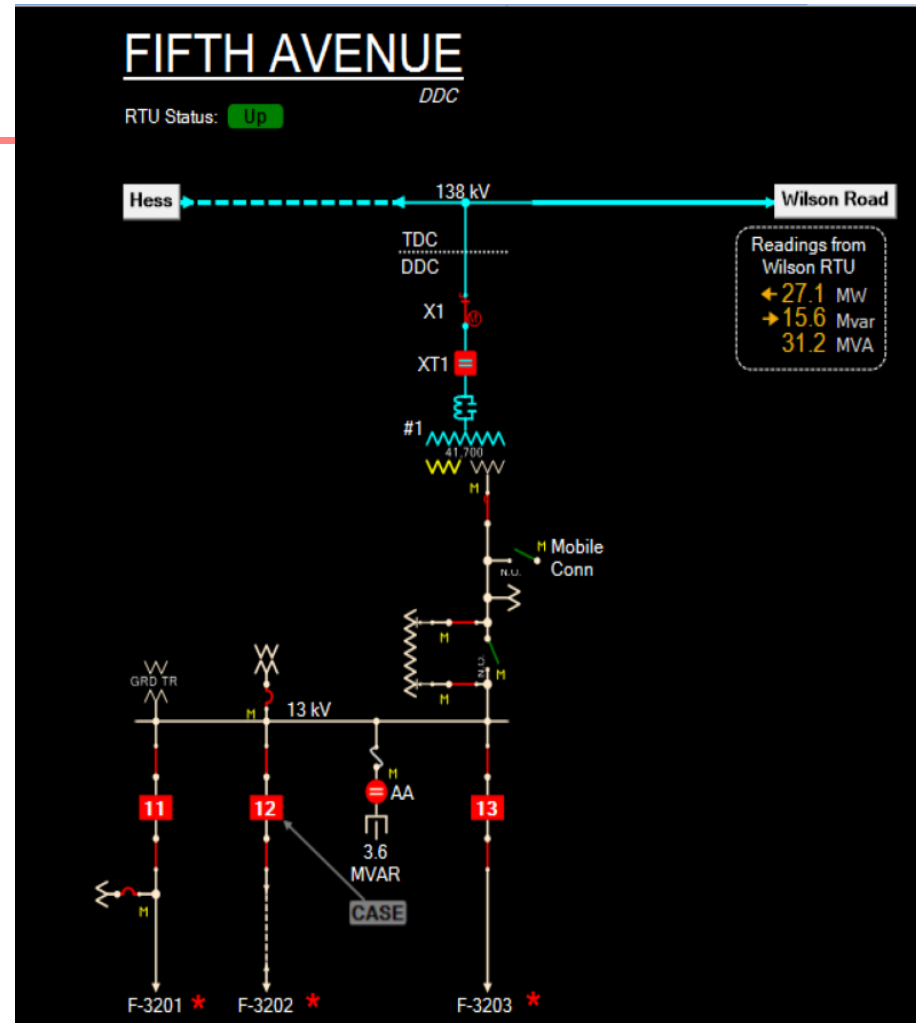
- **138kV line Misoperations**
  - CB-E high speed reclosing will be evaluated with AEP Operations group and the CT connected ratio will be evaluated and connected at the highest ratio possible to help minimize any future CT saturation.
- **345/138/34.5kV T5 lowside lead differential Misoperation**
  - L90 relay settings will be evaluated (break point, differential slopes, and differential pickup) to better handle any future CT saturation that may occur. The connected CTs are already at full tap (600/1) so the CT ratios cannot be raised any higher.

# Minimize risk of CT Saturation

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- Use highest CTR (accounting for sensitivity) for line protection.
- Use separate current inputs into the relays to monitor breaker currents as opposed to external summation if possible.
- Substations are unique (X/R, CT cable lengths etc.) however using high CTR connections at high fault current stations is best practice to avoid high thru-current CT saturation.
- Fault currents have increased at this station ~30% over the past 7 years and one of these lines had not been re-evaluated since 2015 when it was originally chosen at 400/1 instead of the max 600/1 CT ratio

# AEP Fifth Avenue Mobile Misop



# Background

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- TFS needed to do XF maintenance, so a mobile unit was required
- Not your typical distribution XF (it is a wye-grounded high side / delta low side)
- Since delta low side, a grounding XF is required
- To keep things in phase with the existing XF, mobile CSP-9 was selected since it is an auto XF with the same vectors
- Mobile CSP-9 is very modern and is outfitted with all new IED relays



# What Happened?

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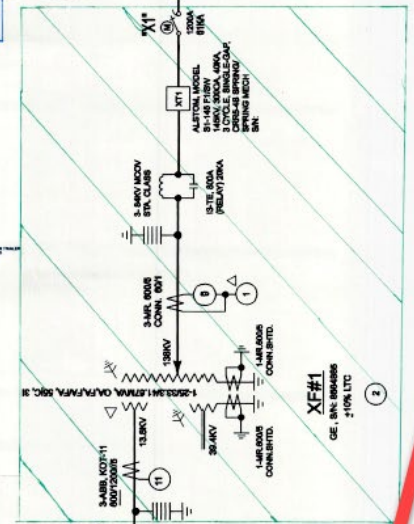
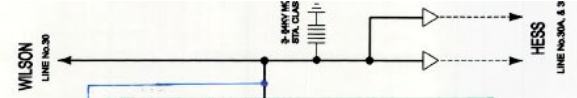
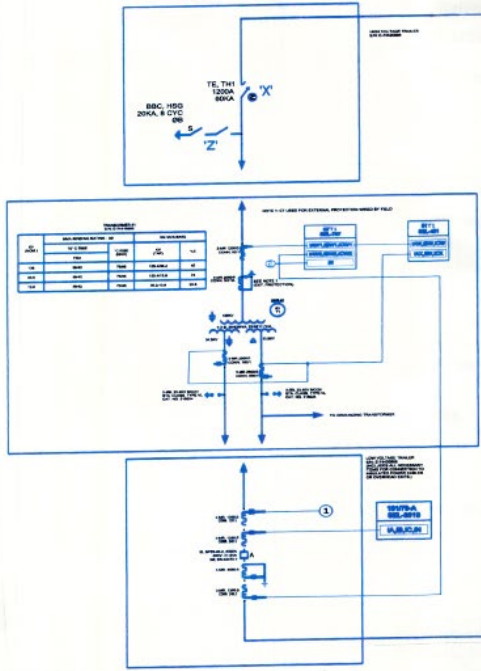
- Mobile had been commissioned and was in service for a few days, but then tripped out via its SEL-787 XF diff for a 1LG feeder fault (out of zone fault)
- During commissioning, no differential current was present on the SEL-787 while doing final load checks

## Result of the Trip

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- The two non-faulted feeder circuits were tripped and locked out along with the feeder that actually had the fault on it
- Since mobile CSP-9 didn't include a high side interrupting device (only ground switch/MOAB) the remote 138kV terminals were also tripped

# CSP-9

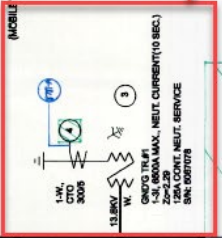


Plan was to re-use the existing GND XF

**XF#1**  
SNL BREAKERS

KV (NOM.)	BRG RISE	FA	FAFA	RSE	ID	MA BASE KV (MVA)	%Z
13.8	25	35.3	41.87	134.3/39.4	6.27		
40	25	35.3	41.87	134.3/39.4	10.02		
13.8	10	13.3	16.67	39.4/13.3	3.95		

\* - AT TAP VOLTAGES SHOWN



F-3001 COLUMBIA GAS

3-COOPER, 11 1200V INT. 1000/228A-100V

3-14KV/14KV 87A CTG

3-14KV/14KV 87A CTG

3-14KV/14KV 87A CTG

3-14KV/14KV 87A CTG

3-14KV/14KV 87A CTG

3-14KV/14KV 87A CTG

3-14KV/14KV 87A CTG

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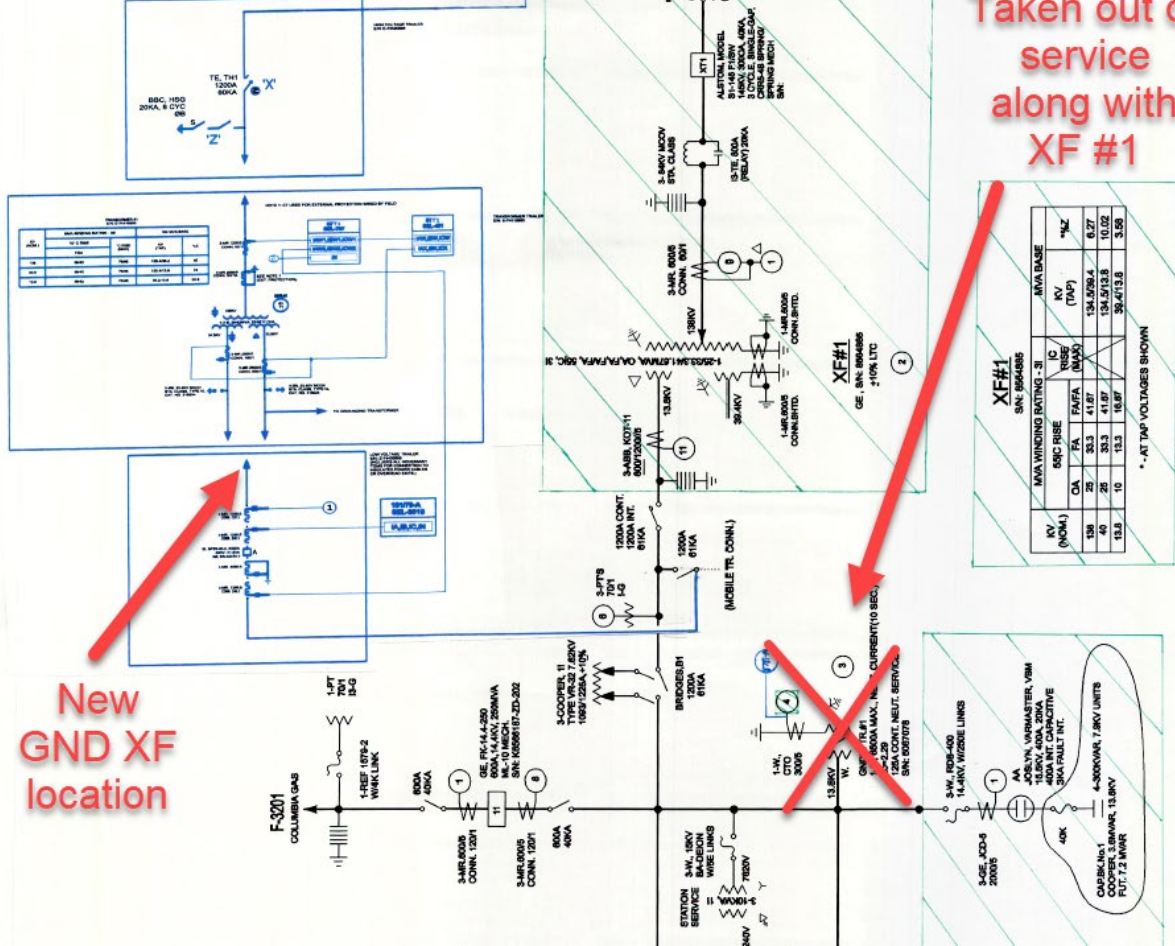
CASBANK 1 COOPER 3.5MWAVE 13.8KV FLT 7.2 MW

# What Happened?

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- During the mobile installation, the plan changed
- Existing GND XF was no longer used (taken out for maintenance along with the main XF) and the GND XF that rides along with CSP-9 was used
- The position of where the GND XF was connected had been modified (bus before, but now between XF and LS CB)

New  
GND XF  
location



Taken out of  
service  
along with  
XF #1



## SEL787 Trip & Fix

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- The SEL-787 XF differential was set based on the original plan with the GND XF outside of the XF differential zone.
- Since the low side winding was delta, the SEL-787 relay doesn't filter out zero sequence current in its low side CT because no zero-sequence current can flow through a delta.
- The fix was very simple:
  - Change the W2CTC setting from 0 to 12.
  - This still maintains the same angle compensation, but the 12 setting also filters out the zero-sequence current.

The WxCTC settings are used to match the phase shifting of the current signals and to remove zero sequence. WxCTC = 0 or 12 provides zero phase shift. If WxCTC = 12 is used then this selection removes the zero sequence. Each increment of WxCTC represents a 30 degree phase shift. For ABC phase rotation each increment in phase shift is in the counter clockwise direction. Reference the SEL787 instruction manual for more details.

# Lessons Learned

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- Whenever a plan changes, all involved groups should reconvene to discuss the effects of the change. A change may seem small to one group but may be a big change to another group.
- Team members should use extra caution and be on alert when working with unique configurations and designs (transformer was not typical delta high side / wye-grounded low side).
- The placement of grounding transformers is very important since they act as a zero-sequence current sources. The protection zone that the grounding transformer is connected within should be examined with extra care to ensure that the grounding transformer is accommodated for properly.

# Quiz

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- Why didn't the XF differential load check test catch these bad XF differential compensation settings during commissioning?



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Questions?