

Novel IBR Control by Emulating Synchronous Generator Fault Response

Dan Kelly, Pratap Mysore, Ned Mohan
University of Minnesota

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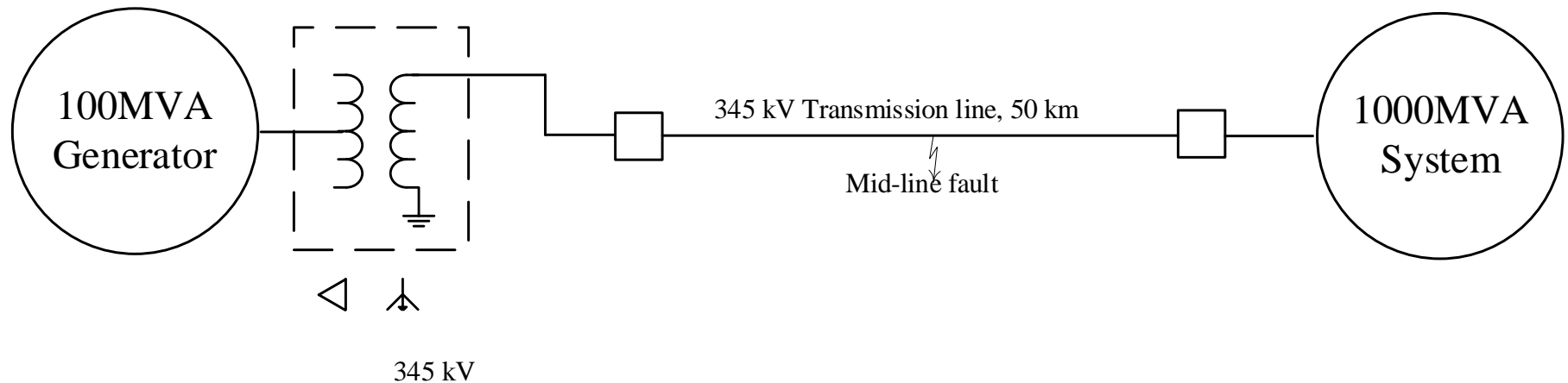
Outline

- Research Problem
- Proposed Solution
- Results
- Questions

Problem Definition

- Inverters are traditionally controlled to always produce balanced currents even during unbalanced faults.
- Distance protection need sequence quantities for proper operation.
- As IBR penetration increases, this may necessitate protective equipment replacement or redesign

Voltages and Currents during Faults – Conventional Generator



System one Line

Voltage and Current relationship

□ Three phase Fault: Pre-Fault Voltage V_A 1.0 PU @ 0°

A-B-C-Gnd

V (PU) :

Line Current

Generator Current

A- Phase

0.03 @ -3°

I @ -87°

IG @ -117°

B-Phase

0.03 @ -123°

I @ 153°

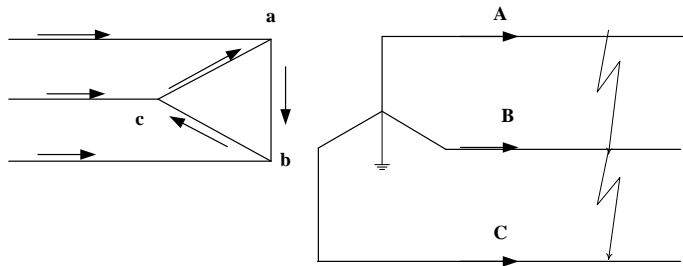
IG @ 123°

C-Phase

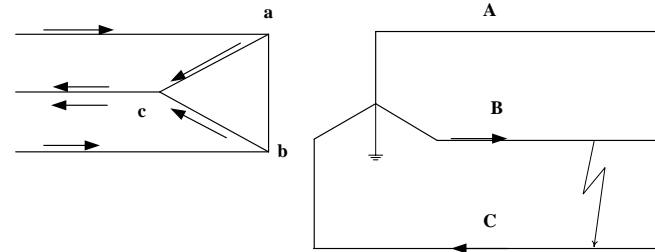
0.03 @ 117°

I @ 33°

IG @ 3°



Three Phase Fault



Phase to Phase Fault

□ Phase –Phase: Pre-Fault Voltage V_A 1.0 PU @ 0°

V (PU) :

Line Current

Generator Current

A- Phase

0.99 @ -0.3°

~ 0 @ 156°

IG_{LL} @ -176.6°

B-Phase

0.50 @ -177.5°

I_{LL} @ -175.6°

IG_{LL} @ -175.1°

C-Phase

0.50 @ 176.8°

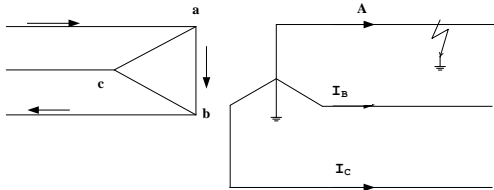
I_{LL} @ 3.9°

2IG_{LL} @ 4.1°

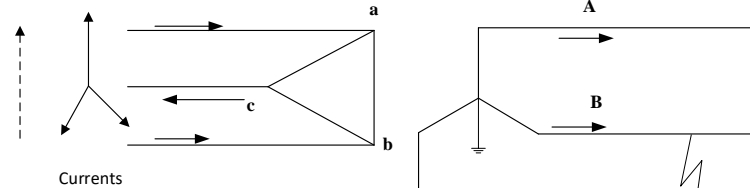
Voltage and Current relationship

Phase to Ground Fault: Pre-Fault: Voltage V_A 1.0 PU @ 0°

A-Gnd Fault	A- Phase	B-Phase	C-Phase
V (PU):	0.08 @ -7.2°	0.96 @ -117.7°	0.97 @ 116.4°
Line Current	$I_{A_{LG}}$ @ -85.3°	$I_{B_{LG}}$ @ -84.9°	$I_{C_{LG}}$ @ -86.9°
Generator Current	$I_{G_{LG}}$ @ -84.8°	$I_{G_{LG}}$ @ 95.0°	0 @ -113.2°



Phase to ground Fault



Two Phase to Ground Fault

Two Phase to Ground Fault: Pre-Fault Voltage V_A 1.0 PU @ 0°

B-C-G Fault	A- Phase	B-Phase	C-Phase
V (PU):	0.93 @ -0.7°	0.07 @ -166.6°	0.07 @ 151.5°
Line Current	$I_{A_{LLG}}$ @ 97.7°	$I_{B_{LLG}}$ @ 142.7°	$I_{C_{LL-G}}$ @ 45.5°
Generator Current	$I_{G_{LL}}$ @ -146.2°	$I_{G_{LL}}$ @ 153.3°	$I_{G_{C_{LL}}}$ @ 3.7°

Proposed Solution

1. Fault identification based on voltage magnitudes at the relay location/ at the inverter transformer terminals.
2. Modify inverter controls to change the magnitude and phase angle of phase currents to emulate sync. gen. response.

Fault Identification (345kV)

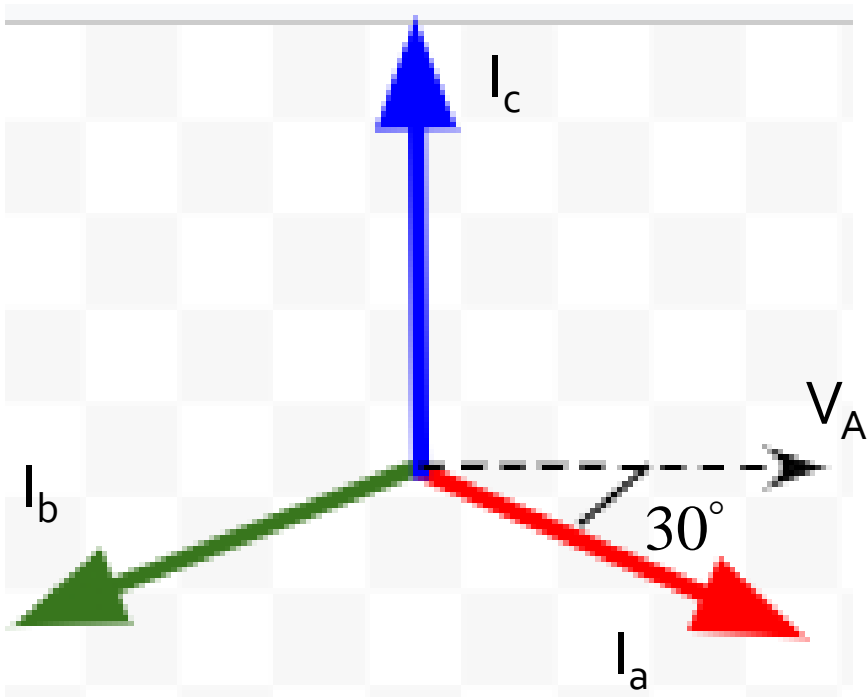
- Single Line to Ground (SLG)
 - Faulted phase to ground voltage below 0.8 pu
 - Healthy phases are above 0.8 pu
- Line to Line (LL)
 - Both faulted phase voltages below 0.8 pu, above 0.4 pu
 - Faulted line to line voltage below 0.8 pu
- Double Line to Ground (LLG)
 - Both phase voltages below 0.4 pu
 - Faulted line to line voltage below 0.8 pu
- Three Phase to Ground Fault
 - All phase voltages below 0.8 pu

Obtaining Reference Currents (A-G)

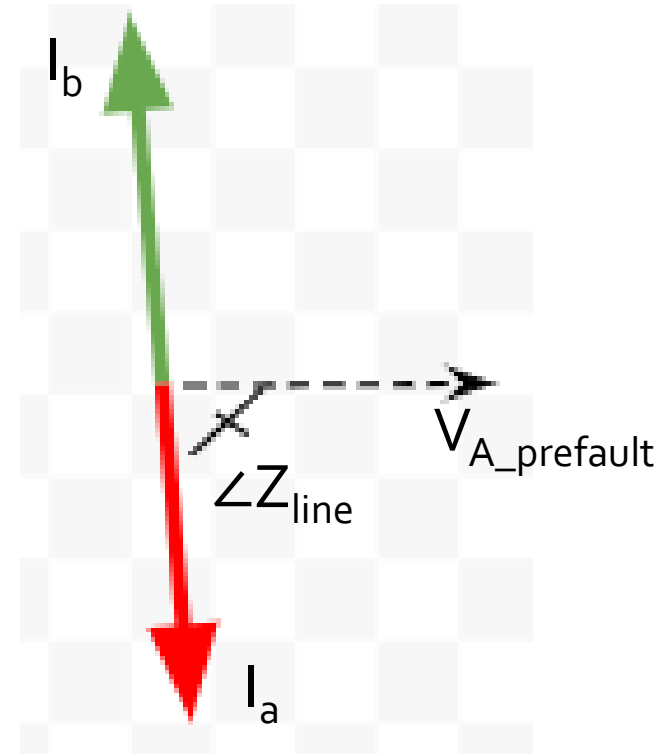
- Sync. Gen. currents on low side of Xfmr are:
 $I_a = -I_b ; I_c = 0$
 - Inverter current magnitude limited to 1.0 pu
- Pre-fault V_A angle is used as a reference to specify appropriate $I_{a,b,c}$ angles

Inverter Currents (A-G Fault)

Pre-Fault



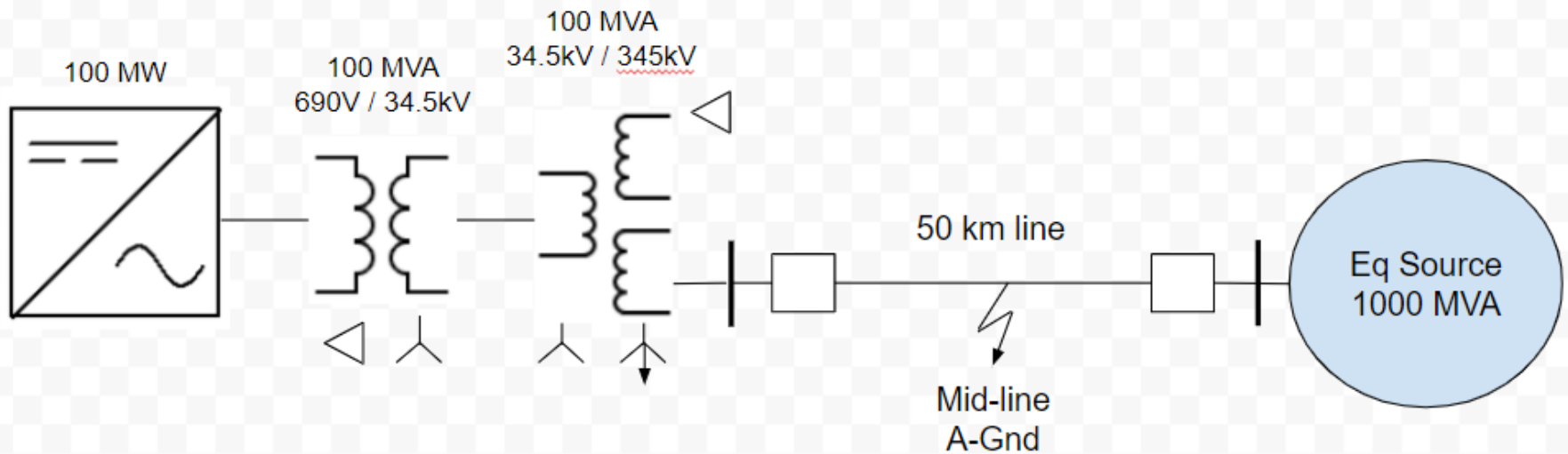
Post-Fault



Reference Currents Table

Fault	I_a	I_b	I_c
A-G	$1 \angle -85^\circ$	$1 \angle 95^\circ$	0
B-C	$0.5 \angle 180^\circ$	$0.5 \angle 180^\circ$	$1 \angle 0^\circ$
B-C-G	$0.5 \angle -150^\circ$	$0.5 \angle 150^\circ$	$1 \angle 0^\circ$
A-B-C-G	$1 \angle -115^\circ$	$1 \angle 125^\circ$	$1 \angle 5^\circ$

System One-line with IBR



690V: a,b,c

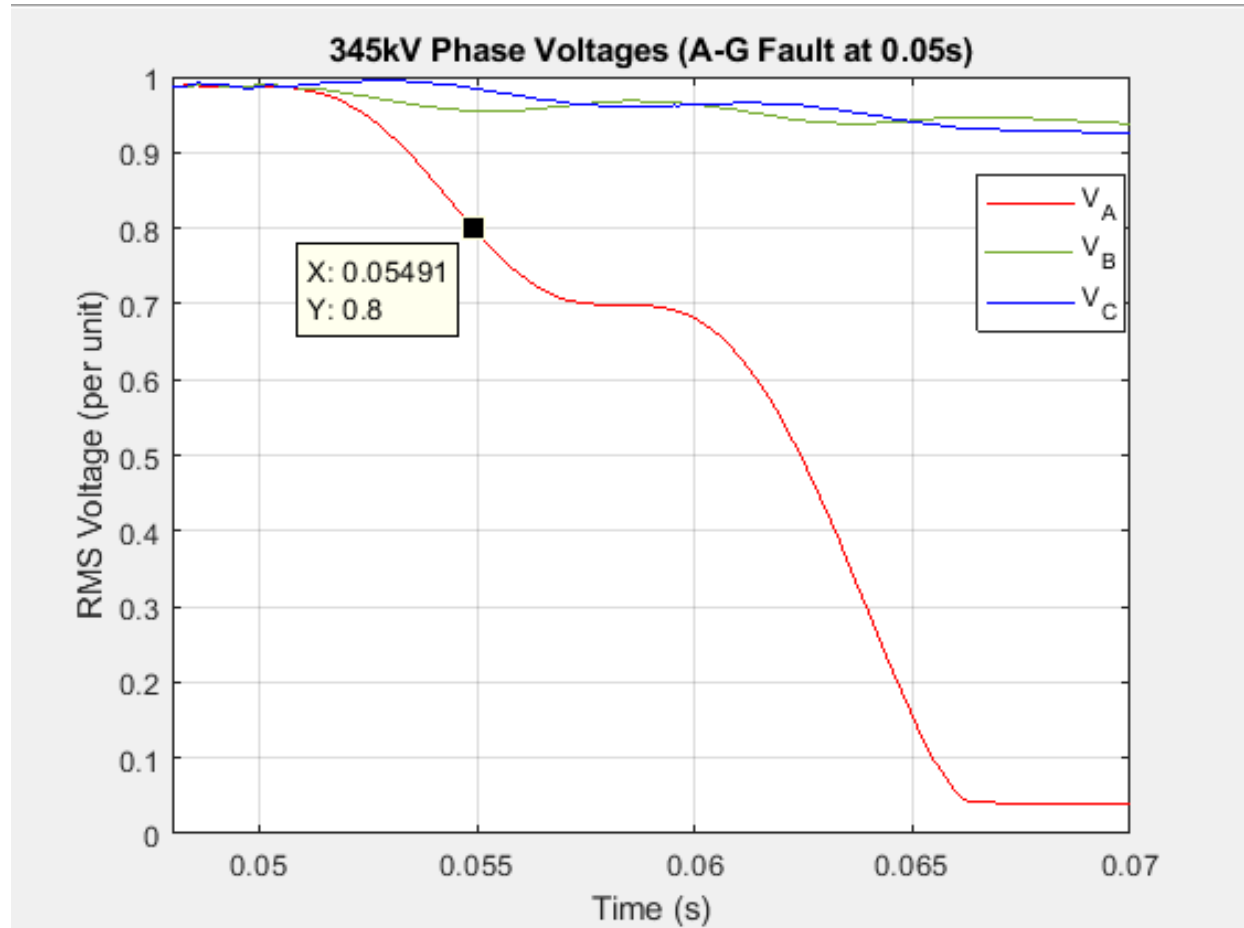
345kV: A,B,C

A-G Mid-line Fault Summary

- Fault detected
 - 1 cycle
- Inverter currents modified
 - 2 cycles
- Sync Gen behavior emulated within 3 cycles
 - I_A lags V_A by $\angle Z_{\text{line}}$

345kV Fault Detection

- A-G fault detected
 - 4.9 ms
- RMS 1 cycle moving window



Inverter Currents (690V)

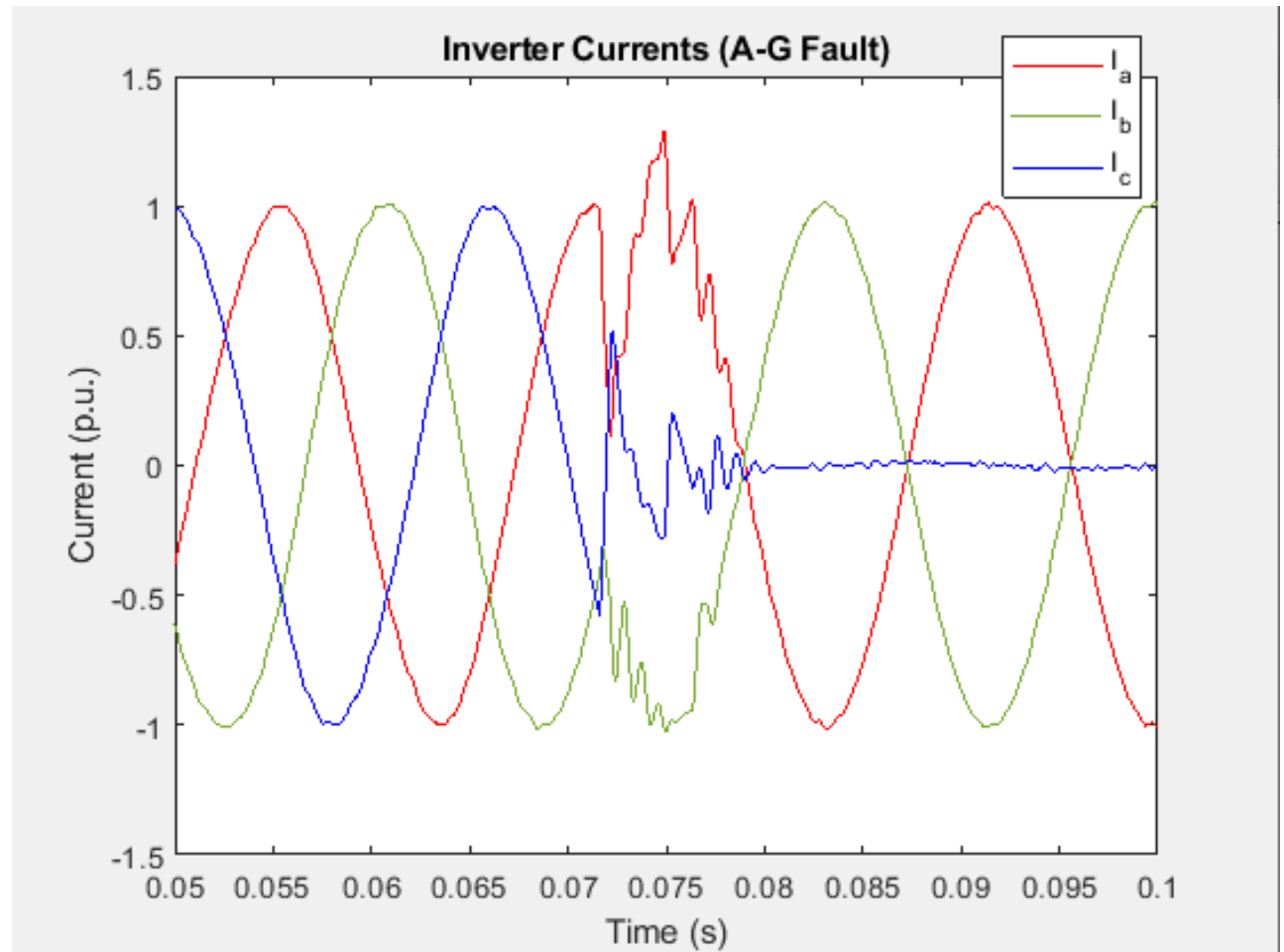
- Pre-fault
Balanced

- Post-fault

$$I_a = -I_b$$

$$I_c = 0$$

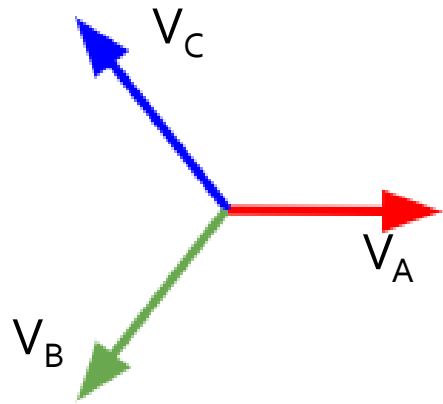
- 29 ms



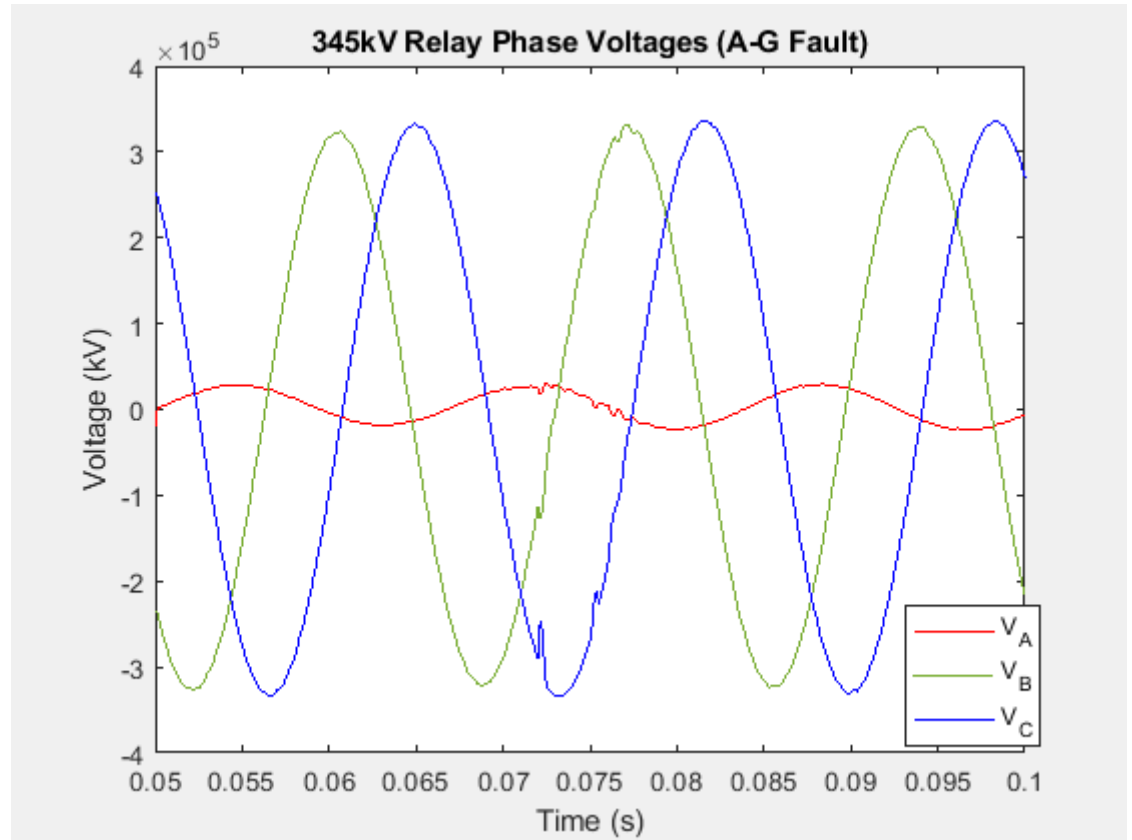
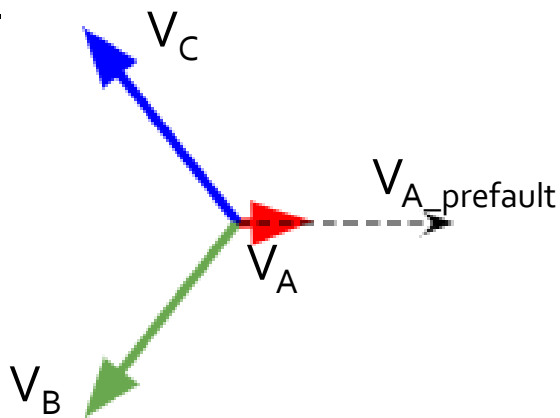
345kV Phase Voltages

Phasors

Pre-fault



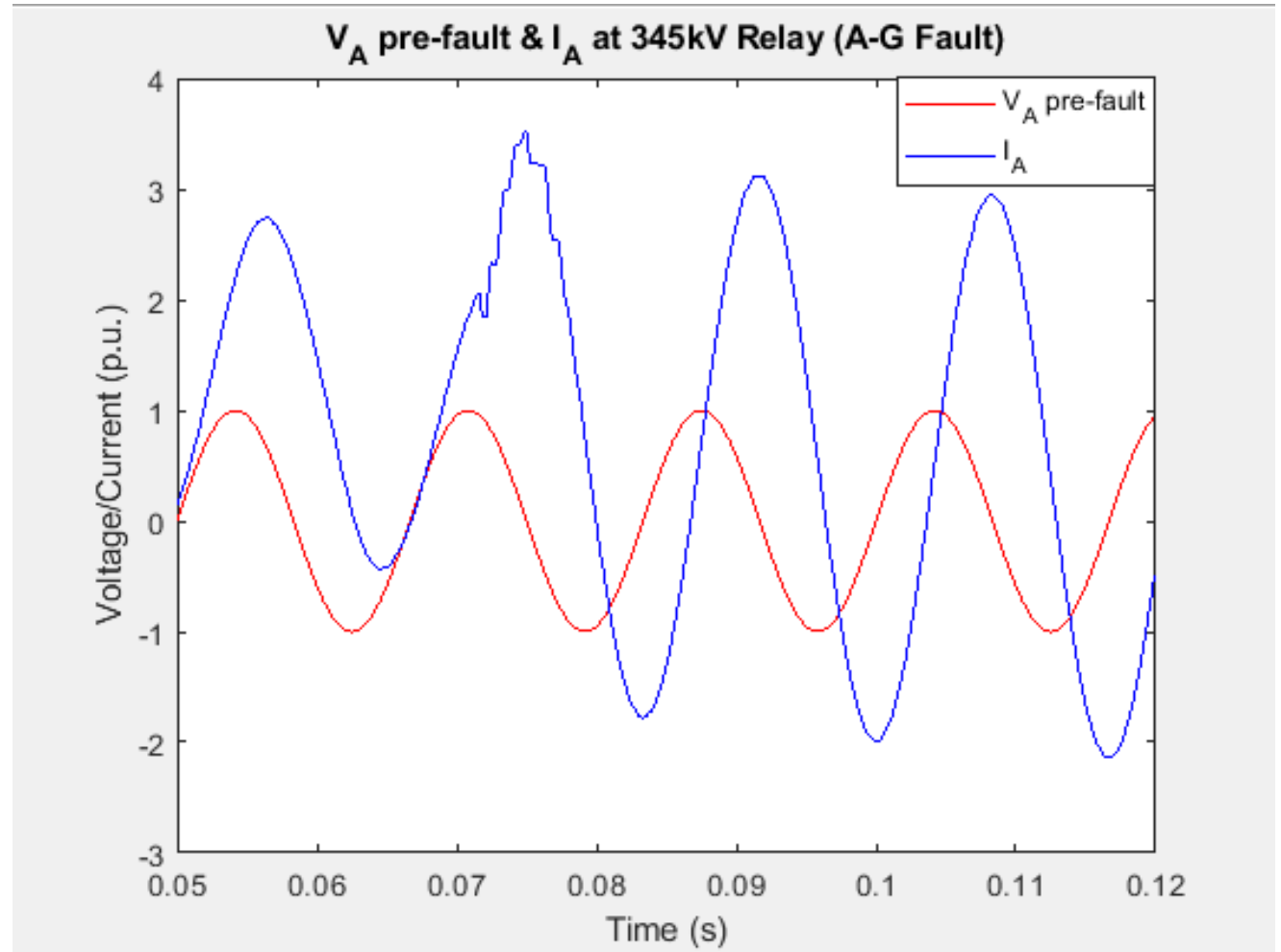
Post-fault



V_A & I_A Phase Relationship

I_A lags V_A
by
 $\angle Z_{\text{line}} (85^\circ)$

Within
3 cycles



COMTRADE Verification

- Played back on a relay from one manufacturer

Fault Type	Mid-Line		End-Line	
	Dist. (p.u.)	Zone-1?	Dist. (p.u.)	Zone-1?
A-G	0.493	Yes	0.991	No
B-C	0.503	Yes	0.995	No
B-C-G	0.562	Yes	1.048	No
A-B-C-G	0.502	Yes	1.009	No

- Fault impedance measured properly for all fault types

Future Work

- Hardware-in-the-loop with Opal-RT
- Energy storage as a source during fault
 - During low pre-fault output
- Testing additional manufacturer's relays

Acknowledgements



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 - kell2390@umn.edu
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