

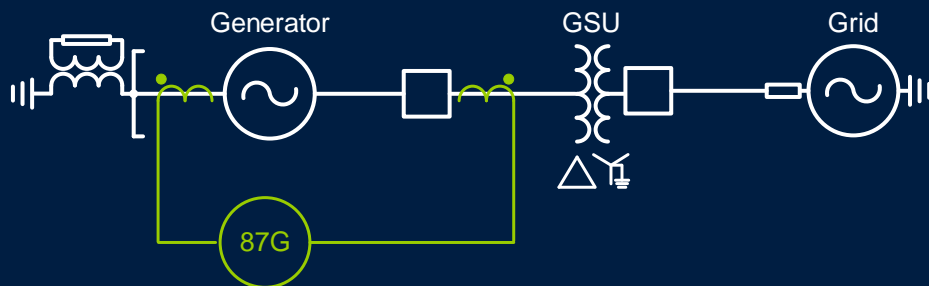
Determining CT Requirements for Generator and Transformer Protective Relays

Ritwik Chowdhury, Dale Finney, and Normann Fischer
Schweitzer Engineering Laboratories, Inc.

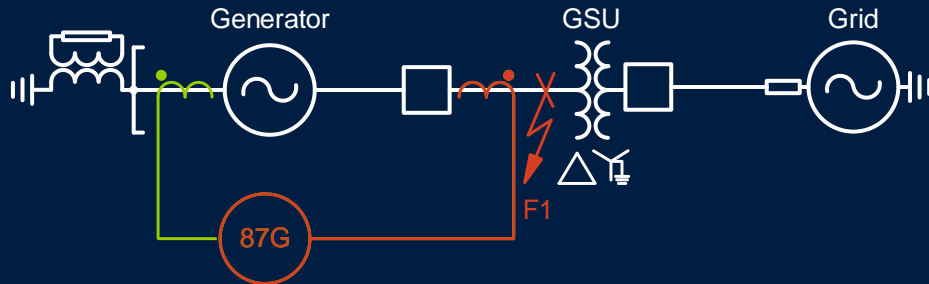
Douglas Taylor
Avista Utilities

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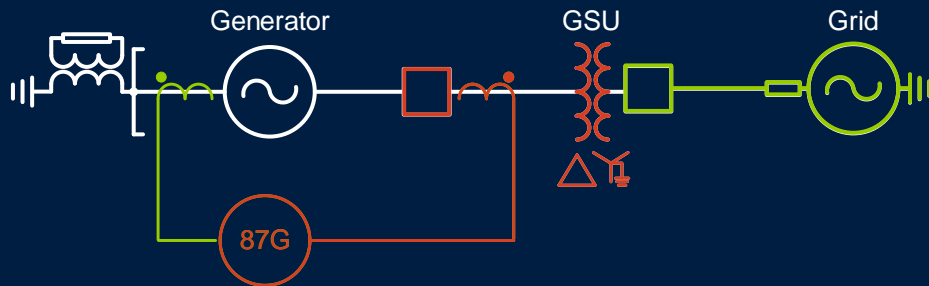
Introduction



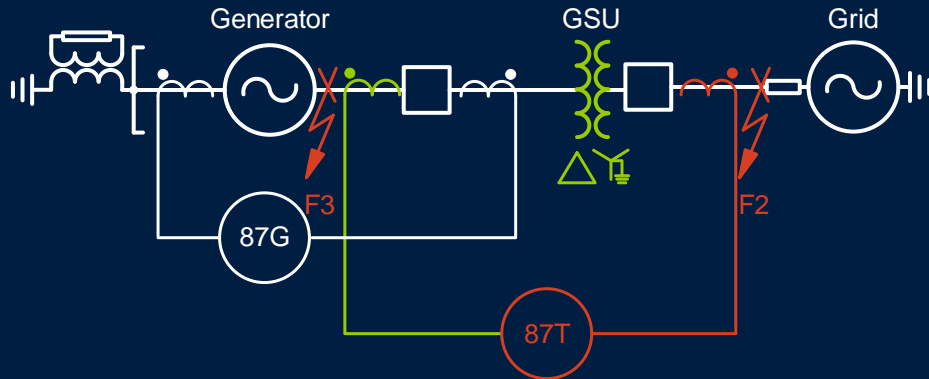
Introduction



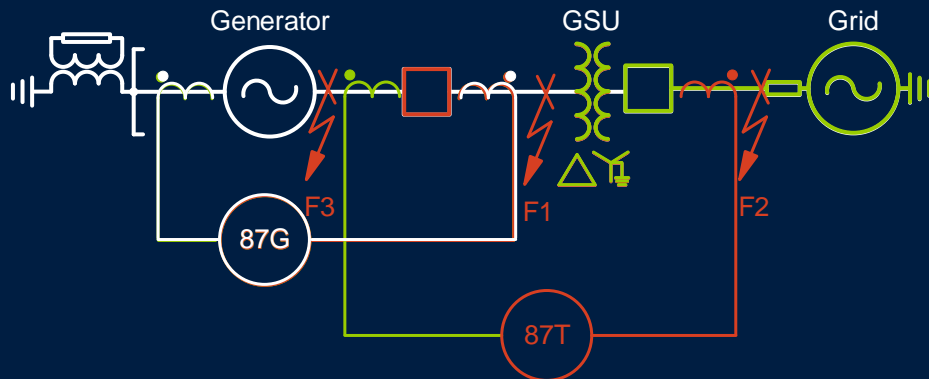
Introduction



Introduction



Introduction



Overview

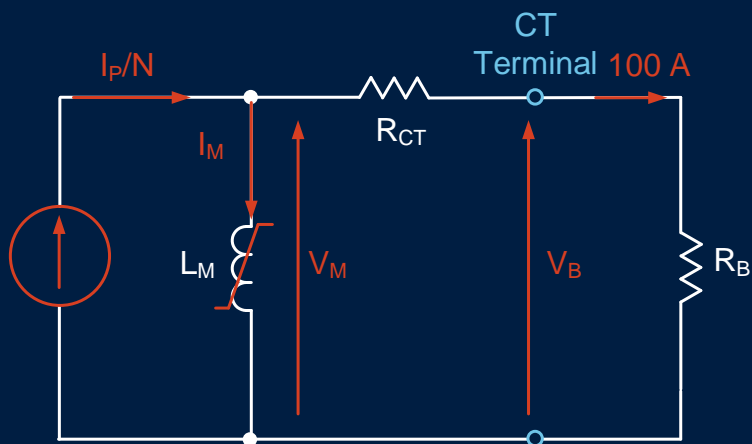
- IEEE and IEC guidance
 - DC offset
 - Remanence
- CT models
- Differential relay scheme
- Test method and results
 - CT sizing
 - Relay settings

Overview

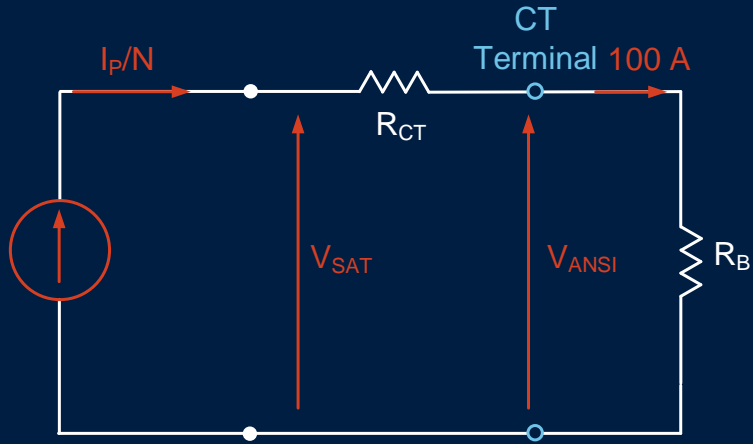
- IEEE and IEC guidance
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IEEE and IEC Guidance

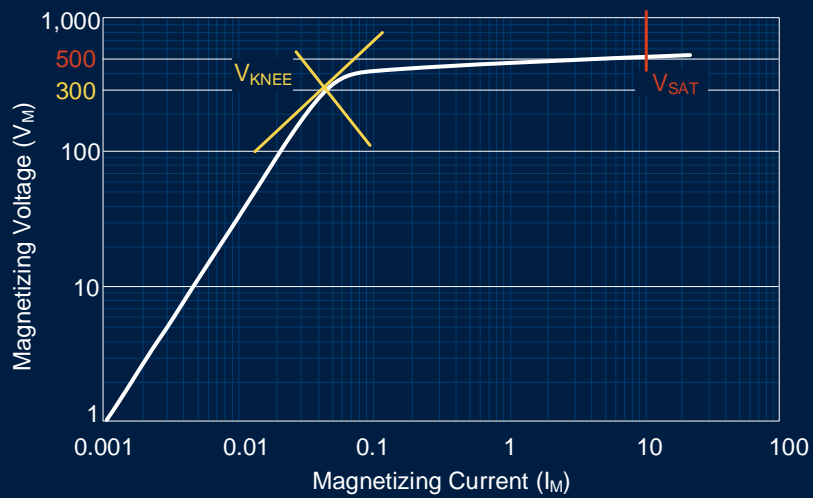
CT Equivalent Circuit



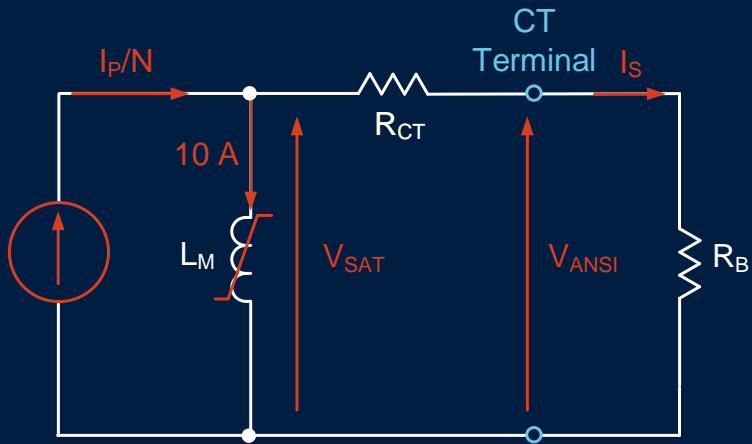
CT Equivalent Circuit



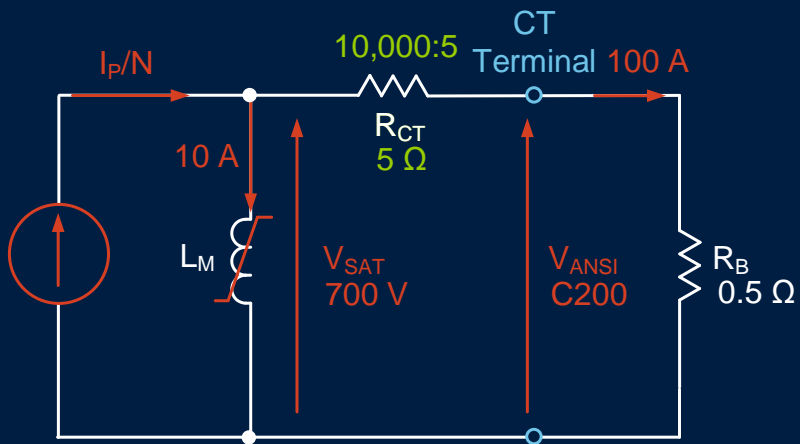
Saturation Voltage in Excitation Curve



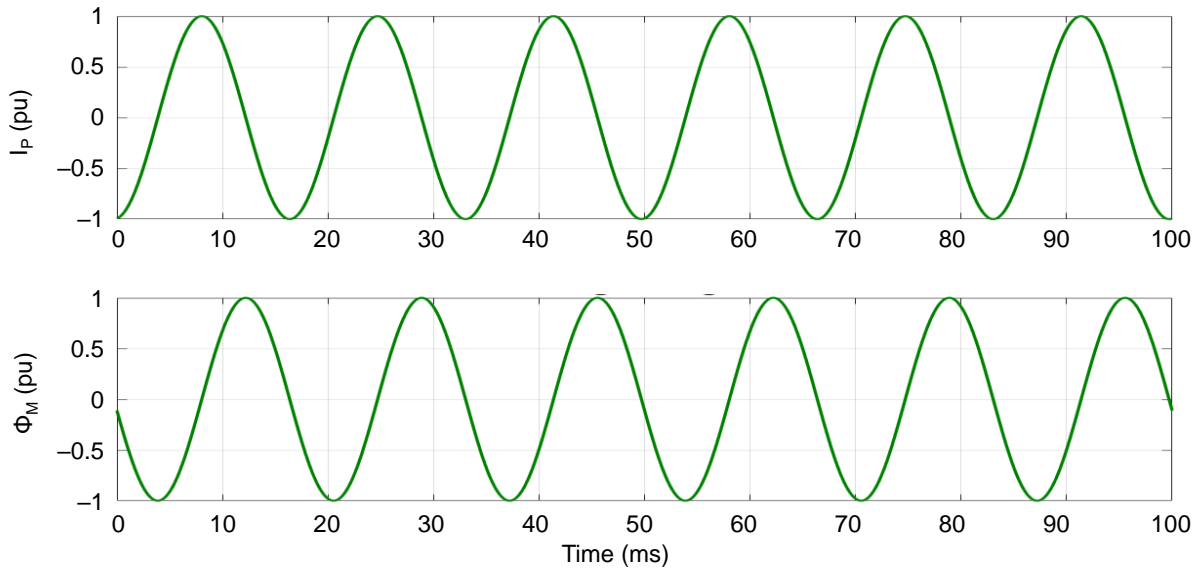
CT Equivalent Circuit



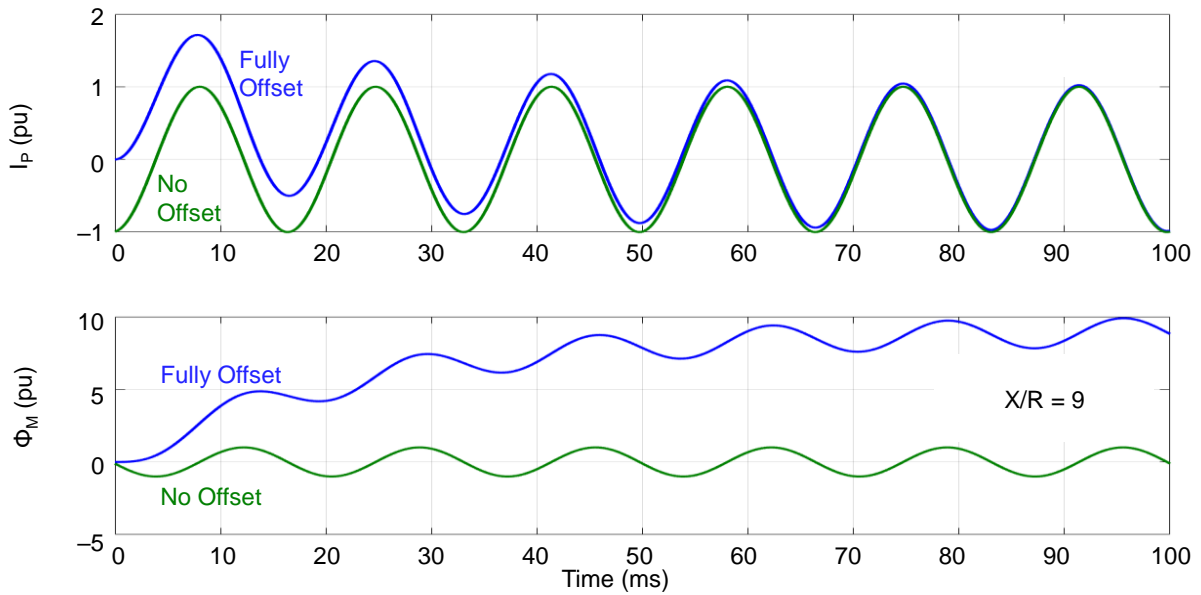
CT Equivalent Circuit



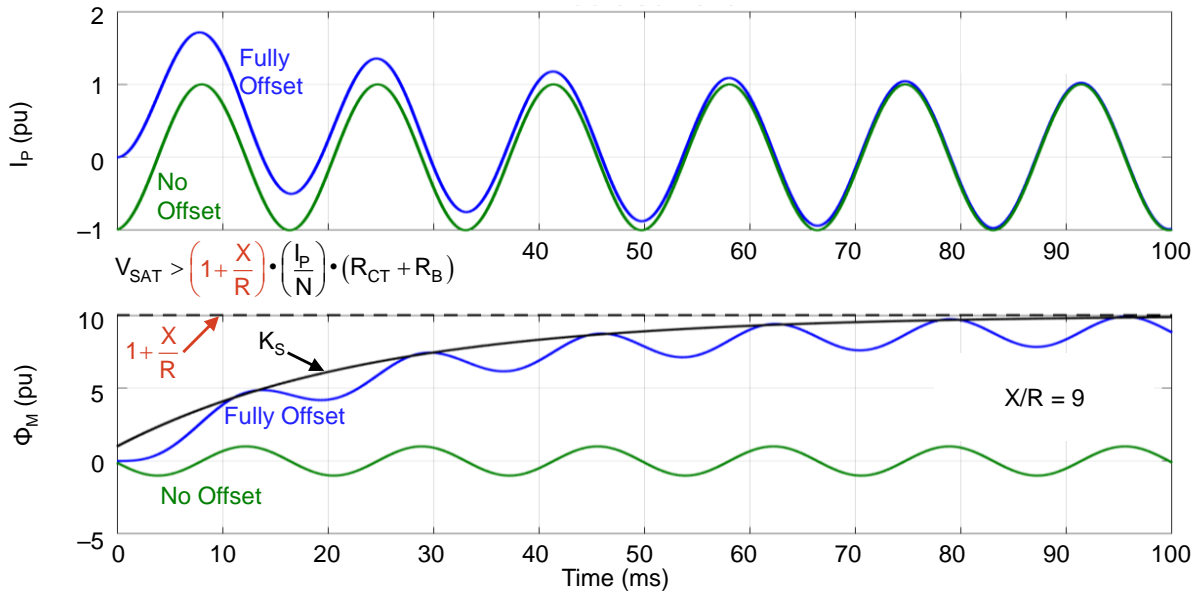
Fault Current and CT Flux



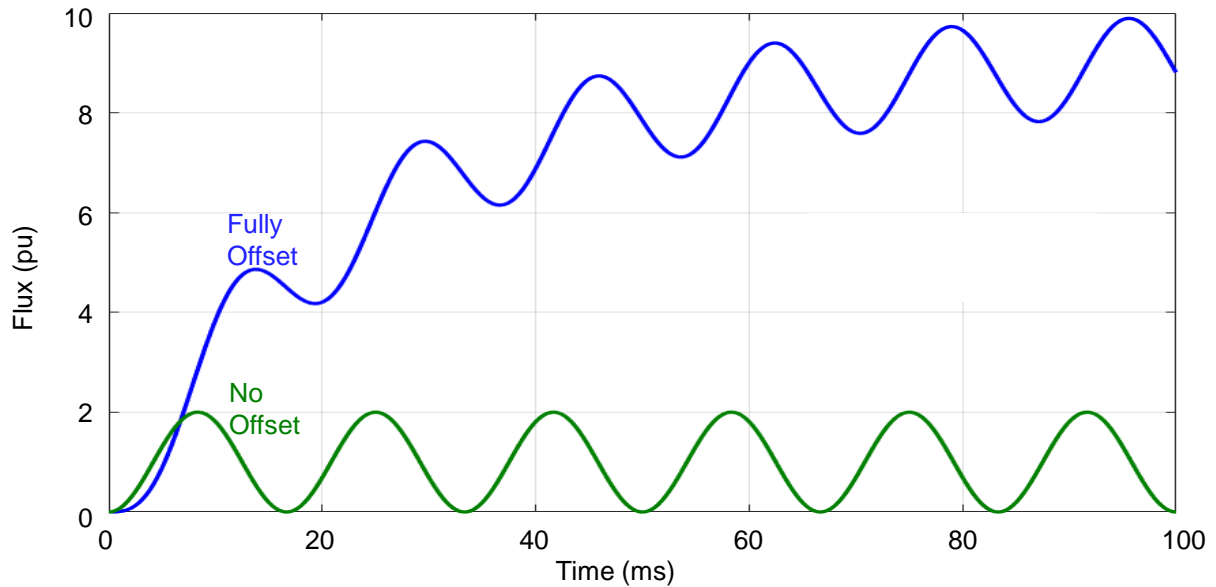
Fault Current and CT Flux



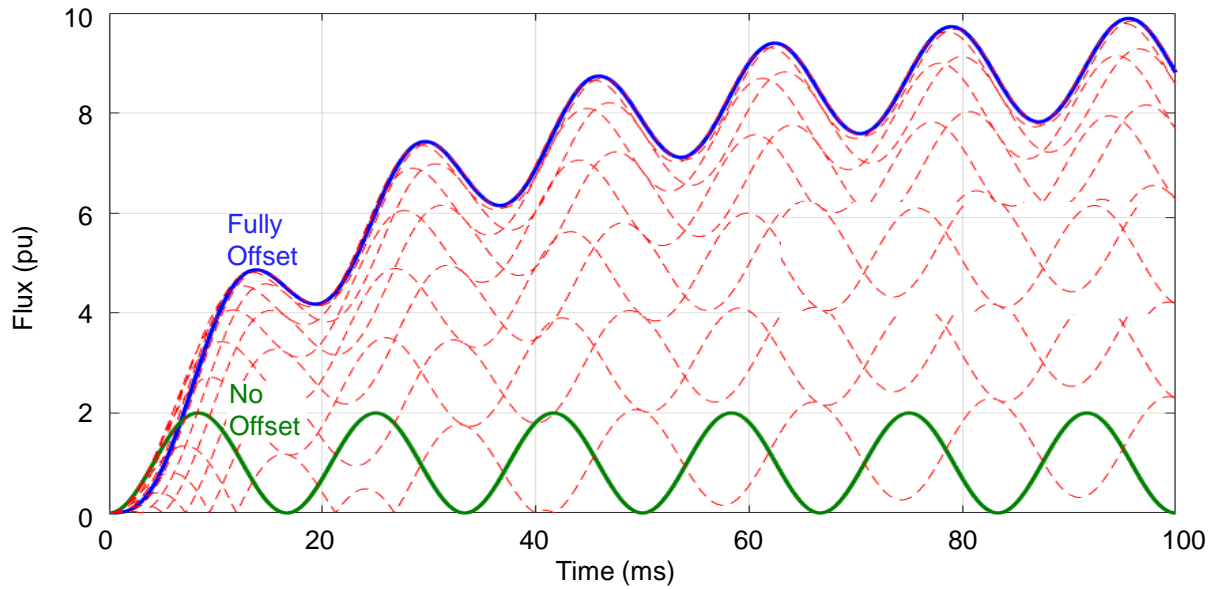
Fault Current and CT Flux



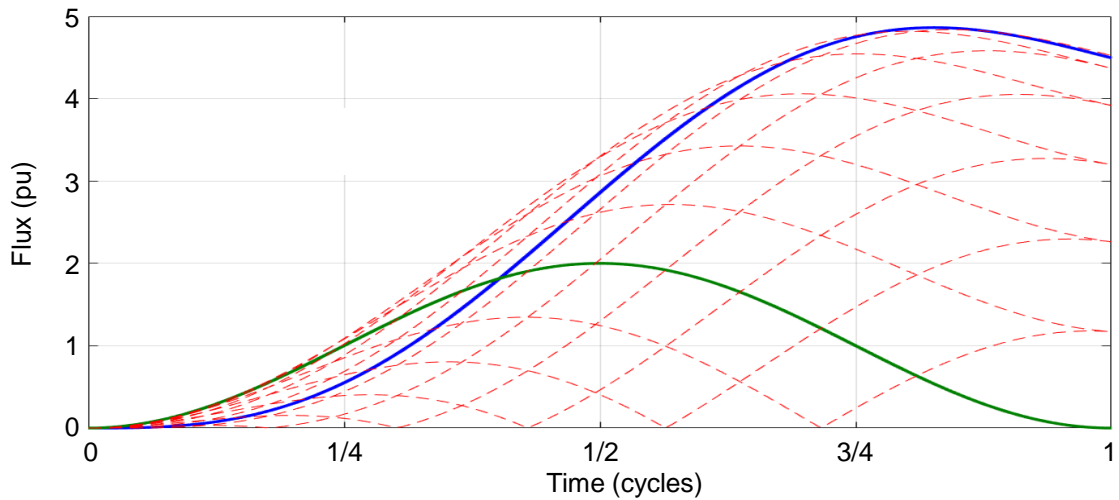
Effect of Fault Inception Angle



Effect of Fault Inception Angle



Effect of Point-on-Wave



$$K_{TD} = K_S = \frac{V_{SAT}}{I_S \cdot (R_{CT} + R_B)}$$

(IEC) (IEEE)

$$\begin{aligned} &\rightarrow V_{ANSI} = K_S \cdot I_S \cdot R_B \\ &\rightarrow V_{SAT} = K_{TD} \cdot I_S \cdot (R_{CT} + R_B) \end{aligned}$$

Remanence

CT Sizing DC Offset and Remanence

IEEE

$$V_{SAT} = \left(1 + \frac{X}{R}\right) \cdot I_S \cdot (R_B + R_{CT})$$

DC and Relay

$$1 - \text{Rem}$$

Remanence

Ohm's Law

IEC

$$E_{AL} = (K_{TD} \cdot K_{REM}) \cdot I_S \cdot (R_B + R_{CT})$$

$$K_{REM} = \frac{1}{1 - \text{Rem}}$$

IEEE and IEC Surveys

IEEE

Remanent Flux	Percentage of CTs
0–20	39
21–40	18
41–60	16
61–80	27

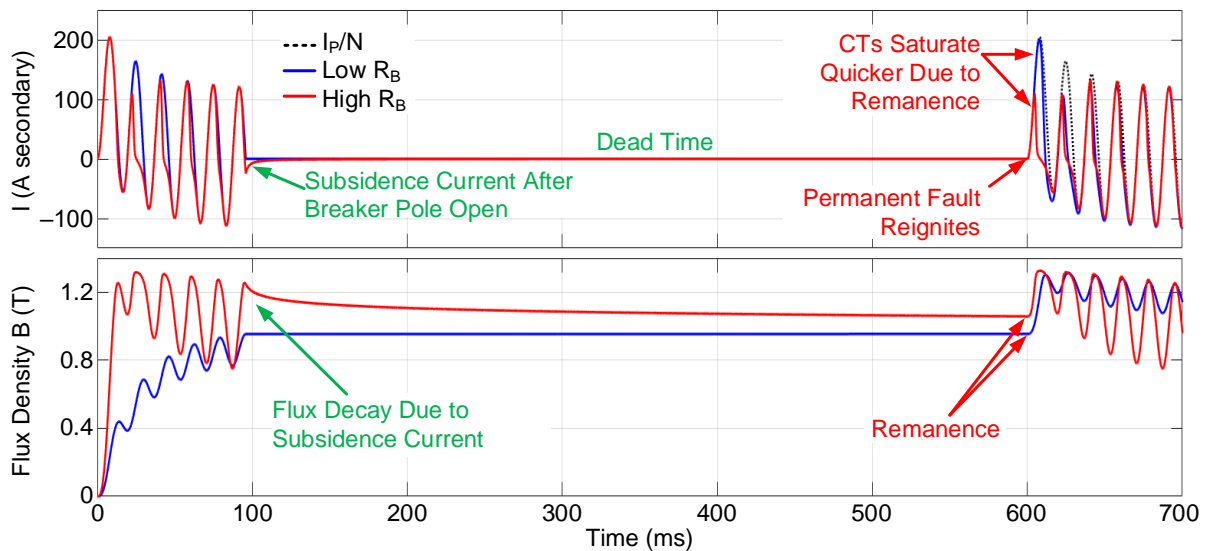
Remanent Flux Survey on 230 kV System

IEC

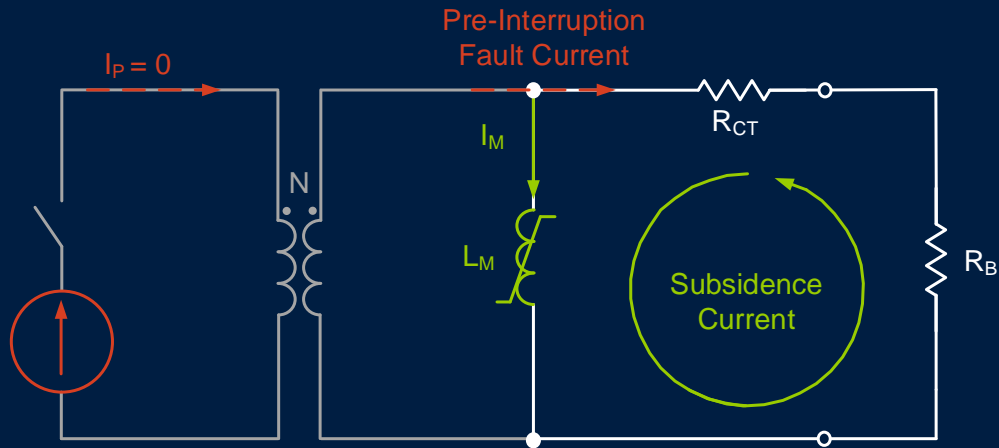
	Old CT Cores	New CT Cores
Theoretical Remanence	75–77%	88–95%
Measured Remanence	70–75%	85–87%

Theoretical and Measured Remanence

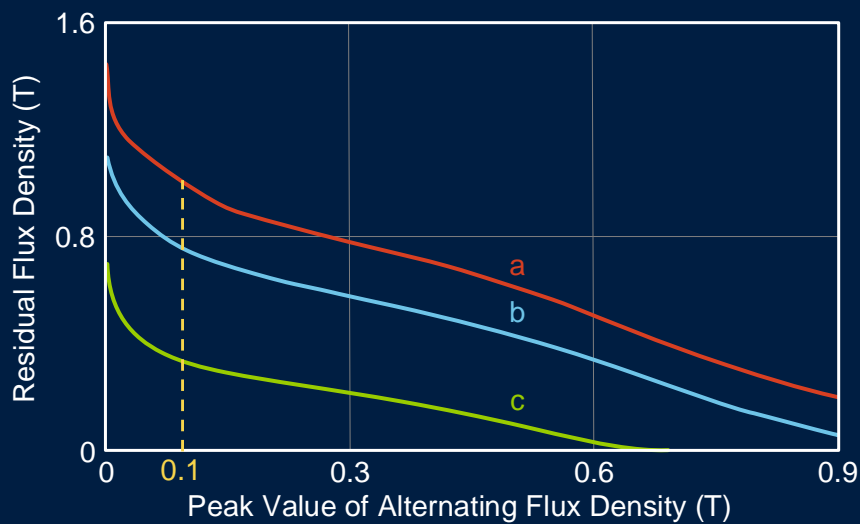
Effect of Faults on Remanence



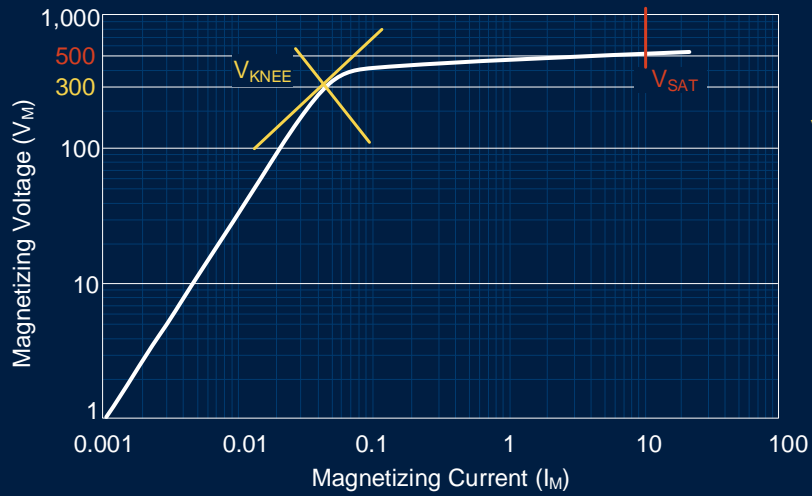
Effect of Fault Current on Remanence



Effect of Load

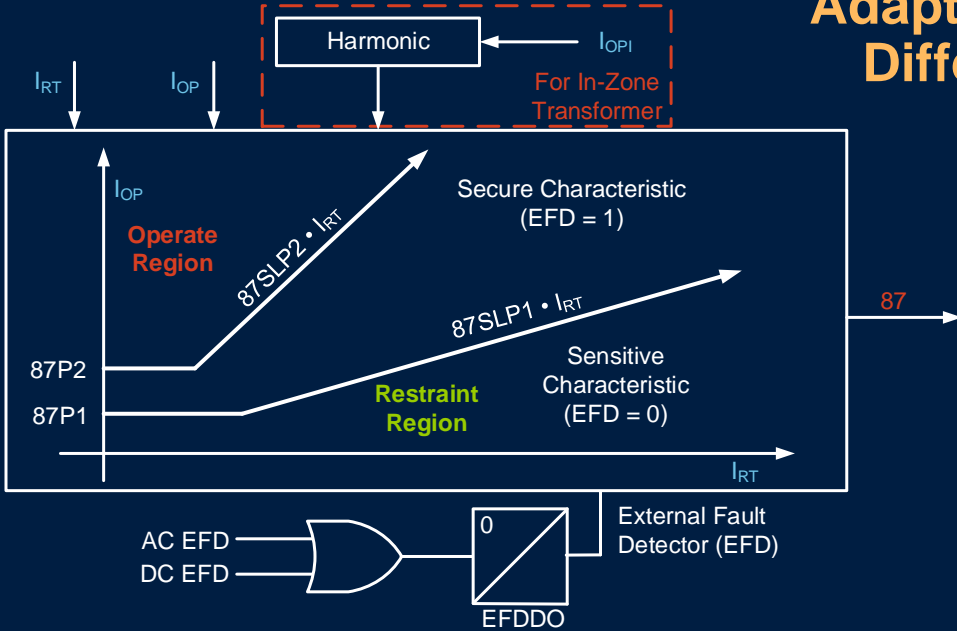


Load and Excitation Curve

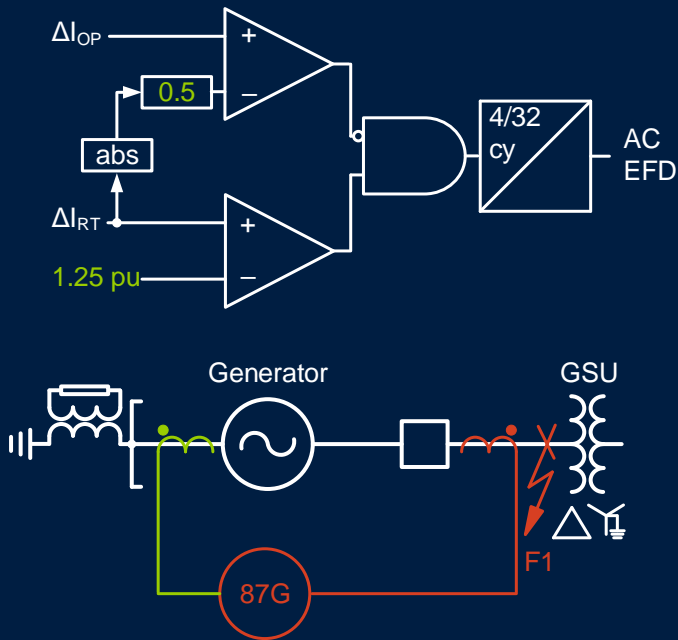


Protective Relay Scheme

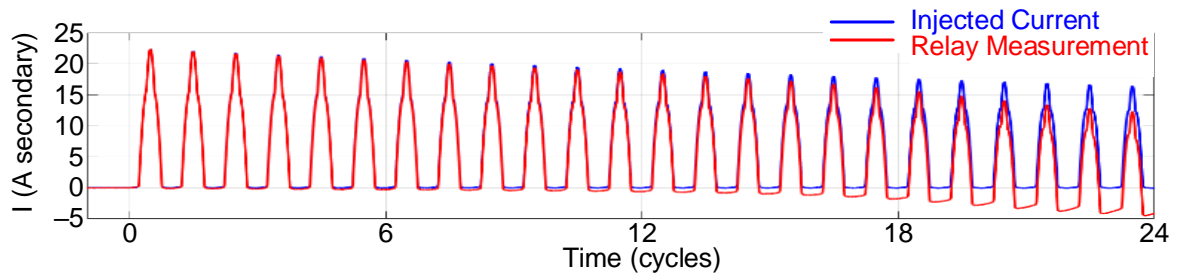
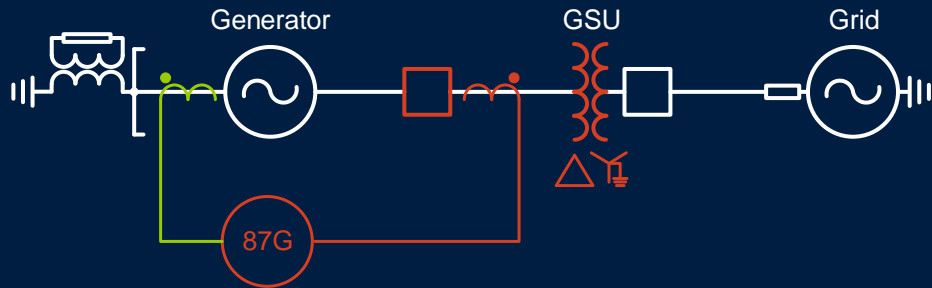
Adaptive Slope Differential



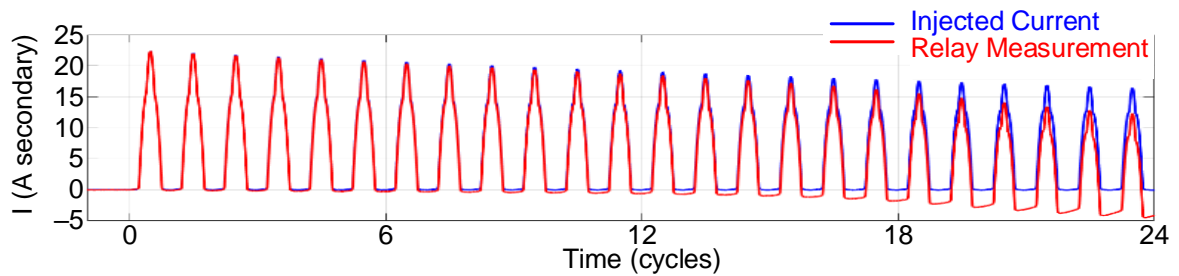
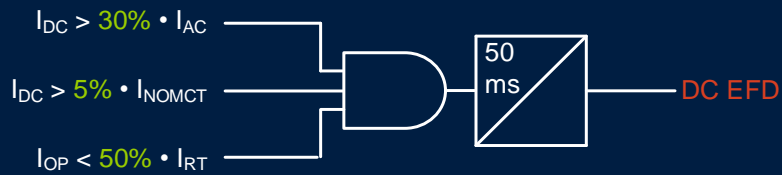
External Fault Detector – AC EFD



External Fault Detector – DC EFD

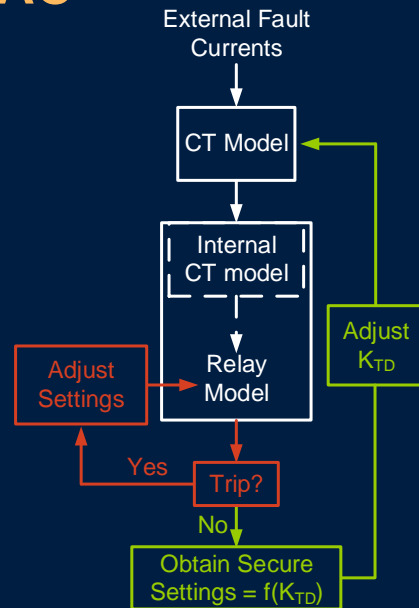


External Fault Detector – DC EFD



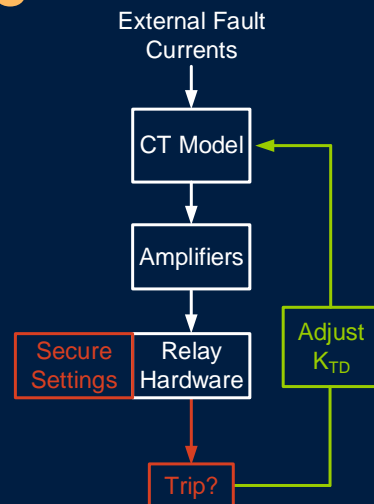
Test Method – AC

- Point on wave (0 to 360)
- X/R: up to 100
- Both ground and phase
- One saturated CT, other not
- 87P1 and 87SLP1 set low
- Simulations with 5% margin

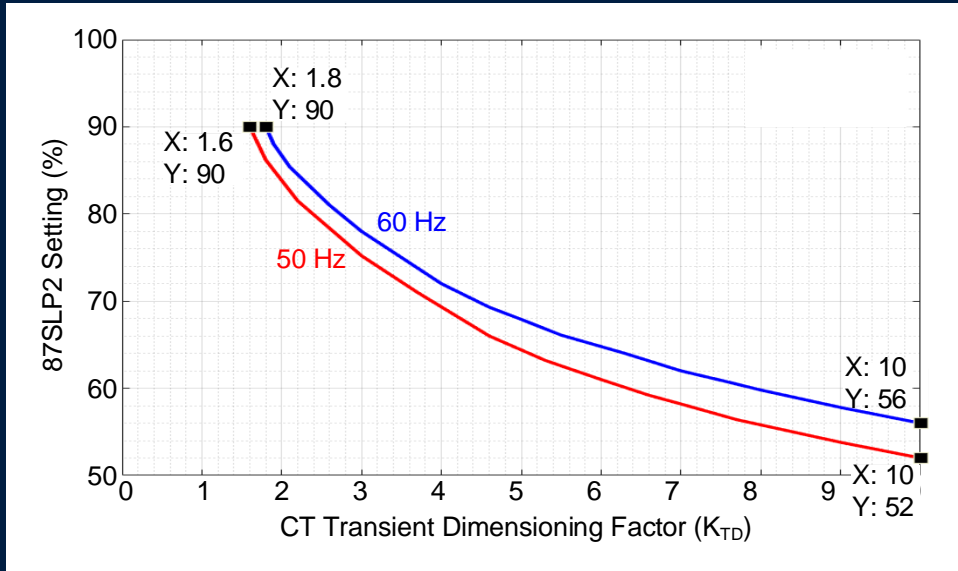


Test Method – AC

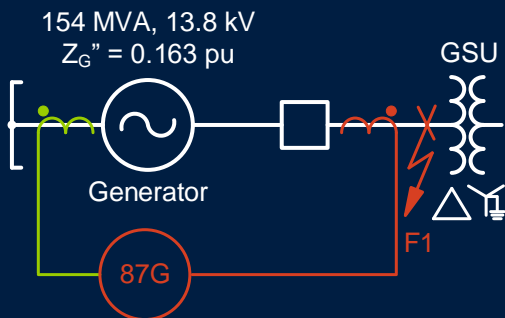
- Point on wave (0 to 360)
- X/R: up to 100
- Both ground and phase
- One saturated CT, other not
- 87P1 and 87SLP1 set low
- Simulations with 5% margin
- Hardware-in-the-loop verification



CT Sizing Requirements and Relay Setting



CT Sizing Requirement



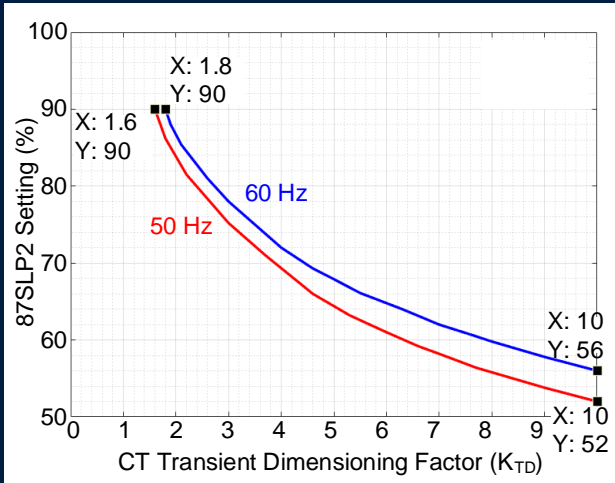
$$V_{ANSI} = K_{REM} \cdot K_{S_MIN} \cdot \left(\frac{I_F}{N}\right) \cdot R_B$$

$$V_{ANSI} = 3 \cdot 1.8 \cdot \left(\frac{39,530 \text{ A}}{2,000}\right) \cdot 0.372 \Omega = 39.7 \text{ V}$$

$$V_{SAT} = 3 \cdot 1.8 \cdot \left(\frac{39,530 \text{ A}}{2,000}\right) \cdot (0.372 \Omega + 5 \Omega) = 573.3 \text{ V}$$

$$V_{SAT_CT} = 100 \text{ V} + 20 \cdot 5 \text{ A} \cdot 5 \Omega = 600 \text{ V}$$

CT Sizing Requirements and Relay Setting



$$V_{ANSI} = K_{REM} \cdot K_{S_MIN} \cdot \left(\frac{I_F}{N}\right) \cdot R_B$$

$$V_{ANSI} = 3 \cdot 1.8 \cdot \left(\frac{39,530 \text{ A}}{2,000}\right) \cdot 0.372 \Omega = 39.7 \text{ V}$$

$$V_{SAT} = 3 \cdot 1.8 \cdot \left(\frac{39,530 \text{ A}}{2,000}\right) \cdot (0.372 \Omega + 5 \Omega) = 573.3 \text{ V}$$

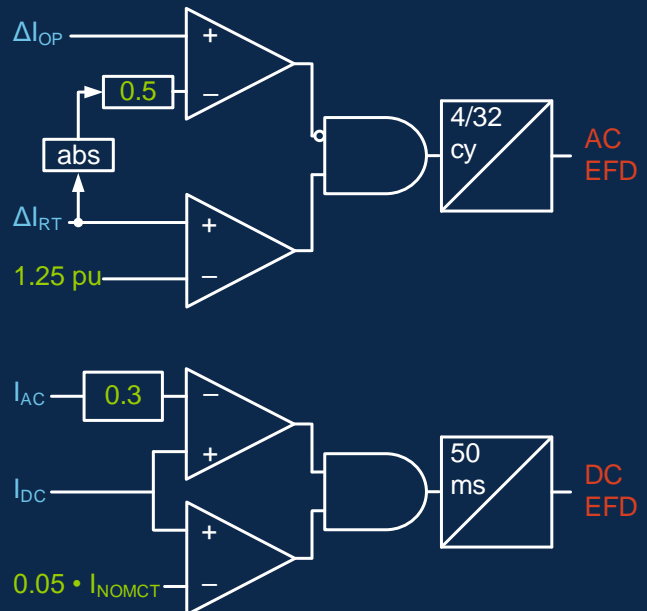
$$V_{SAT_CT} = 400 \text{ V} + 20 \cdot 5 \text{ A} \cdot 5 \Omega = 900 \text{ V}$$

$$K_{TD} = \left(\frac{900 \text{ V}}{573.3 \text{ V}}\right) \cdot 1.8 = 2.83$$

87SLP2 = 79%

Test Method and Results – DC

- Down to a K_S of 1
- Lower inrush
 - AC EFD drops out, but dc EFD does not
87P2 = 0.50 pu
 - DC EFD drops out
87P1 = 0.15 pu • I_{nom}/TAP
~ 0.25 pu



CT Requirements Summary

CT Size and Relay Setting

Before  After

$$V_{\text{SAT}} = \left(1 + \frac{X}{R}\right) \cdot I_{\text{S}} \cdot (R_{\text{B}} + R_{\text{CT}})$$

$$V_{\text{SAT}} = 100 \cdot \frac{39,530 \text{ A}}{2,000} \cdot 5.372 \Omega = 1,062 \text{ V}$$

$$V_{\text{ANSI}} = \text{C800} + (20 \cdot 5 \text{ A} \cdot 5 \Omega) = 1,300 \text{ V}$$

$$\text{SLP2} = \text{SLP1} = 10\%?$$

Remanence?

$$V_{\text{SAT}} = (K_{\text{REM}} \cdot K_{\text{TD}}) \cdot I_{\text{S}} \cdot (R_{\text{B}} + R_{\text{CT}})$$

$$V_{\text{SAT}} = (3 \cdot 1.8) \cdot \frac{39,530 \text{ A}}{2,000} \cdot 5.372 \Omega = 573.3 \text{ V}$$

$$V_{\text{ANSI}} = \text{C100} + (20 \cdot 5 \text{ A} \cdot 5 \Omega) = 600 \text{ V}$$

$$\text{SLP2} = 90\%$$

CT Size and Relay Setting

Before  After

$$V_{\text{SAT}} = \left(1 + \frac{X}{R}\right) \cdot I_{\text{S}} \cdot (R_{\text{B}} + R_{\text{CT}})$$

$$V_{\text{SAT}} = 100 \cdot \frac{39,530 \text{ A}}{2,000} \cdot 5.372 \Omega = 1,062 \text{ V}$$

$$V_{\text{ANSI}} = \text{C800} + (20 \cdot 5 \text{ A} \cdot 5 \Omega) = 1,300 \text{ V}$$

$$\text{SLP2} = \text{SLP1} = 10\% ?$$

Remanence?

$$V_{\text{SAT}} = (K_{\text{REM}} \cdot K_{\text{TD}}) \cdot I_{\text{S}} \cdot (R_{\text{B}} + R_{\text{CT}})$$

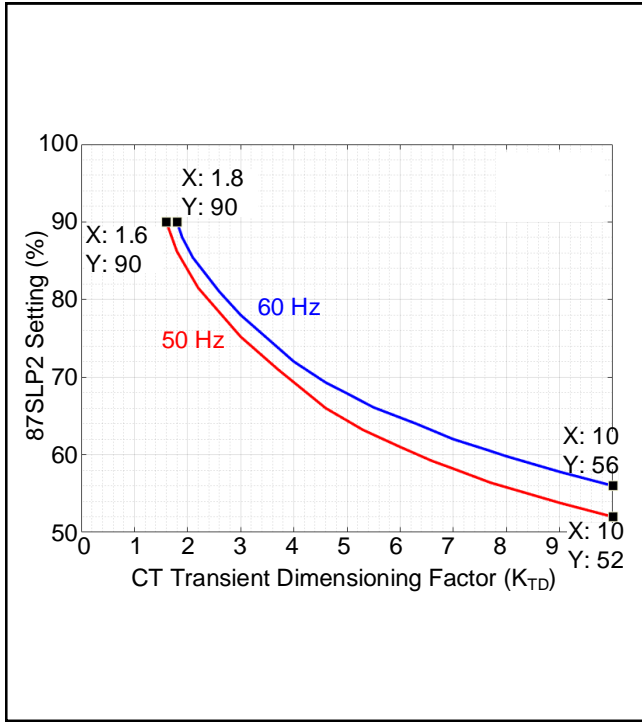
$$V_{\text{SAT}} = (3 \cdot 1.8) \cdot \frac{39,530 \text{ A}}{2,000} \cdot 5.372 \Omega = 573.3 \text{ V}$$

$$V_{\text{ANSI}} = \text{C400} + (20 \cdot 5 \text{ A} \cdot 5 \Omega) = 900 \text{ V}$$

$$\text{SLP2} = 79\%$$

Conclusion

- Both IEEE and IEC consider dc offset and remanence
- Use of CT models is neither ideal nor required
- Modern differential relay schemes can drastically reduce CT requirements
- Unambiguous application guidance results in precise
 - CT sizing
 - Relay settings



Questions?