

SDG&E Relay Standards – Updating Tertiary Bus and Reactor Protection

Bill Cook

Retired From San Diego Gas & Electric

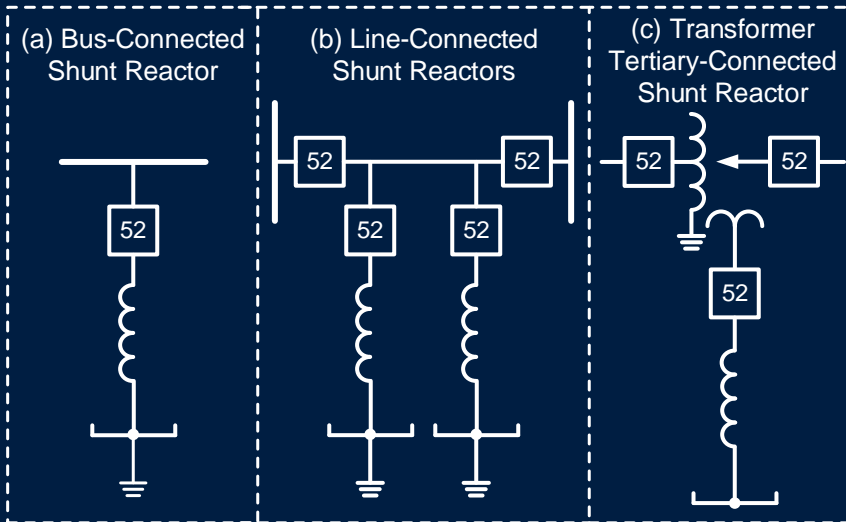
Michael J. Thompson and Kamal Garg
Schweitzer Engineering Laboratories, Inc.

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Introduction

- Overview of shunt reactor design
- Shunt reactor protection and design
- Tertiary-connected, air-core shunt reactor
- Overview of SDG&E system and standards
 - Existing standards
 - Future standards
 - Protection scheme and set points

Overview of Shunt Reactor

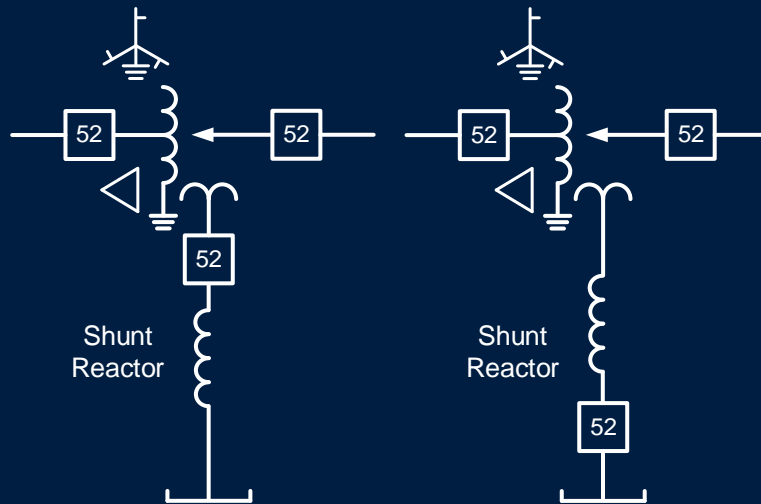


- Above 52 kV usually directly connected at bus
- Typical reactor size 30–300 MVAR
- Single phase 125–375 MVAR

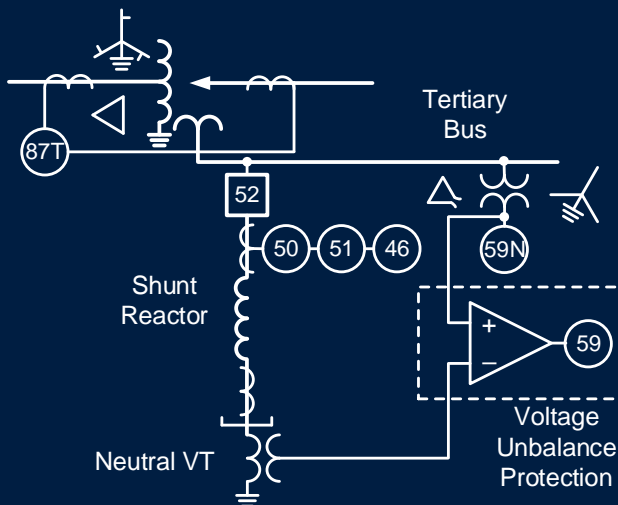
Overview of Shunt Reactor

- Three-legged gapped iron core
- Five-legged gapped iron core
- Shell-type gapped iron core
- Coreless (air core)

Tertiary-Connected, Dry-Type Reactor Protection

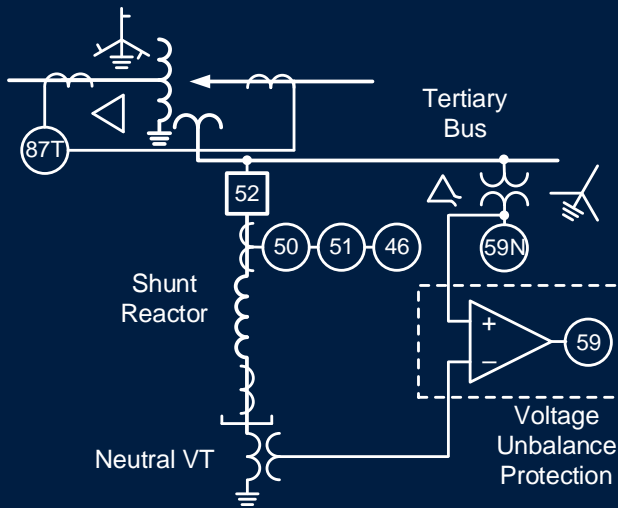


Tertiary-Connected, Dry-Type Reactor Protection



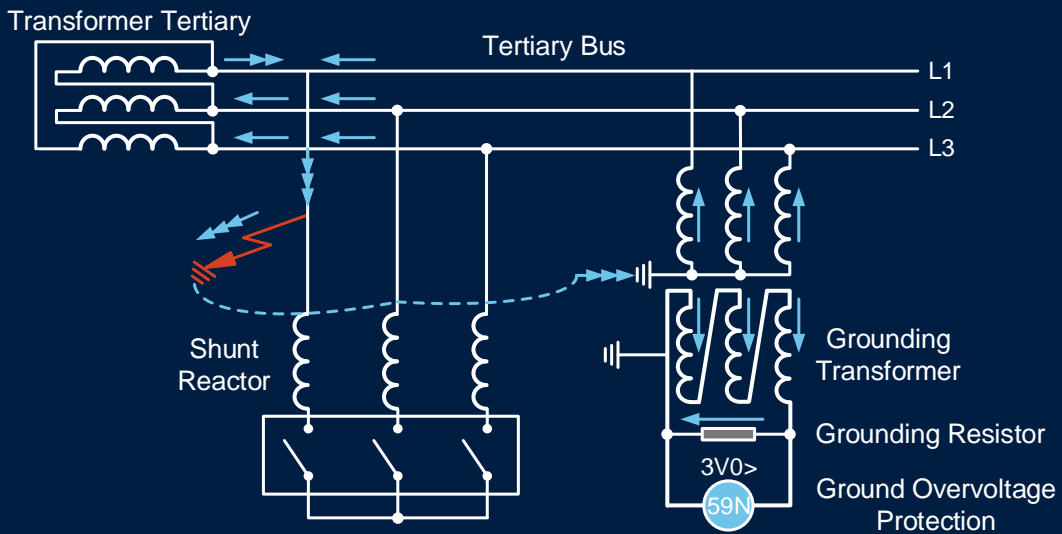
- Instantaneous overcurrent (50)
- Time-delayed overcurrent (51)
- Negative-sequence (46)
- Ground overvoltage (59N)
- Special schemes: turn-to-turn (T-T) faults

Tertiary-Connected, Dry-Type Reactor Protection

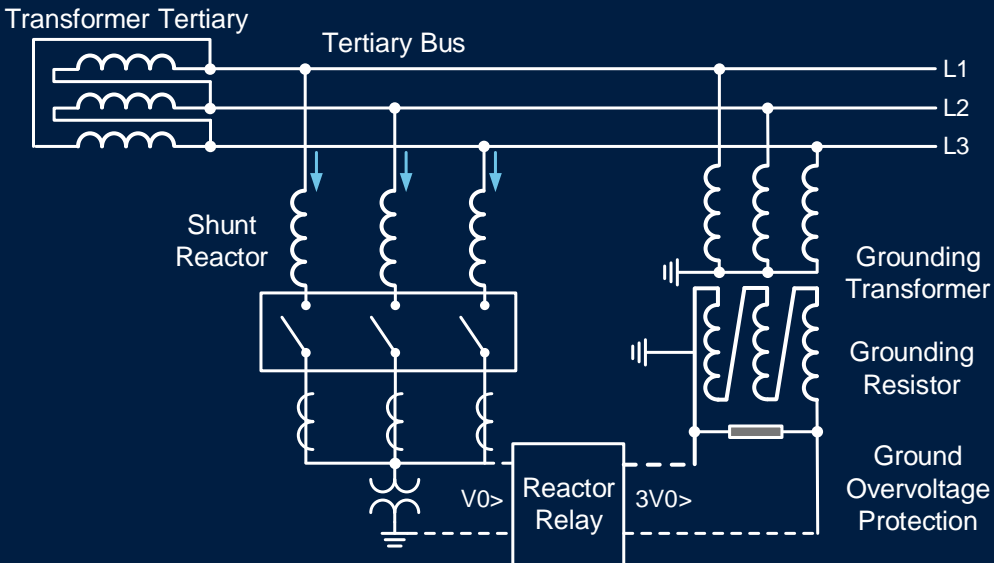


- Phase differential
 - Transformer differential (87T) when shunt reactor included in power transformer
 - Separate reactor phase differential protection
- Breaker failure (50BF)

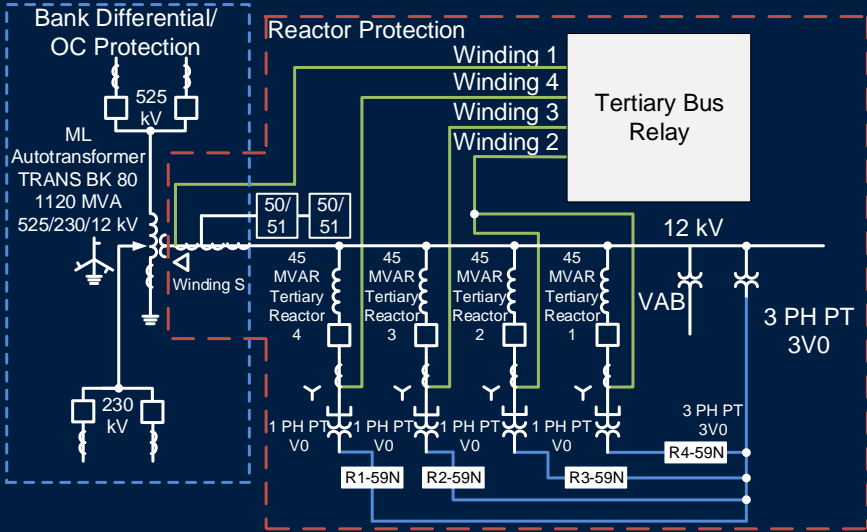
Tertiary Bus Ground Voltage



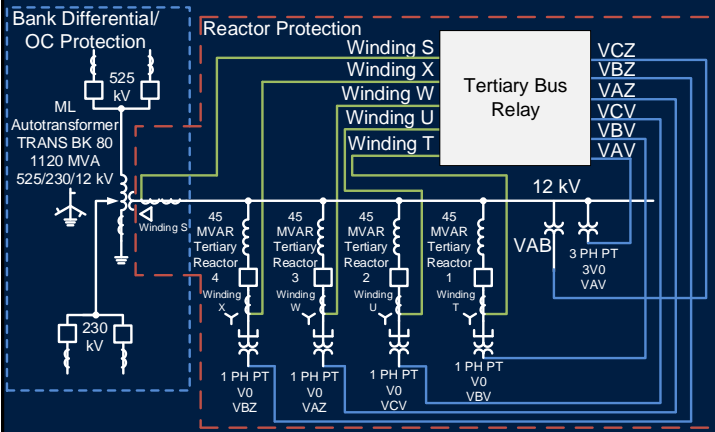
Tertiary Reactor – Normal and Fault Scenarios



SDG&E Shunt Reactor Upgrade 1 – 2004

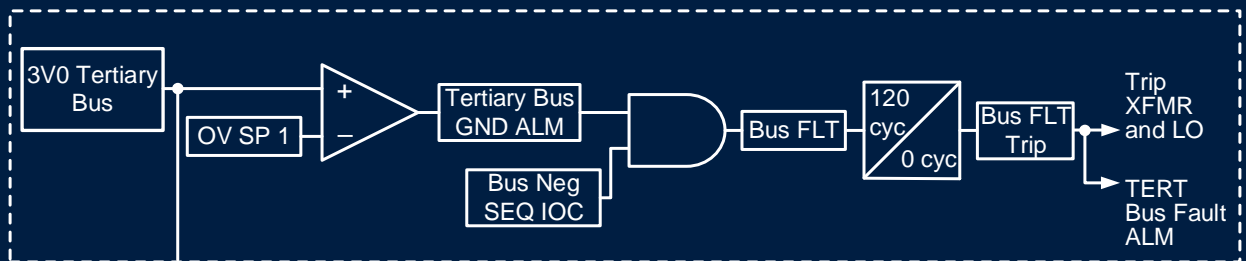


SDG&E Shunt Reactor Upgrade 2 – 2019



Winding / Connection	Device	Comments
Wdg. S	12 kV bus	3-phase CT, delta
Wdg. T	Reactor 1	3-phase CT, wye
Wdg. U	Reactor 2	3-phase CT, wye
Wdg. W	Reactor 3	3-phase CT, wye
Wdg. X	Reactor 4	3-phase CT, wye
VAV	12 kV ground detection	3-phase PT = 3V0
VBV	Reactor 1	1-phase PT = V0
VCV	Reactor 2	1-phase PT = V0
VAZ	Reactor 3	1-phase PT = V0
VBZ	Reactor 4	1-phase PT = V0
VCZ	VAB 12 kV bus	Voltage reference

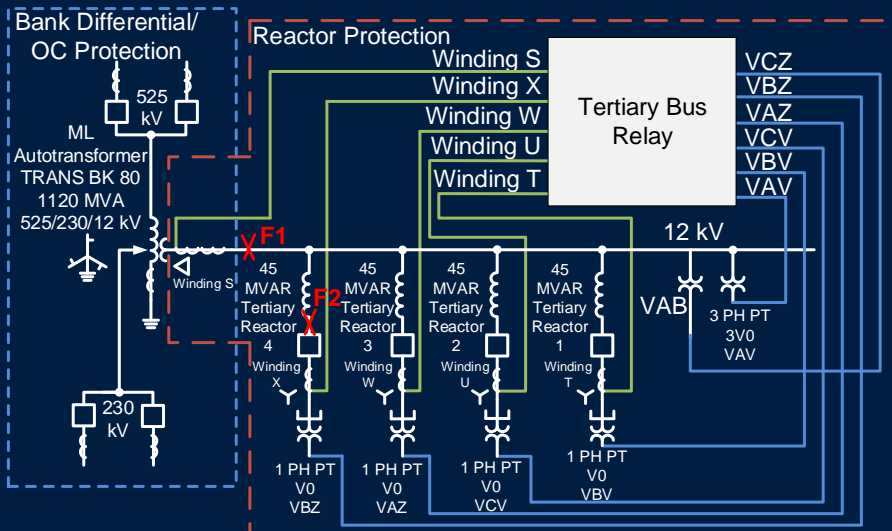
Tertiary Fault – Neutral Side of Reactor



Front-Panel Design Details

<input type="radio"/> ENABLED	<div style="border: 1px solid black; border-radius: 50%; width: 40px; height: 40px; display: flex; align-items: center; justify-content: center;"> TARGET RESET </div>
<input type="radio"/> TRIP	
<input type="radio"/> TER BUS GND	<input type="radio"/> TER BUS DIFF
<input type="radio"/> REAC1 CB STATUS	<input type="radio"/> TER BUS OC
<input type="radio"/> REAC2 CB STATUS	<input type="radio"/> TER NEG SEQ
<input type="radio"/> REAC3 CB STATUS	<input type="radio"/> SPARE
<input type="radio"/> REAC4 CB STATUS	<input type="radio"/> SPARE
<input type="radio"/> SPARE	<input type="radio"/> SPARE
<input type="radio"/> REAC1 TT FAULT	<input type="radio"/> REAC3 TT FAULT
<input type="radio"/> REAC1 CB FAIL	<input type="radio"/> REAC3 CB FAIL
<input type="radio"/> REAC1 BF	<input type="radio"/> REAC3 BF
<input type="radio"/> REAC2 TT FAULT	<input type="radio"/> REAC4 TT FAULT
<input type="radio"/> REAC2 CB FAIL	<input type="radio"/> REAC4 CB FAIL
<input type="radio"/> REAC2 BF	<input type="radio"/> REAC4 BF

F1 / F2 and Protection Discussion



- F1 fault
 - 3P – 87R / 50P
 - PP – 87R / 50P
- F2 fault
 - 3P – 87R
 - PP – 87R / 50Q / 51Q

F1 / F2 faults require opening high-side breakers

Protection Element Guidelines

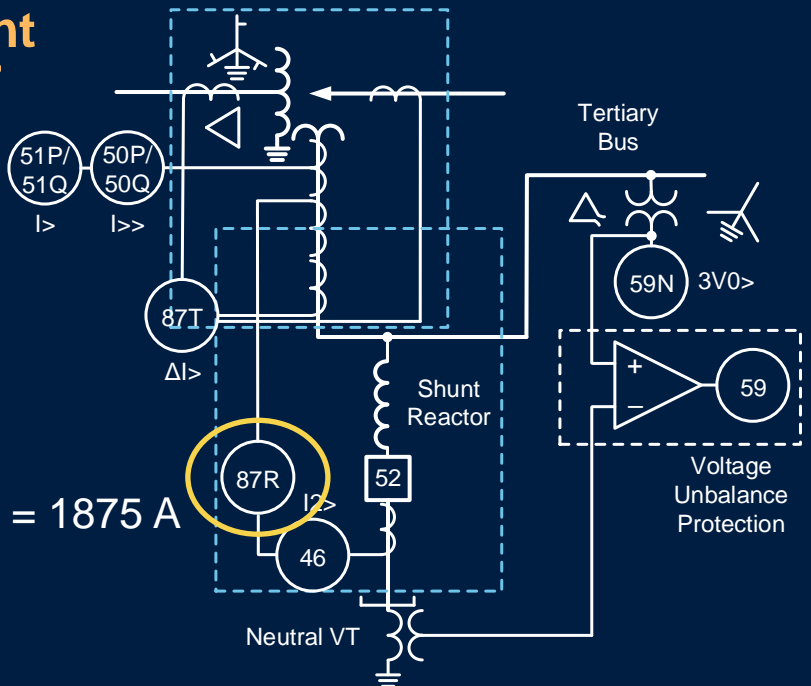
- Differential (87P)
- Phase overcurrent (50P / 51P) on bank tertiary current transformer (CT) winding
- Negative-sequence (50Q / 51Q) on bank tertiary CT winding
- T-T (50 / 51Q) on reactor breaker CTs
- V0 and 3V0 (59 ground detection, custom logic)

Protection Element Guidelines – DIFF

Differential (87R)

$$\begin{aligned} O_{87P} &= 0.2 \cdot I_{NOM} \\ &= 0.2 \cdot 8660 \text{ A} \\ &= 1732 \text{ A} \end{aligned}$$

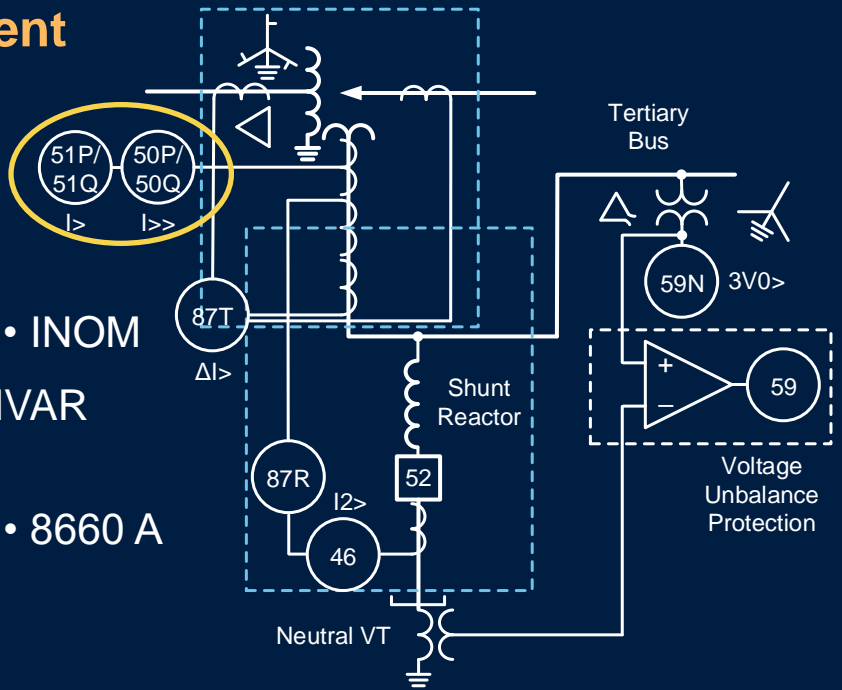
- Adaptive slope
- Phase-to-phase fault = 1875 A
- SLP1 = 15%
- SLP2 = 50%



Protection Element Guidelines – Overcurrent

50P / 51P element

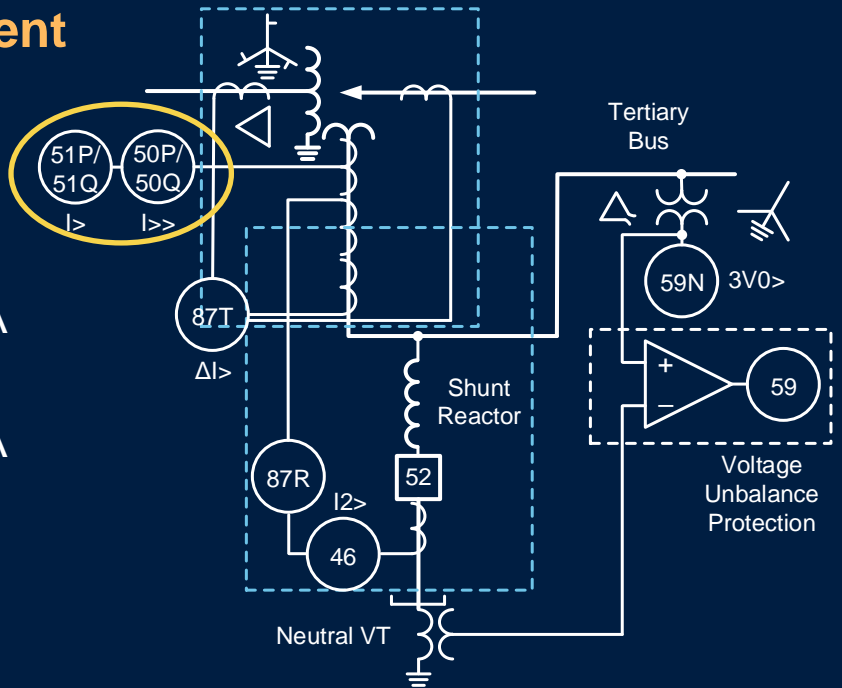
- $50P = 1.1 \cdot 1.25 \cdot INOM$
- $INOM = 4 \cdot 45 \text{ MVAR} = 8660 \text{ A}$
- $50P = 1.1 \cdot 1.25 \cdot 8660 \text{ A} = 11,900 \text{ A}$
- 51P OFF



Protection Element Guidelines – Overcurrent

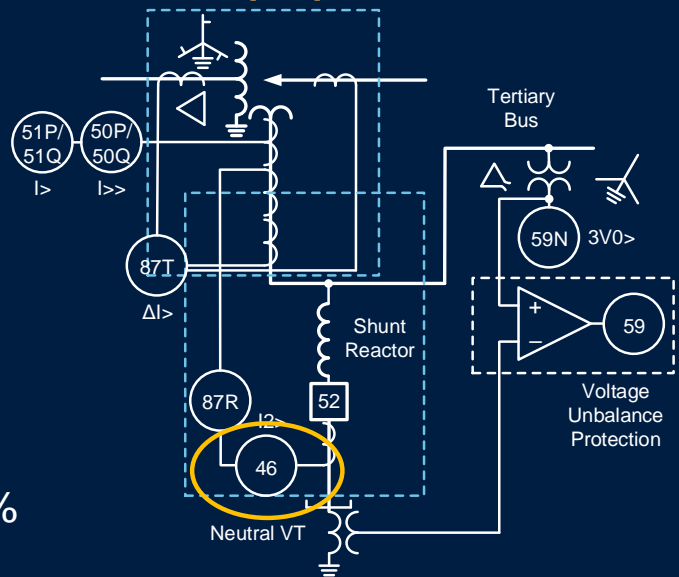
50Q / 51Q element

- $50Q = 0.4 \cdot 3264 \text{ A} = 1300 \text{ A}$
- $51Q = 0.2 \cdot 3264 \text{ A} = 650 \text{ A}$
- IEEE Inverse and time dial = 0.5



Reactor Breaker Turn-to-Turn Fault Negative-Sequence Overcurrent (46)

- Breaker on neutral
- Opening breaker clears T-T fault
- Inductance varies with turn short
 - $(0.95)^2 \cdot X_L = 0.9 X_L$
 - $(0.90)^2 \cdot X_L = 0.8 X_L$
- 150 A pickup provides 2.6% T-T, 2 seconds



Conclusion

- Dry-type tertiary bus and reactor protection standards
- SDG&E protection design using modern relays
- Improved redundancy and simplified design
- Negative-sequence overcurrent with ground detection
- Protection element selection and settings
- Design and documentation

Questions?