

A Creative Line Differential Protection Scheme for the Hudson River Crossing Section of a 345kV Transmission Line

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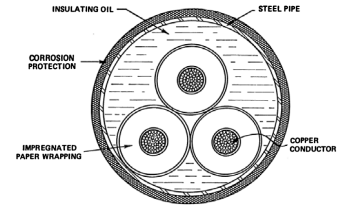
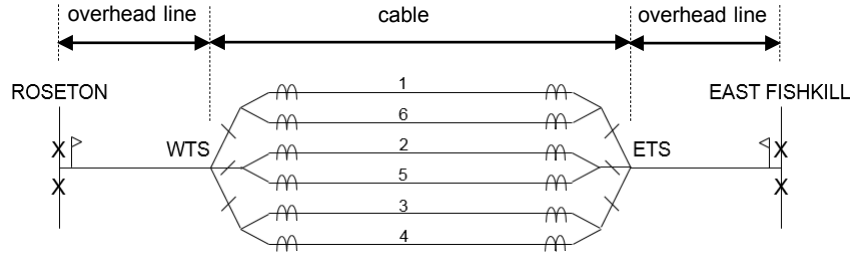
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Application overview

Roseton – East Fishkill 345kV line

- Under river (Hudson River) section WTS – ETS (1.3 mile)
 - Six 3-phase HPOF cables (pipes)

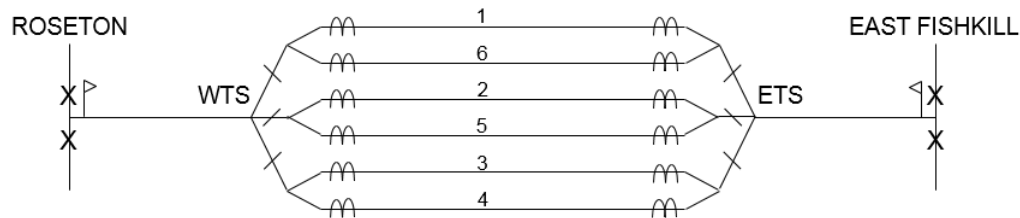


- Cable differential protection, required to...
 - detect cable fault
 - identify actual faulted cable (pipe)
 - at WTS-side, operate LORs to send DTT to Roseton to LO autoreclosing for a fault on the cable portion

Application overview

Situation prior to upgrade

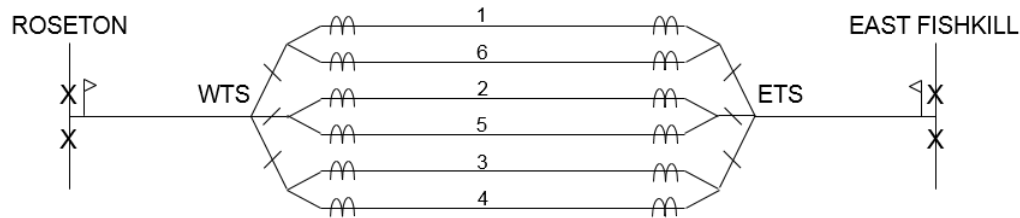
- 18 obsolete solid state differential relays, all located at WTS
 - parts becoming an increasing problem
- To get ETS currents to WTS, used small gauge copper wires installed with the main conductors
- impedance matching transformers were required at ETS to ‘boost’ the strength of the transmitted current signals from ETS to WTS (impedance matching transformers: increased signs of degradation, replacements not readily available, would require a custom build)



Application overview

Requirements for upgrade

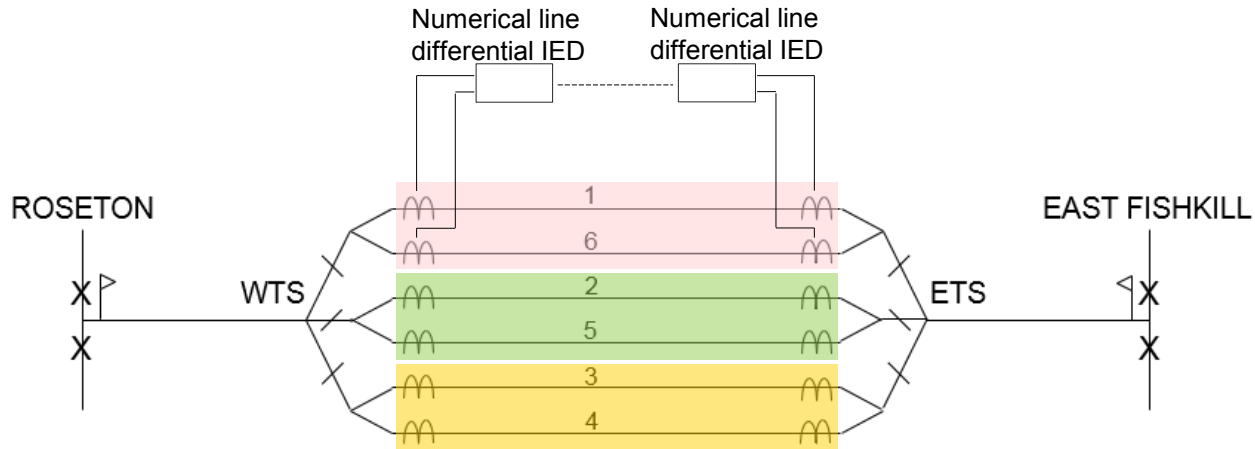
- Utilize the existing infrastructure, i.e. no fiber to be installed, so need to use the existing CT circuit copper wires as WTS – ETS inter-IED communications interface
- Do away with the impedance matching transformers - must not be required
- Utilize WTS LORs (lockout relays) and existing DTT (direct transfer trip) equipment and infrastructure
- Identify the faulted phase/s, as well as the actual faulted cable (pipe)



Application overview

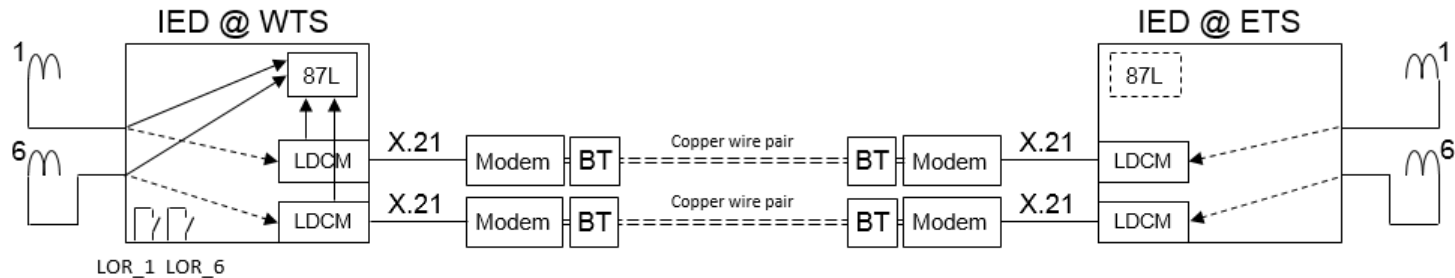
New solution

- Install modern numerical line differential IEDs at WTS and ETS
- Optimum solution – 6 IEDs, 2 IEDs per pipe pair

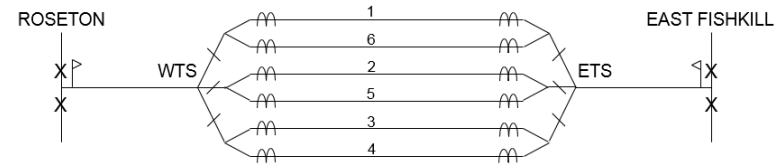


Application overview

87L for pipes 1 and 6



- LDCM (Line Data Communications Module), with X.21 output
- Modem (with X.21 plug-in module) to interconnect the line differential IEDs using the copper wires
- BT insulating barrier transformer



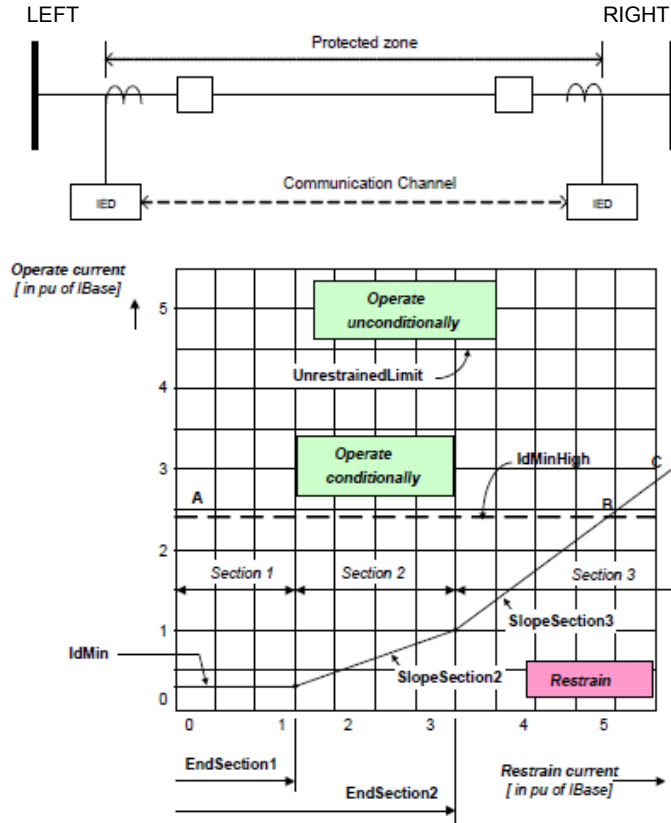
Verification of copper wire usability as communications interface

Measurements made for line attenuation and signal-to-noise (checking purity of the copper)

Result:

Existing copper wires OK to use as communications interface

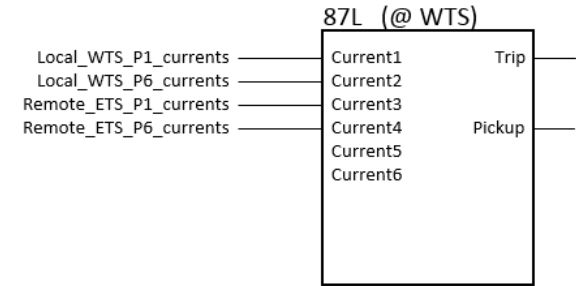
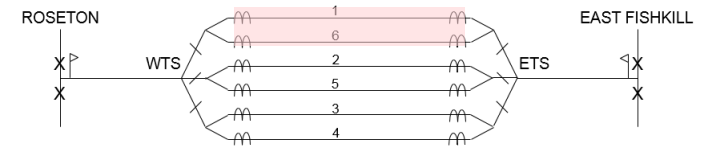
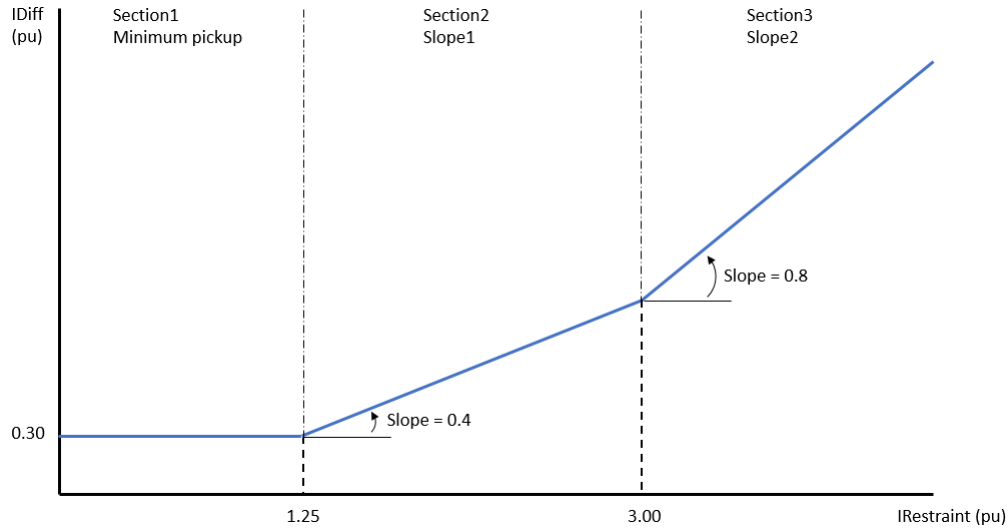
87L – overview



- Operate/Restraining characteristic
 - Minimum pickup (I_{dMin}) + one or more slopes
 - Operate area above the characteristic
 - Operate current (Y-axis value)
 - $I_{Op_A} = I_{Diff_A} = I_{L_A} + I_{R_A}$
 - Similarly for phases B and C
 - Restraining current (X-axis value)
 - Different methods
 - This application
 - $I_{Res} = \text{MAX}(|I_{L_A}|, |I_{L_B}|, |I_{L_C}|, |I_{R_A}|, |I_{R_B}|, |I_{R_C}|)$,
 - common for all 3 phases

87L – this application

87L characteristic

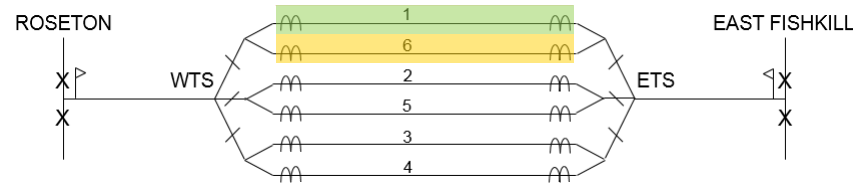


Faulted pipe identification

The 87L function will...

- operate for an internal fault in the pipe pair (1&6, 2&5, 3&4)
- indicate the faulted phase/s

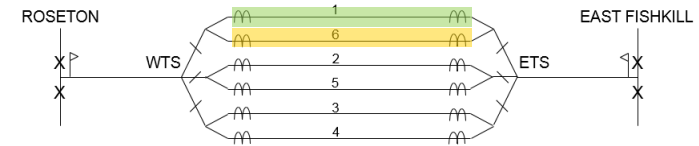
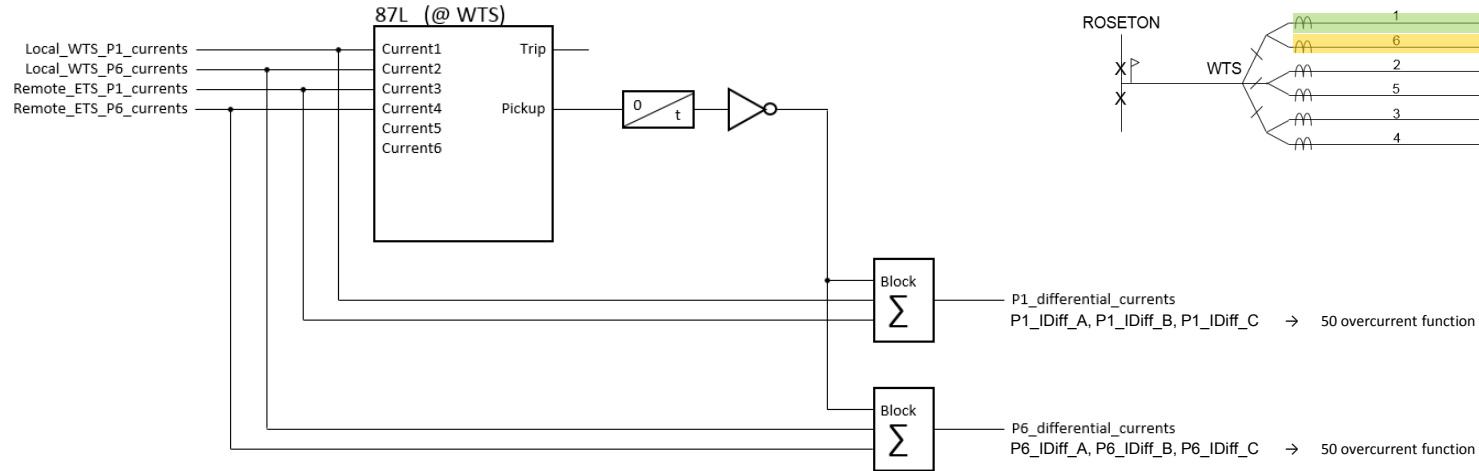
To determine the actual faulted pipe, need to establish two additional differential zones, one per pipe



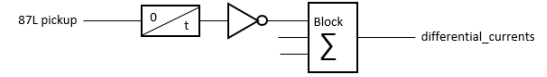
Faulted pipe identification

Pipe differential zone

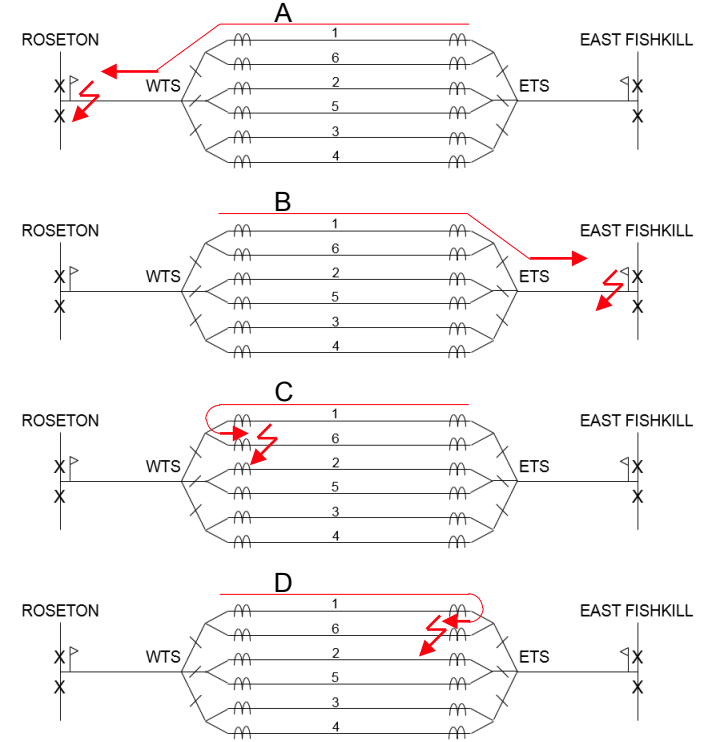
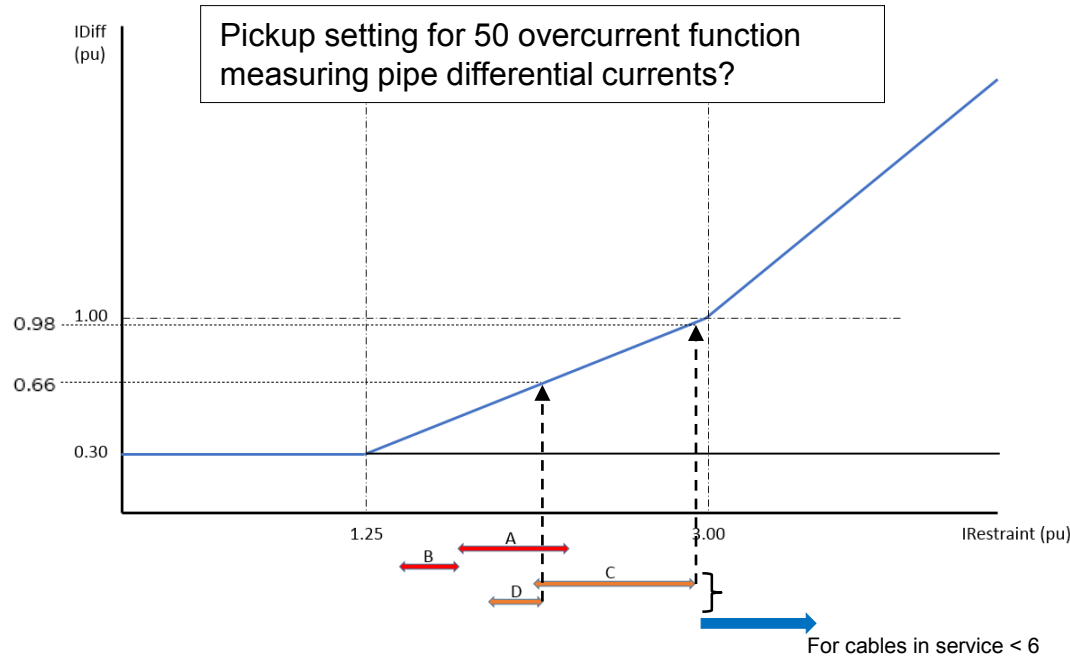
- Sum WTS + ETS currents, per phase, per pipe



Faulted pipe identification

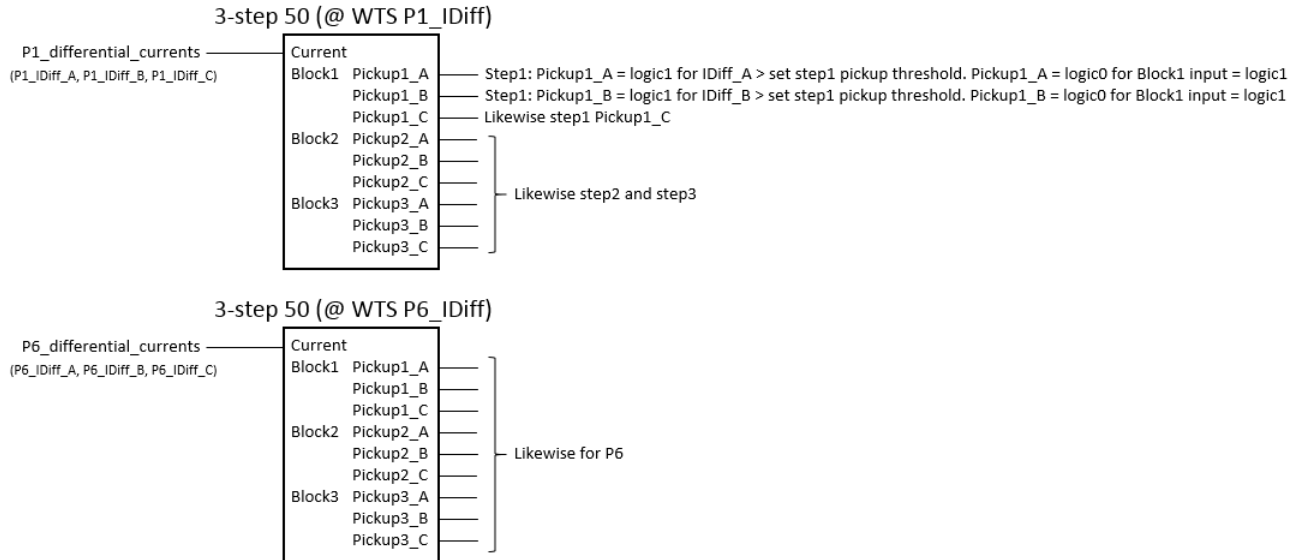


Fault levels



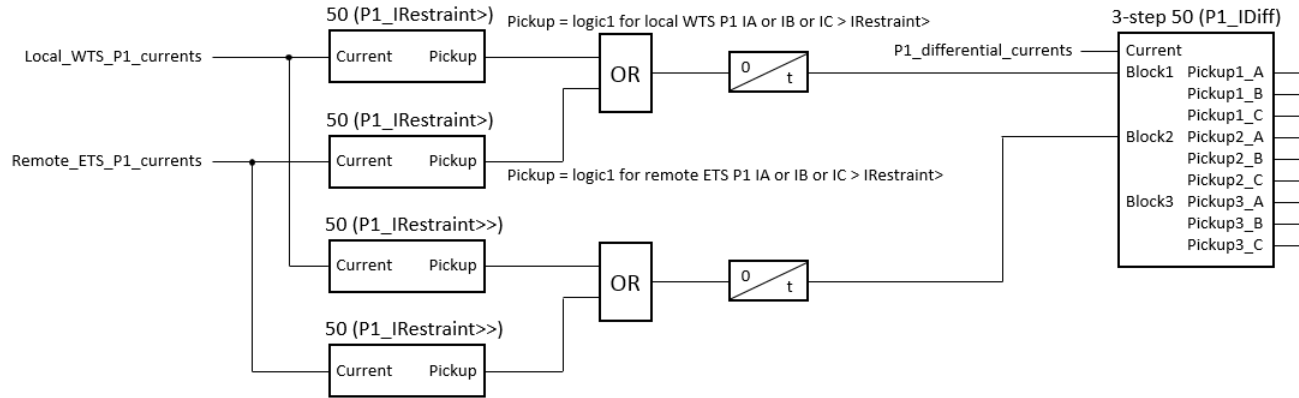
Faulted pipe identification

3-step IDiff 50 overcurrent function, per pipe



Faulted pipe identification

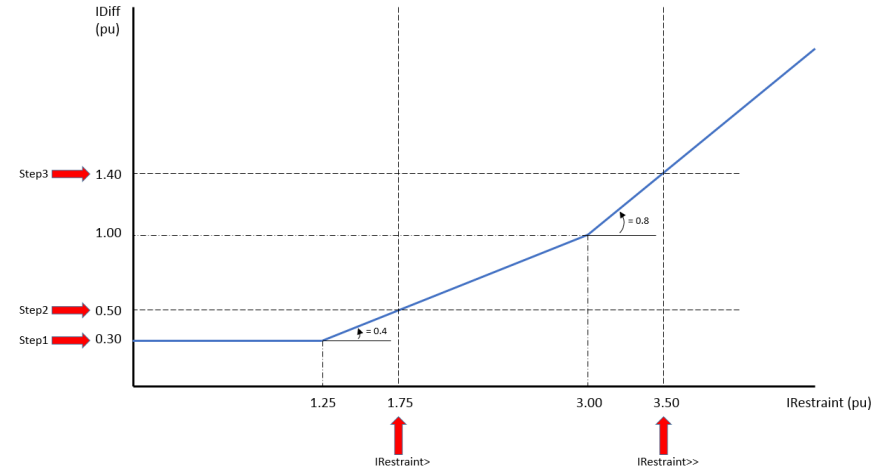
IRestrstraint 50 overcurrent functions, per pipe (shown for P1)



Faulted pipe identification

Faulted pipe identification “characteristic”

- More sensitive than 87L characteristic
- Task 1: select values for IRestr> and IRestr>>
 - IRestr>: set = 1.75 pu
 - IRestr>>: set = 3.50 pu
- Task 2: select values for 3-step IDiff 50 function
 - Step1: set = 87L minimum pickup = 0.30 pu
 - Step2: set = 87L pickup at IRestr = 1.75 pu
 - Step3: set = 87L pickup at IRestr = 3.50 pu

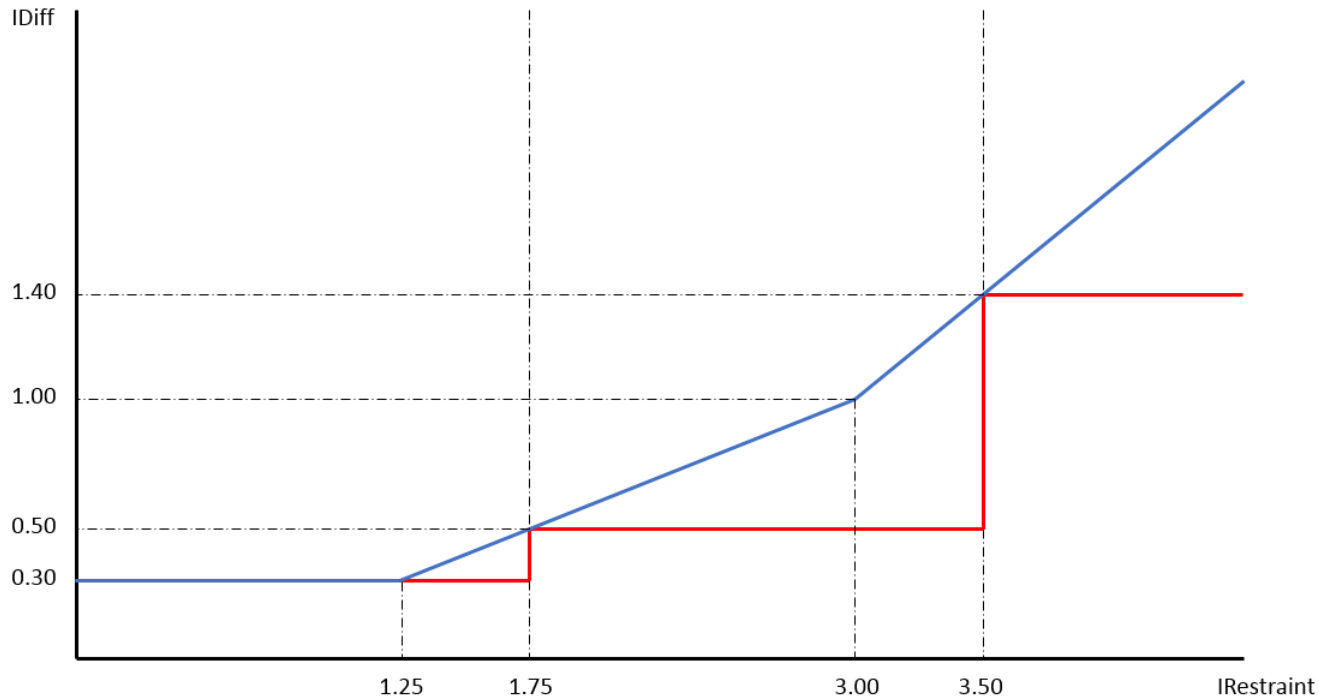


$$\text{Step2: set} = 0.30 + (0.40 \cdot (1.75 - 1.25)) = 0.50 \text{ pu}$$

$$\text{Step3: set} = 0.30 + (0.40 \cdot (3.00 - 1.25)) + (0.80 \cdot (3.50 - 3.00)) = 1.40 \text{ pu}$$

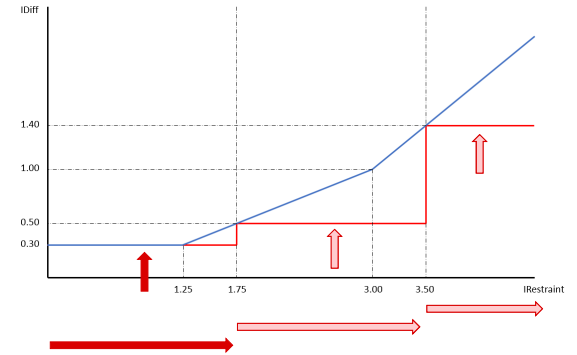
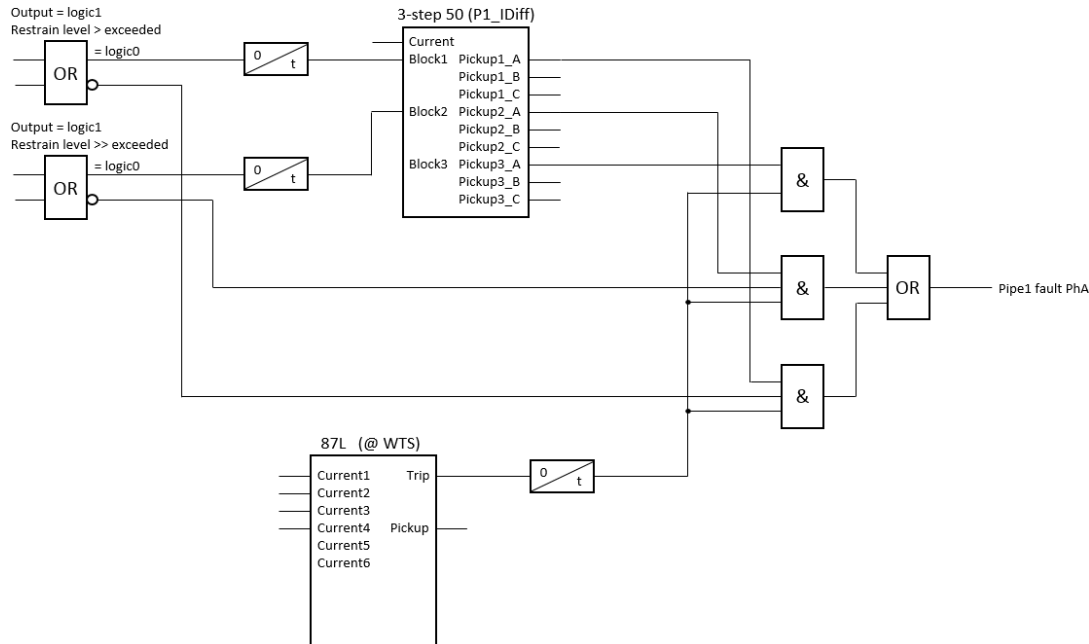
Faulted pipe identification

Faulted pipe identification “characteristic” + 87L characteristic



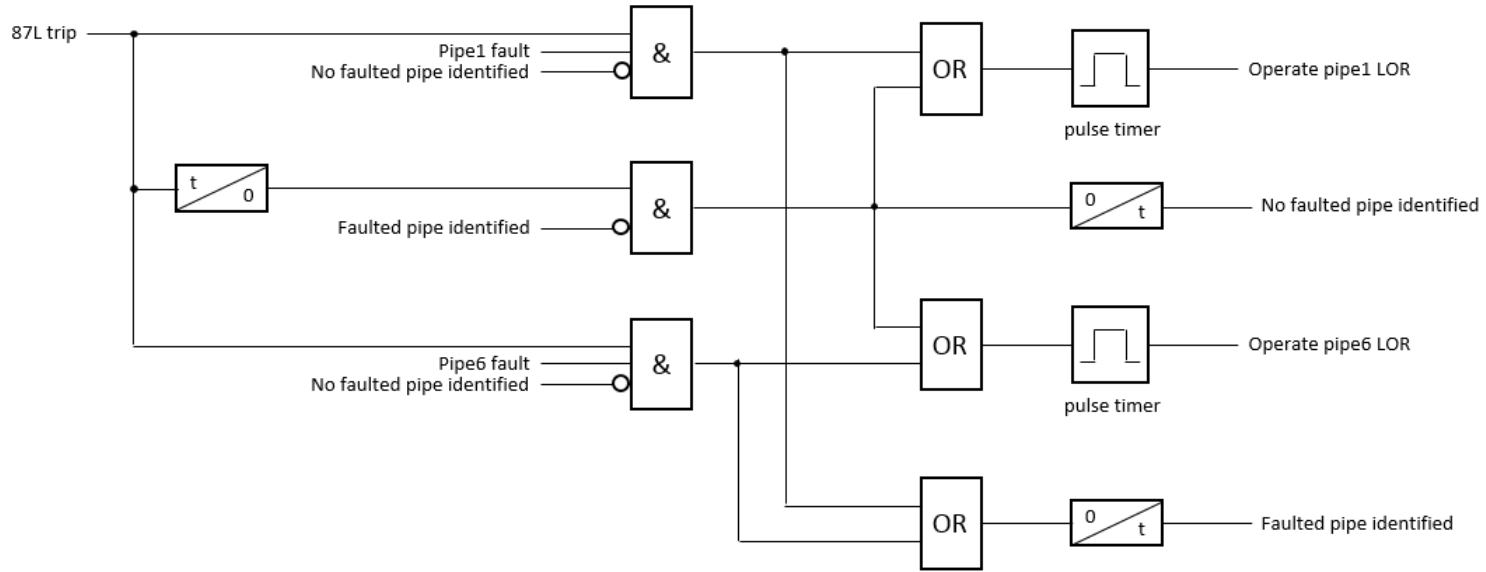
Faulted pipe identification

Faulted pipe identification, per phase



Faulted pipe identification

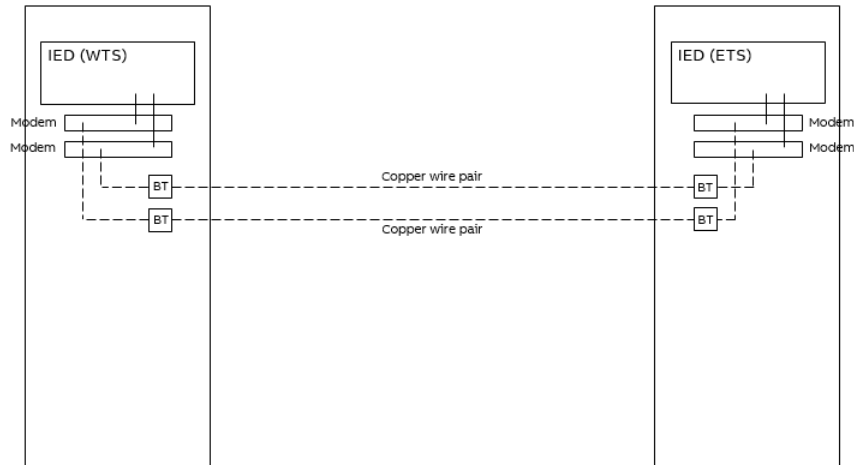
LOR relay operation



Evaluation Testing (FAT)

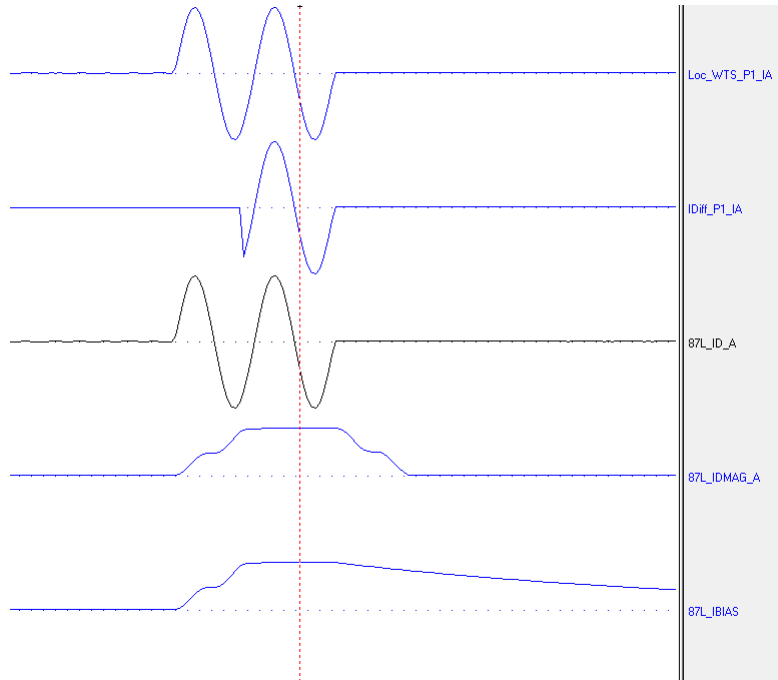
Complete assembly of both IED panels, including the communications interconnections

- Also served as a 'dry-run' for the on-site commissioning



Evaluation Testing (FAT)

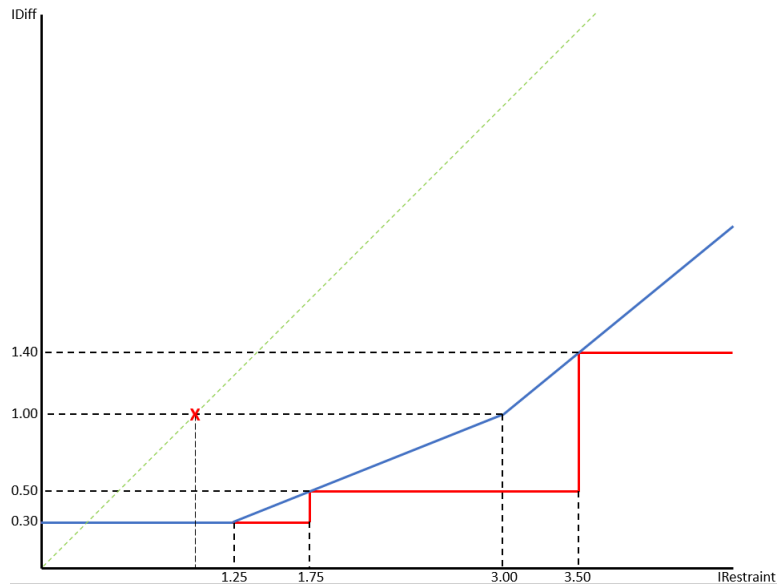
Single ended, cont.



- 5.00A (= 1 pu) phase A injection at WTS IED
 - $Loc_WTS_P1_IA$ = injected current
 - $IDiff_P1_IA = Loc_WTS_P1_IA + Rem_ETS_P1_IA$
- Output from Σ
 - released on 87L pickup
 - connected to the P1 pipe identification 3-step IDiff 50 overcurrent function

Evaluation Testing (FAT)

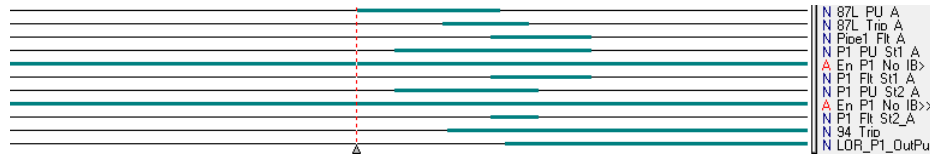
Single ended, cont.



- 5.00A (= 1 pu) phase A injection at WTS IED
 - No Restraint level exceeded
 - No steps of the 3-step IDiff 50 overcurrent function are blocked
 - IDiff 50 overcurrent function
 - P1 differential current > step1 and step2, but < step3

Evaluation Testing (FAT)

Single ended, cont.

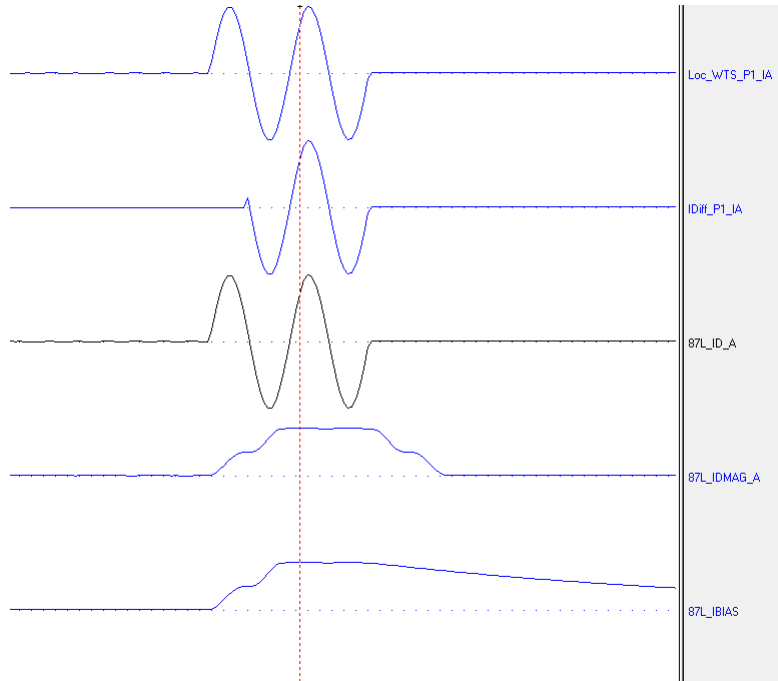


– 5.00A (= 1 pu) phase A injection at WTS IED

- 87L pickup and trip, phase A
- P1 fault identified, phase A
- Restrain level > (IB>) not exceeded
- IDiff 50 function pickup step1 phase A
- Restrain level >> (IB>>) not exceeded
- IDiff 50 function pickup step2 phase A
- Operate P1 LOR

Evaluation Testing (FAT)

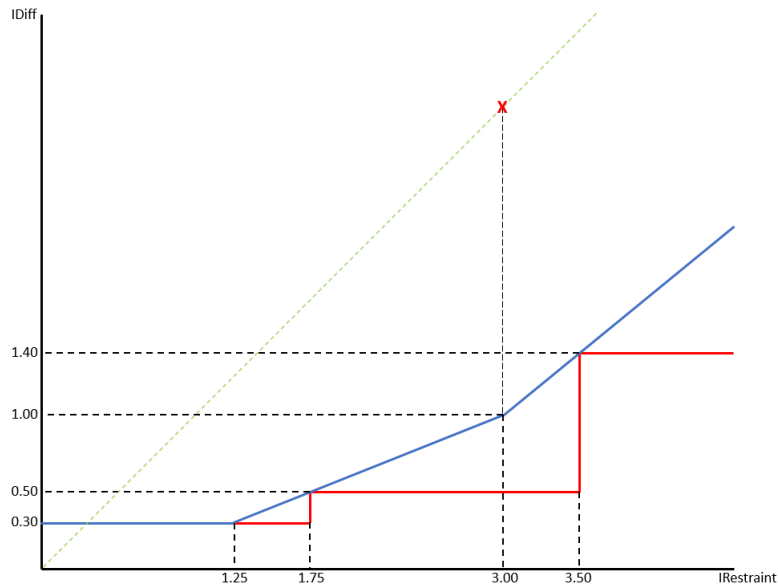
Single ended, cont.



- 15.00A (= 3 pu) phase A injection at WTS IED
 - $Loc_WTS_P1_IA$ = injected current
 - $IDiff_P1_IA = Loc_WTS_P1_IA + Rem_ETS_P1_IA$
- Output from Σ
 - released on 87L pickup
 - connected to the P1 pipe identification 3-step IDiff 50 overcurrent function

Evaluation Testing (FAT)

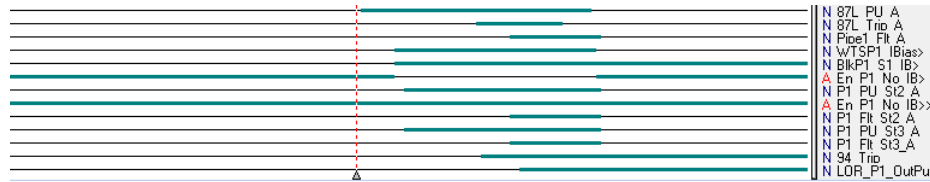
Single ended, cont.



- 15.00A (= 3 pu) phase A injection at WTS IED
 - Restraint level $I_{Restraint}$ is exceeded, but not $I_{Restraint} >$
 - Step1 of the 3-step $I_{Diff} 50$ overcurrent function will be blocked
 - $I_{Diff} 50$ overcurrent function
 - P1 differential current $>$ all steps, but step1 is blocked

Evaluation Testing (FAT)

Single ended, cont.



– 15.00A (= 3 pu) phase A injection at WTS IED

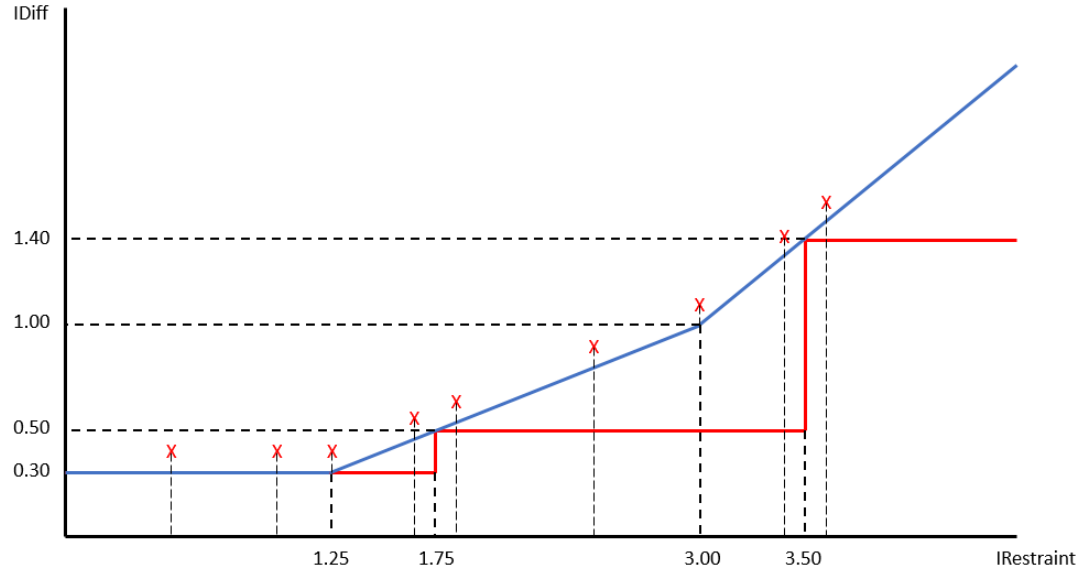
- 87L pickup and trip, phase A
- P1 fault identified, phase A
- Restrain level > (IB>) exceeded
- Restrain level >> (IB>>) not exceeded
- IDiff 50 function pickup step2 phase A
- IDiff 50 function pickup step3 phase A
- Operate P1 LOR

Evaluation Testing (FAT)

Inject @ WTS IED				Inject @ ETS IED			
2.50	∠0°	300	~	2.50	∠180°	300	~
2.50	∠0°	2.0	~	0.50	∠180°	2.0	~
5.00	∠0°	300	~	5.00	∠180°	300	~
5.00	∠0°	2.0	~	3.00	∠180°	2.0	~
6.25	∠0°	300	~	6.25	∠180°	300	~
6.25	∠0°	2.0	~	4.25	∠180°	2.0	~
8.25	∠0°	300	~	8.25	∠180°	300	~
8.25	∠0°	2.0	~	5.45	∠180°	2.0	~
9.25	∠0°	300	~	9.25	∠180°	300	~
9.25	∠0°	2.0	~	6.05	∠180°	2.0	~
12.50	∠0°	300	~	12.50	∠180°	300	~
12.50	∠0°	2.0	~	8.00	∠180°	2.0	~
15.00	∠0°	300	~	15.00	∠180°	300	~
15.00	∠0°	2.0	~	9.50	∠180°	2.0	~
17.00	∠0°	300	~	17.00	∠180°	300	~
17.00	∠0°	2.0	~	9.90	∠180°	2.0	~
18.00	∠0°	300	~	18.00	∠180°	300	~
18.00	∠0°	2.0	~	10.10	∠180°	2.0	~

Double ended, 2 stage injection

- stage1, balanced through current
- stage2, reduce one side by a pre-determined amount



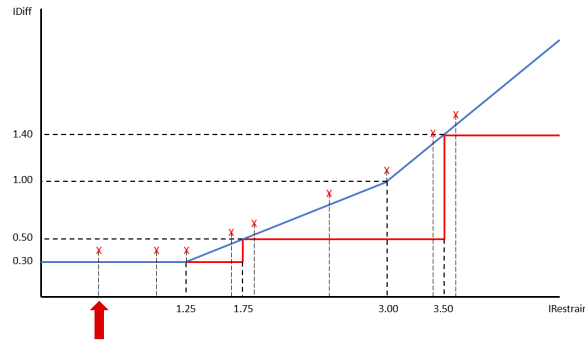
Evaluation Testing (FAT)

Double ended, 2 stage injection

–At IRestraint (X-axis) = 2.50A = 0.50 pu, IDiff (Y-axis) value for pickup = 0.30 pu

–Add margin of 0.10 pu → 0.40 pu = 2.00A

Inject @ WTS IED				Inject @ ETS IED			
2.50	∠0°	300	~	2.50	∠180°	300	~
2.50	∠0°	2.0	~	0.50	∠180°	2.0	~
5.00	∠0°	300	~	5.00	∠180°	300	~
5.00	∠0°	2.0	~	3.00	∠180°	2.0	~
6.25	∠0°	300	~	6.25	∠180°	300	~
6.25	∠0°	2.0	~	4.25	∠180°	2.0	~
8.25	∠0°	300	~	8.25	∠180°	300	~
8.25	∠0°	2.0	~	5.45	∠180°	2.0	~
9.25	∠0°	300	~	9.25	∠180°	300	~
9.25	∠0°	2.0	~	6.05	∠180°	2.0	~
12.50	∠0°	300	~	12.50	∠180°	300	~
12.50	∠0°	2.0	~	8.00	∠180°	2.0	~
15.00	∠0°	300	~	15.00	∠180°	300	~
15.00	∠0°	2.0	~	9.50	∠180°	2.0	~
17.00	∠0°	300	~	17.00	∠180°	300	~
17.00	∠0°	2.0	~	9.90	∠180°	2.0	~
18.00	∠0°	300	~	18.00	∠180°	300	~
18.00	∠0°	2.0	~	10.10	∠180°	2.0	~



- Stage2, keep one current (WTS) unchanged (= 2.50A), and drop the other (ETS) by 2.00A to 0.50A
- X-axis point remains unchanged, and Y-axis point jumps to 0.40 pu

- Expected result: P1 fault identified, phase A
- No restraint level exceeded, no IDiff 50 overcurrent function steps blocked, only step1 pickup phase A

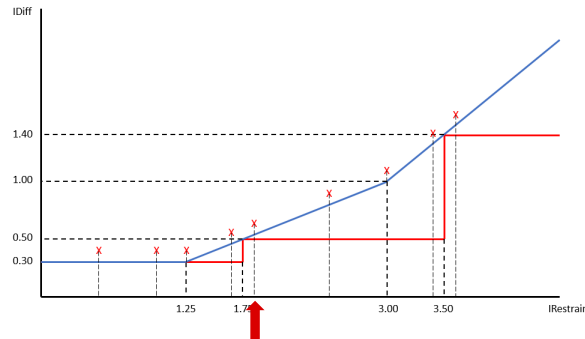
Evaluation Testing (FAT)

Double ended, 2 stage injection

–At IRestraint (X-axis) = $9.25A = 1.85 \text{ pu}$, IDiff (Y-axis) value for pickup = 0.54 pu

–Add margin of $0.10 \text{ pu} \rightarrow 0.64 \text{ pu} = 3.20A$

Inject @ WTS IED				Inject @ ETS IED			
2.50	∠0°	300	~	2.50	∠180°	300	~
2.50	∠0°	2.0	~	0.50	∠180°	2.0	~
5.00	∠0°	300	~	5.00	∠180°	300	~
5.00	∠0°	2.0	~	3.00	∠180°	2.0	~
6.25	∠0°	300	~	6.25	∠180°	300	~
6.25	∠0°	2.0	~	4.25	∠180°	2.0	~
8.25	∠0°	300	~	8.25	∠180°	300	~
8.25	∠0°	2.0	~	5.45	∠180°	2.0	~
9.25	∠0°	300	~	9.25	∠180°	300	~
9.25	∠0°	2.0	~	6.05	∠180°	2.0	~
12.50	∠0°	300	~	12.50	∠180°	300	~
12.50	∠0°	2.0	~	8.00	∠180°	2.0	~
15.00	∠0°	300	~	15.00	∠180°	300	~
15.00	∠0°	2.0	~	9.50	∠180°	2.0	~
17.00	∠0°	300	~	17.00	∠180°	300	~
17.00	∠0°	2.0	~	9.90	∠180°	2.0	~
18.00	∠0°	300	~	18.00	∠180°	300	~
18.00	∠0°	2.0	~	10.10	∠180°	2.0	~



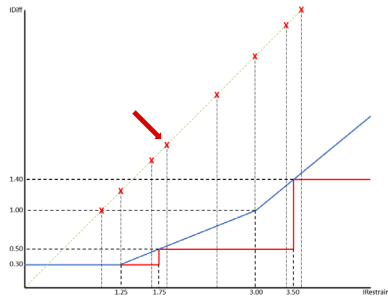
- Stage2, keep one current (WTS) unchanged (= $9.25A$), and drop the other (ETS) by $3.20A$ to $6.05A$
- X-axis point remains unchanged, and Y-axis point jumps to 0.64 pu

- Expected result: P1 fault identified, phase A
- Restraint level ($>$) exceeded, step1 of IDiff 50 overcurrent function blocked, only step2 pickup phase A

Conclusion

FAT

- Successful – ‘expected’ operation for all test cases



- E.G. for test indicated

- IDiff = 1.85 pu >> pickup setting = 0.30 pu (step1)
- IRestrict = 1.85 pu just > pickup setting = 1.75 pu (IRestrict>)
- IDiff step1 operated faster than IRestrict>, picking up momentarily before being blocked by IRestrict> pickup
- OK for increased margin between IRestrict and pickup setting
- ‘Gray’ area around the transition point

Commissioning

- Put into service 12 May 2017
- All equipment, including the communications, has to date performed as expected