

Fast Fault Detection Challenge for Alienation Coefficient Based Bus Fault Discriminator

Presented in:
71st Annual Conference for Relay Engineers

Monir Hossain
PhD Candidate

Dr. Ittiphong Leevongwat
Associate Professor

Dr. Parviz Rastgoufard
Professor

Dept. of Electrical and Engineering
University of New Orleans

CONTENT

- *Problem Statement*
- *Fault Discrimination by Alienation Coefficient*
- *Issues Identified with Present Method*
- *Proposed Method*
- *Performance Validation*
- *Concluding Remarks*
- *References*

PROBLEM STATEMENT

- *One of the key challenges for bus differential protection is to prevent mis-operation due to CT saturation during close-in external faults.*
- *Various techniques have been used to supervise traditional bus differential characteristics in order to solve this challenge:*



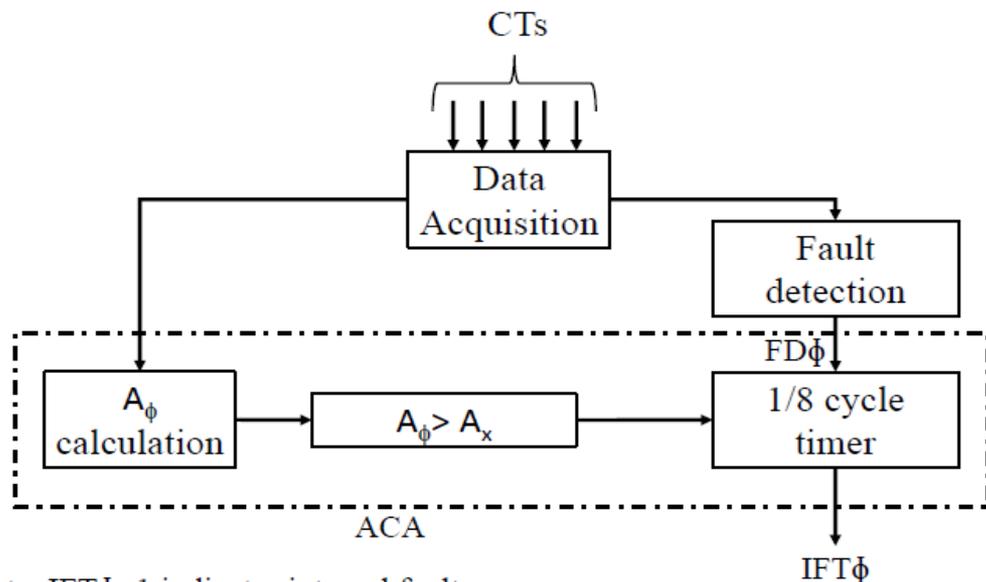
- *Logical follow-up to block trip during CT saturation*
- *It blocks internal faults if CT saturates!*
- *Directional supervision*
- *It blocks high impedance internal faults as load current continue to flow!*
- *Supervision based on change of system parameters (differential current, restraint current)*
- *Mis-trip during fast CT saturation!*

PROBLEM STATEMENT

- *ACA: Use of alienation coefficient of two current signals from two-terminal equivalent busbar configuration to discriminate internal and external faults.*
- ***Delayed detection of fault inception results mis-trip during external faults.***
- *This paper presents:*
 - *The performance evaluation of ACA for currently used fault detection technique.*
 - *An alternative fault detection technique.*
 - *Performance validation for modified fault discriminator.*



Fault Discrimination by Alienation Coefficient



Note: $IFT_\phi=1$ indicates internal fault

$$r_\Phi = \left(\sum_{n=1}^m i_{\Phi E1} i_{\Phi E2} - (1/m) \sum_{n=1}^m i_{\Phi E1} \sum_{n=1}^m i_{\Phi E2} \right) / \sqrt{\left(\sum_{n=1}^m i_{\Phi E1}^2 - (1/m) \left(\sum_{n=1}^m i_{\Phi E1} \right)^2 \right) \left(\sum_{n=1}^m i_{\Phi E2}^2 - (1/m) \left(\sum_{n=1}^m i_{\Phi E2} \right)^2 \right)}$$

$$A_\Phi = 1 - (r_\Phi)^2$$

- A_ϕ becomes high instantaneously with the inception of internal fault.
- A_ϕ becomes high after 1/8 cycle of fault inception in case of external faults.

Important: Detection of fault (fault inception) instantaneously if possible

Issues Identified with Present Method

What?

- *Fault discriminator responds incorrectly by detecting external fault as internal fault*

Why?

- *Delayed fault detection*

When?

- *Fast CT saturation during external faults*

How?

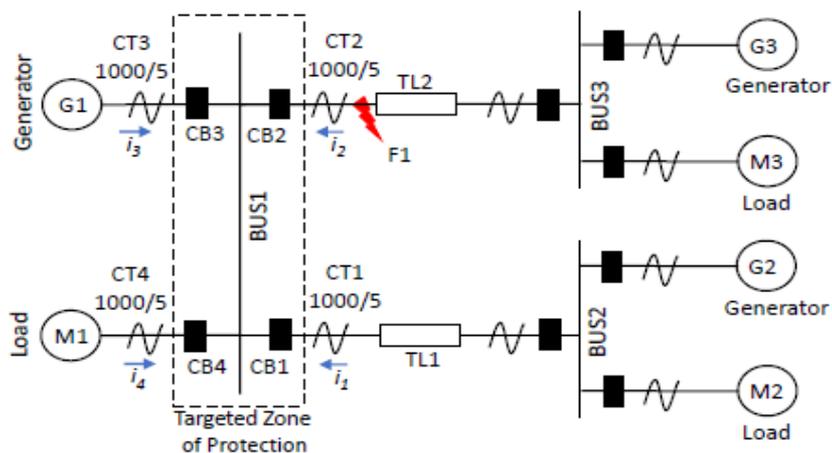
- *Time difference between fault detection and starting of CT saturation becomes less than 1/8 cycle*

Fault detection:

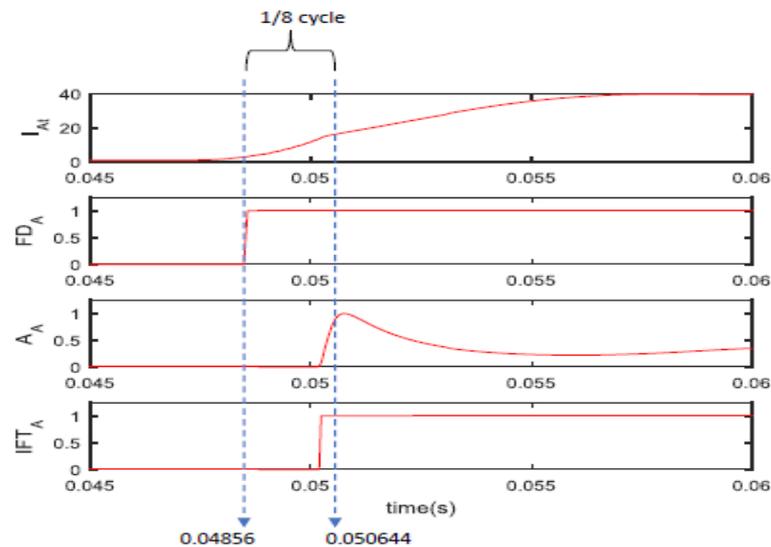
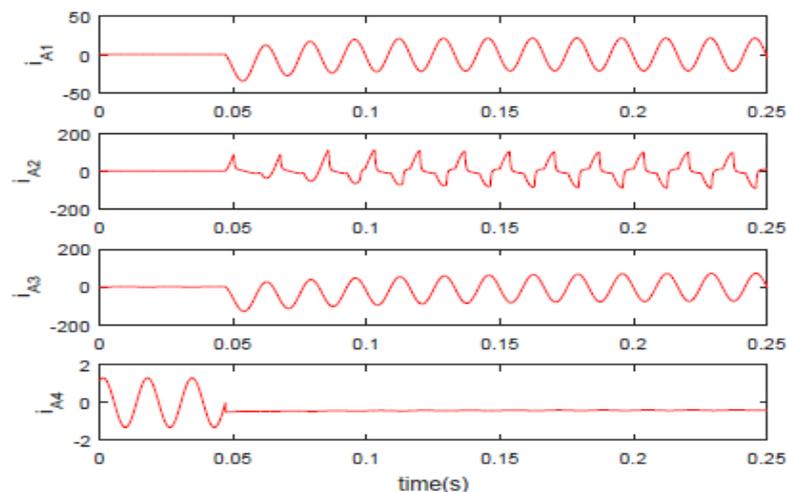
$$I_{\Phi t} = \frac{1}{2} \sum_{k=1}^n I_{\Phi k}$$

Fault: If $\Delta I_{\phi t} > 0.2I_n$

Issues Identified with Present Method



I_n is considered 2000A.



Issues Identified with Present Method

PERFORMANCE ANALYSIS WITH EXISTING FAULT DETECTOR

Fault	Location	R_f (Ω)	Time (ms)				Response of discriminator
			T1	T2	T3	T3 - T2	
AG	F1	0.1	47	48.56	50.23	1.67	Internal fault
AG	F1	5	47	48.64	50.56	1.92	Internal fault
AG	F1	10	47	48.73	50.98	2.25	External fault
AG	F1	0.1	49	50.15	51.77	1.62	Internal fault
AG	F1	5	49	50.23	52.10	1.87	Internal fault
AG	F1	10	49	50.31	52.52	2.21	External fault
ABG	F1	0.1	47	48.73	50.48	1.75	Internal fault
ABG	F1	5	47	48.81	50.77	1.96	Internal fault
ABG	F1	10	47	48.90	51.23	2.23	External fault
ABG	F1	0.1	49	50.23	51.90	1.67	Internal fault
ABG	F1	5	49	50.31	52.19	1.88	Internal fault
ABG	F1	10	49	50.40	52.60	2.20	External fault

Proposed Fault Detection Method

In steady-state:

$$i_{\Phi k}(t) = \sqrt{2}I_{\Phi km} \cos(\omega t + \theta_k)$$

$$\left| \frac{di_{\Phi k}(t)}{dt} \right| = \sqrt{2}\omega I_{\Phi km} |\sin(\omega t + \theta_k)|$$

$$|\sin(\omega t + \theta_k)|_{max} = 1.$$

$$\left| \frac{di_{\Phi k}(t)}{dt} \right|_{max} = \sqrt{2}\omega I_{\Phi km}$$

$$I_{\Phi km}(t) = I_{\Phi km}(t - T)$$

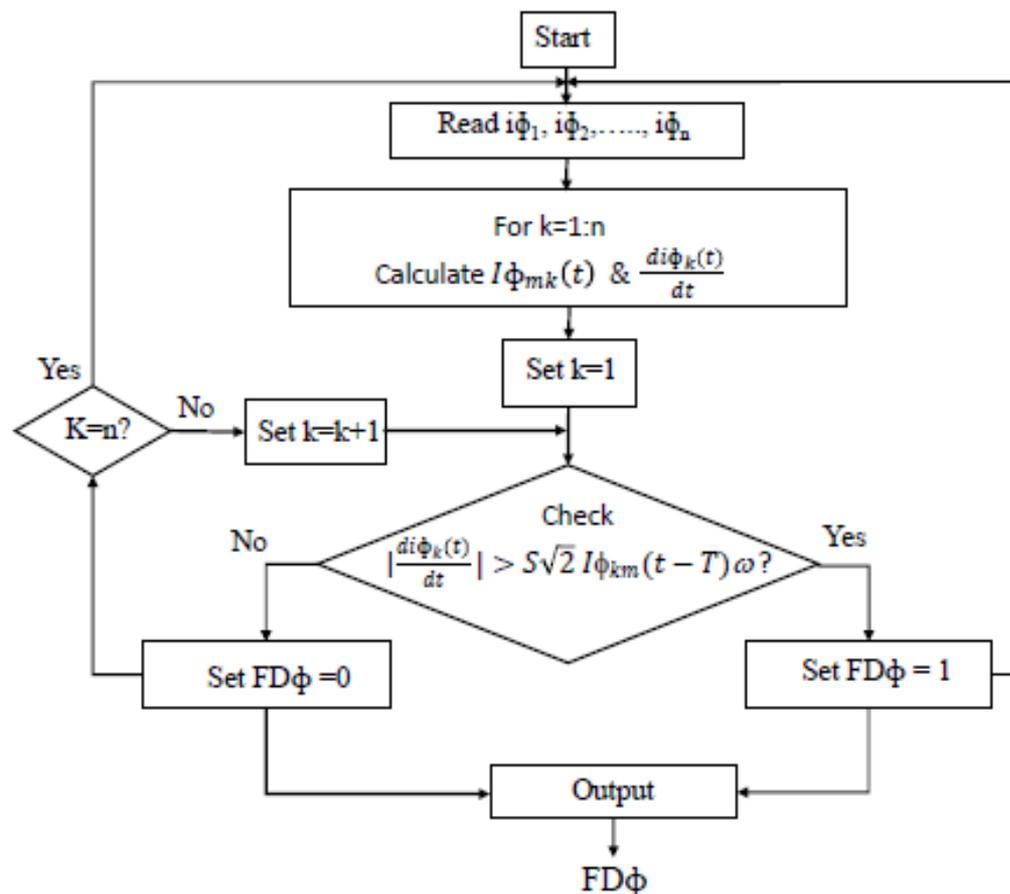
$$\left| \frac{di_{\Phi k}(t)}{dt} \right|_{max} = \sqrt{2}\omega I_{\Phi km}(t - T)$$

In transient (fault):

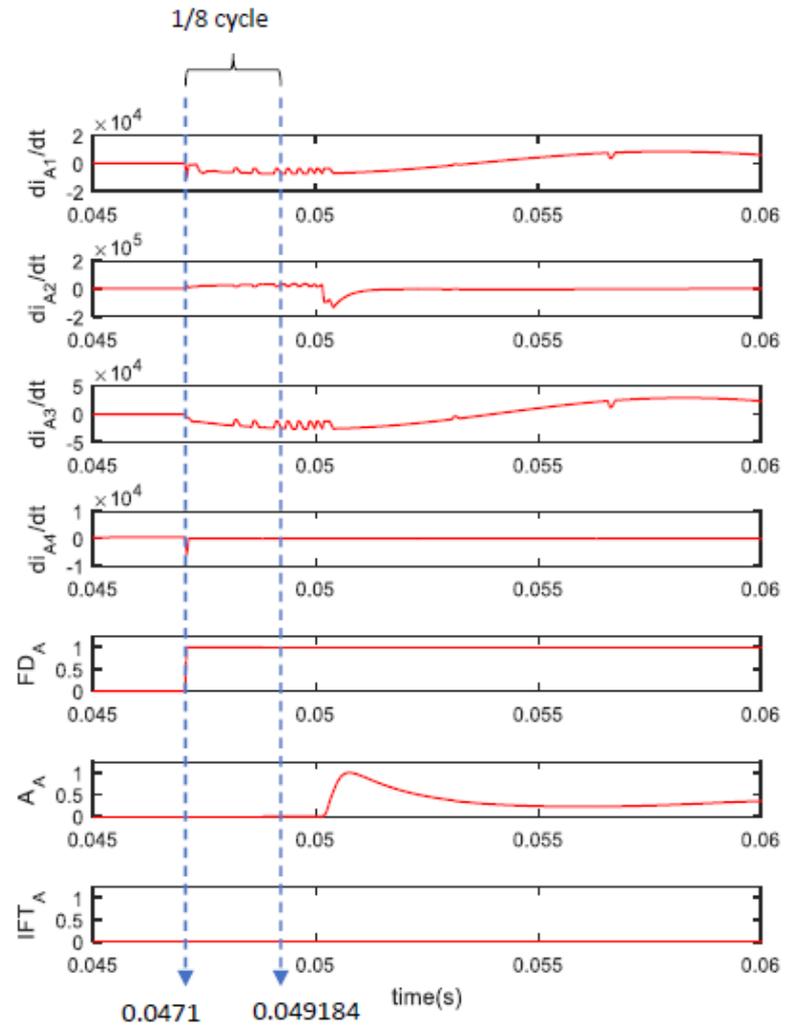
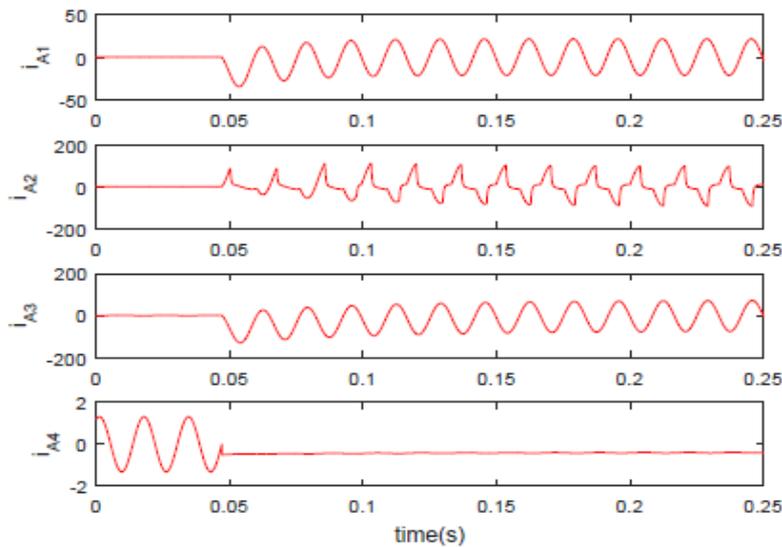
$$\left| \frac{di_{\Phi k}(t)}{dt} \right| \gg \sqrt{2}\omega I_{\Phi km}(t - T)$$

OR

$$\left| \frac{di_{\Phi k}(t)}{dt} \right| > S\sqrt{2}\omega I_{\Phi km}(t - T), S \text{ is a marginal constant}$$



Performance Validation



Performance Validation

PERFORMANCE ANALYSIS WITH PROPOSED FAULT DETECTOR

Fault	Location	R_f (Ω)	Time (ms)				Response of discriminator
			T1	T2	T3	T3 - T2	
AG	F1	0.1	47	47.10	50.23	3.13	External fault
AG	F1	5	47	47.10	50.56	3.46	External fault
AG	F1	10	47	47.10	50.98	3.88	External fault
AG	F1	0.1	49	49.11	51.77	2.66	External fault
AG	F1	5	49	49.11	52.10	2.99	External fault
AG	F1	10	49	49.11	52.52	3.41	External fault
ABG	F1	0.1	47	47.10	50.48	3.38	External fault
ABG	F1	5	47	47.10	50.77	3.67	External fault
ABG	F1	10	47	47.10	51.23	4.13	External fault
ABG	F1	0.1	49	49.11	51.90	2.79	External fault
ABG	F1	5	49	49.11	52.19	3.08	External fault
ABG	F1	10	49	49.11	52.60	3.49	External fault

Concluding Remarks

- *This paper examines the performance of alienation coefficient-based bus fault discriminator including existing fault detector by simulation study.*
- *The study suggests that existing fault detector can introduce mis-operation during external faults due to delayed fault detection.*
- *An alternative fault detection method is proposed based on the first derivative of instantaneous terminal current to overcome the aforesaid problem.*
- *The performance of the proposed fault detector is validated by simulation study.*
- *The results of the study indicate that the proposed method is able to detect fault inception almost instantaneously which addresses the risk of mis-operation of alienation coefficient-based bus fault discriminator.*

References

- [1] X. Lin and Q. Tian and M. Zhao, "Comparative analysis on current percentage differential protections using a novel reliability evaluation criterion", IEEE Trans. Power Deliv., vol. 21, no. 1, pp. 62-72, 2006
- [2] Shihong Miao and Pei Liu and Xiangning Lin, "An Adaptive Operating Characteristic to Improve the Operation Stability of Percentage Differential Protection", IEEE Trans. Power Deliv., vol. 25, no. 3, pp. 1410-1417, 2010
- [3] M. Thompson, "Percentage restrained differential, percentage of what?", 64th Annual Conference for Protective Relay Engineers, College Station, USA, pp. 278-289, 2011.
- [4] L.F. Kennedy and C.D. Hayward, "Harmonic-current-restrained relays for differential protection," AIEE Trans., vol. 57, no. 5, pp. 262-266, 1938.
- [5] H.S. Gill, T.S. Sidhu, M.S. Sachdev, "Microprocessor-based busbar protection system," IEE Proc. Gener. Transm. Distrib., vol. 147, no. 4, pp. 252-260, 2000.
- [6] S.A. Gafoor, N.R. Devi, P.V.R. Rao, "A transient current based bus zone protection scheme using wavelet transform," IEEE Conference on Sustainable Energy Technologies, Singapore, Singapore, pp. 1195-1199, November 2008.
- [7] B. Kasztenny, G. Brunello and L. Sevov, "Digital low impedance bus differential protection with reduced requirements for CTs," IEEE Transmission and distribution conference and exposition, Atlanta, USA, pp 703-708, November 2001.
- [8] Krish Narendra and Dave Fedirchuk, "Secured busbar differential protection using a computationally efficient dot product technique," Power System Protection and Automation Conference, New Delhi, India, Dec. 2010.
- [9] K. Narendra, D. Fedirchuk, N. Zhang and *et al*, "Phase angle comparison and differential rate of change methods used for differential protection of busbars and transformers," IEEE Electrical Power and Energy Conference, Oct. 2011.
- [10] K. Narendra, D. Fedirchuk and N. Zhang, "Differential rate of change method for busbar protection," US Patent 20120182657A1, 2012.
- [11] M. Hossain, I. Leevongwat, P. Rastgoufard, "Comparative analysis of fault discrimination algorithms on sensitivity to high impedance busbar faults", North American Power Symposium (NAPS), Morgantown, West Virginia, USA, pp. 1-6, 2017.
- [12] M. Hossain, I. Leevongwat and P. Rastgoufard, "Partial operating current characteristics to discriminate internal and external faults of differential protection zone", IET Generation, Transmission and Distribution, vol. 12, no. 2, pp. 379-387, 2018.
- [13] M. Hossain, I. Leevongwat and P. Rastgoufard, "Design and testing of a bus differential protection scheme using partial operating current (POC) algorithm", Elsevier Electric Power Systems Research, vol. 157, pp. 29-38, 2018.
- [14] R. Abd Allah, "Busbar protection scheme based on alienation coefficients for current signals," IJEAT, vol. 3, no. 3, pp. 103-115, April 2014.
- [15] R. Abd Allah, "Experimental results and technique evaluation based on alienation coefficients for busbar protection scheme," Elsevier Int. J. Electr. Power Energy Syst., vol. 73, pp. 943954, 2015.
- [16] R. Abd Allah, "Adaptive busbar differential relaying scheme during saturation period of current transformers based on alienation concept," IET Generation, Transmission and Distribution, vol. 10, no. 15, pp. 3803-3815, 2016.
- [17] M. Hossain, L. Mittal and P. Rastgoufard, "A dynamic current allocation algorithm for alienation coefficient based busbar fault discrimination", 19th International Conference on Intelligent System Application to Power Systems (ISAP), San Antonio, Texas, USA, pp. 1-6, 2017.

Fast Fault Detection Challenge for Alienation Coefficient Based Bus Fault Discriminator



THANK YOU! 😊