

Distance Protection: Why Have We Started With a Circle, Does It Matter, and What Else Is Out There?

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What Is a Distance Protection Element?

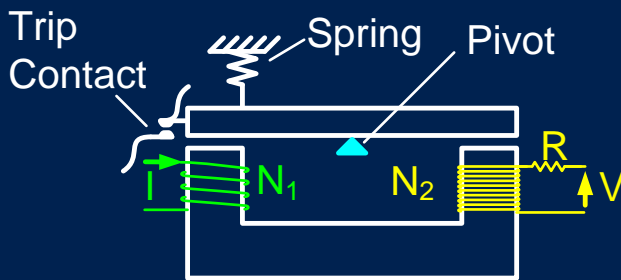


- Uses local voltage and current only
- Responds to faults within a predetermined reach
- Operates independently of fault current level, pre-fault load, fault type, or fault resistance

Distance Element Applications

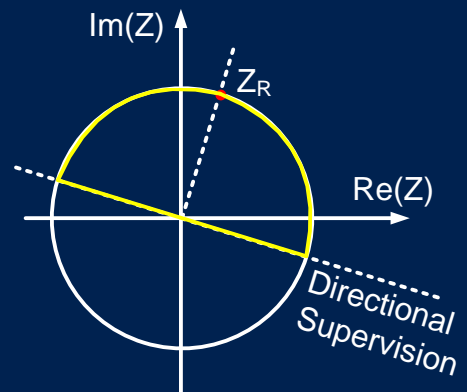
- Line protection without a pilot channel
 - Underreaching element (Zone 1)
 - Stepped distance (time coordinated)
- Directional comparison schemes
- Applications that require impedance elements
 - Out-of-step, power swing, loss of excitation

Why Did We Start With a Circle?

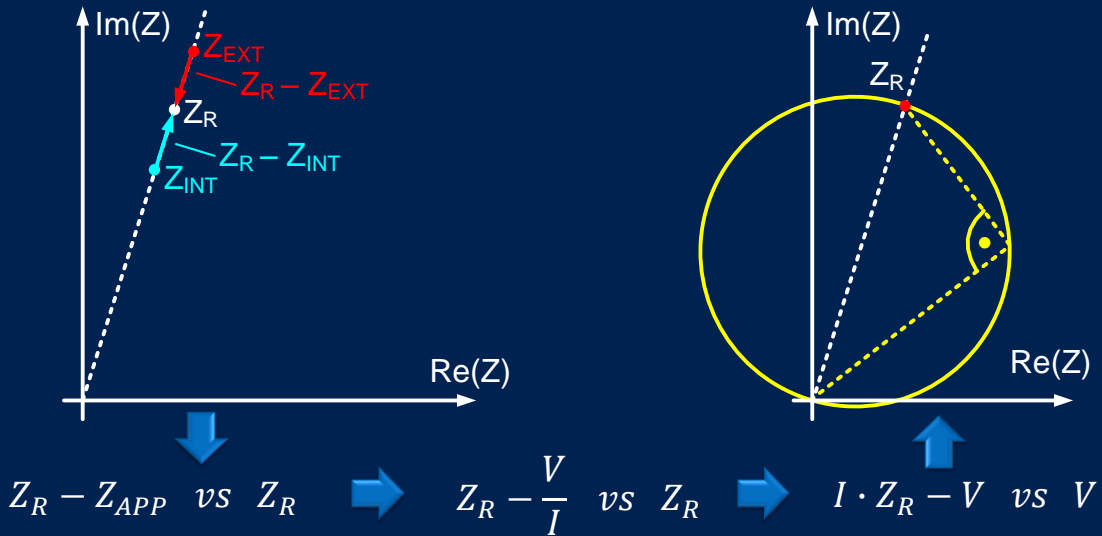


$$N_1 \cdot |I| > \frac{|V|}{R} \cdot N_2 \quad \Rightarrow \quad \frac{|V|}{|I|} < |Z_R|$$

$$|Z_R| = R \cdot \frac{N_1}{N_2}$$



Innovation and Progress Directional Mho Characteristic



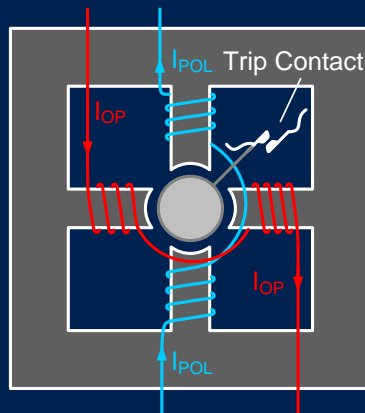
Implementation With a Cylinder-Unit Relay

$$\angle(S_{OP}, S_{POL}) < \pm 90^\circ$$

$$S_{POL} = V$$

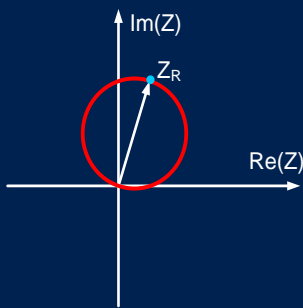
$$S_{OP} = I \cdot Z_R - V$$

Replica Current



Shaping Distance Characteristics Using Phase Comparators

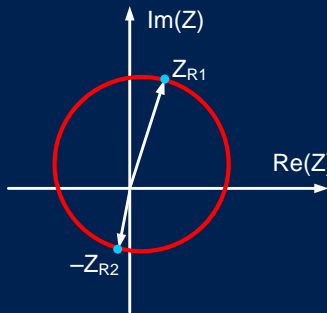
Directional Mho



$$S_{OP} = I \cdot Z_R - V$$

$$S_{POL} = V$$

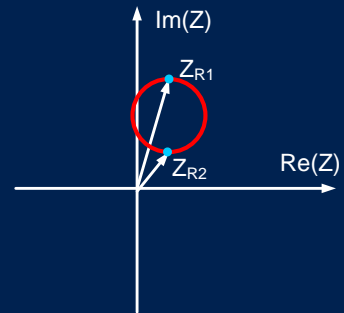
Reverse Offset Mho



$$S_{OP} = I \cdot Z_{R1} - V$$

$$S_{POL} = -(I \cdot Z_{R2} + V)$$

Forward Offset Mho

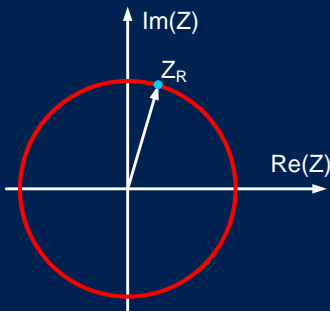


$$S_{OP} = I \cdot Z_{R1} - V$$

$$S_{POL} = I \cdot Z_{R2} - V$$

Shaping Distance Characteristics Using Phase Comparators

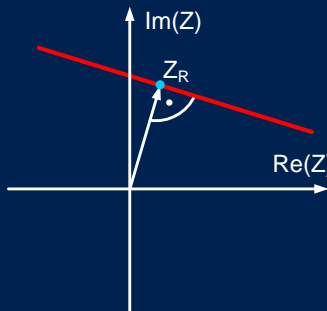
Nondirectional Mho



$$S_{OP} = I \cdot Z_R - V$$

$$S_{POL} = -(I \cdot Z_R + V)$$

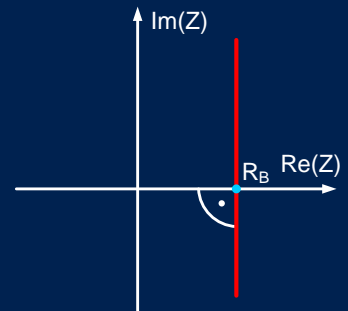
Reactance



$$S_{OP} = I \cdot Z_R - V$$

$$S_{POL} = I \cdot Z_R$$

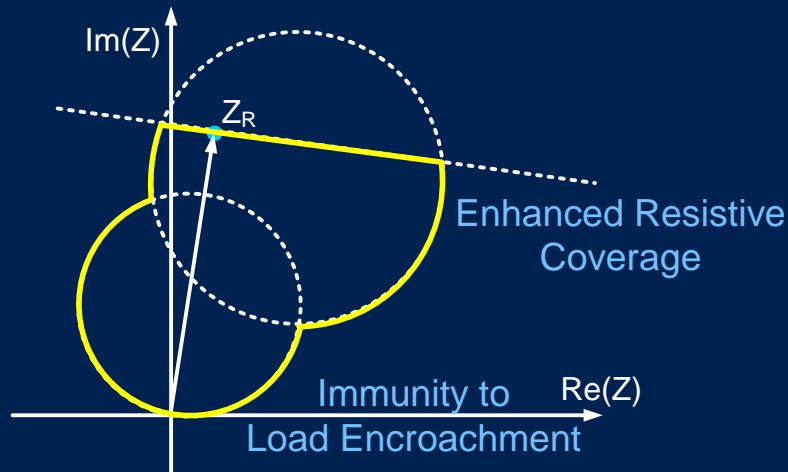
Resistive Blinder



$$S_{OP} = I \cdot R_B - V$$

$$S_{POL} = I \cdot R_B$$

Shaping Complex Characteristics



Need for Speed, 1969

A.R. van C. Warrington

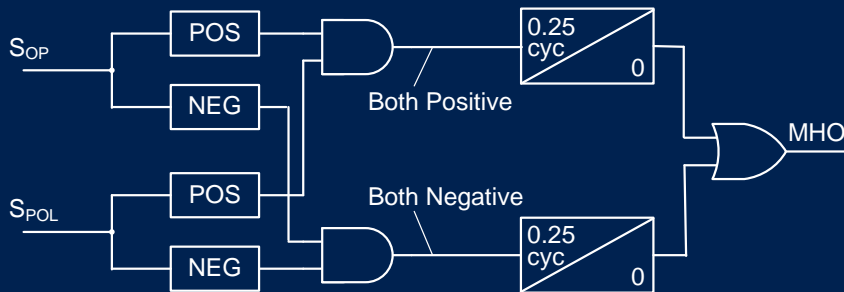
Protective Relays Their Theory and Practice: Vol. 2:

“Faults on E.H.V. links must be cleared as fast as possible to prevent instability on the H.V. system. Modern relays can trip in less than 1 cycle but **half-cycle tripping time is the desirable goal**, making an overall clearing time of $2\frac{1}{2}$ cycles.

There is **very little possibility of improvement in electromagnetic relays** in these respects and this may be a reason for **accelerating the acceptance of transistorized relays.**”

Static Implementations

- “Analog machines” with electronics
- Speed vs security is a design choice (filtering)
- Coincidence timing as a phase comparator



Microprocessor-Based Implementations

- First μP -based relays sampled at low rates
- Phasors were the only practical solution
 - Cosine filter, or
 - Fourier with mimic prefiltering
- Full-cycle band-pass filtering set the speed vs security balance
- Operating characteristics through calculations on complex numbers, such as $\angle(I \cdot Z_R - V, V) < \pm 90^\circ$

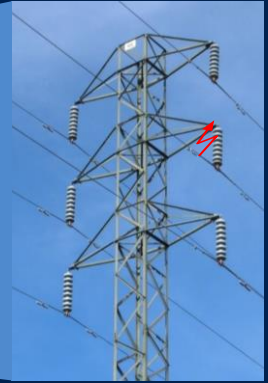
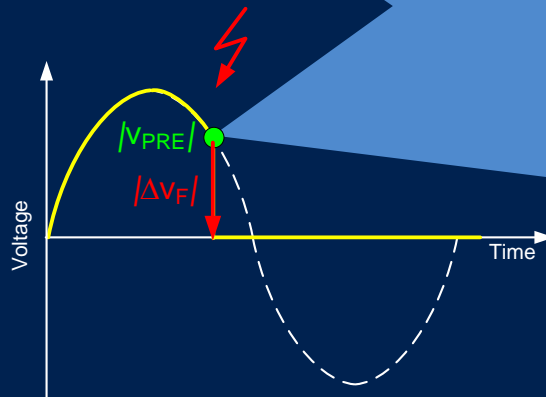
Incremental Quantity Distance Element

$$|V_{PRE}| / |\Delta V_F|$$

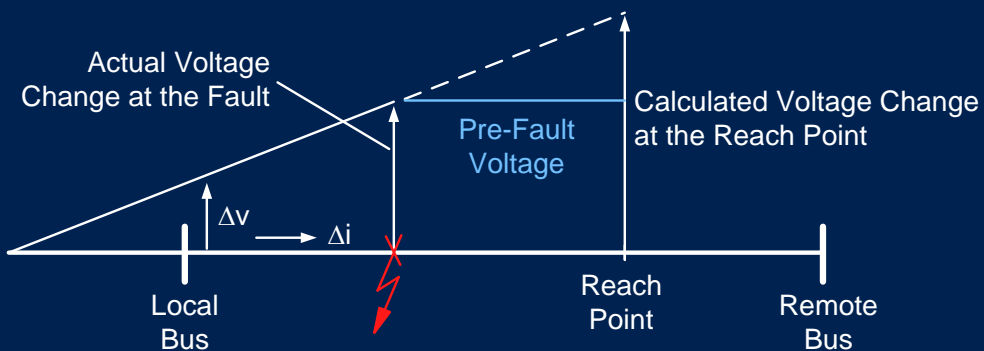
$\Delta V, \Delta i$ Line Parameters (Z_1, Z_0)

TD Distance

Intended Z_1 Reach

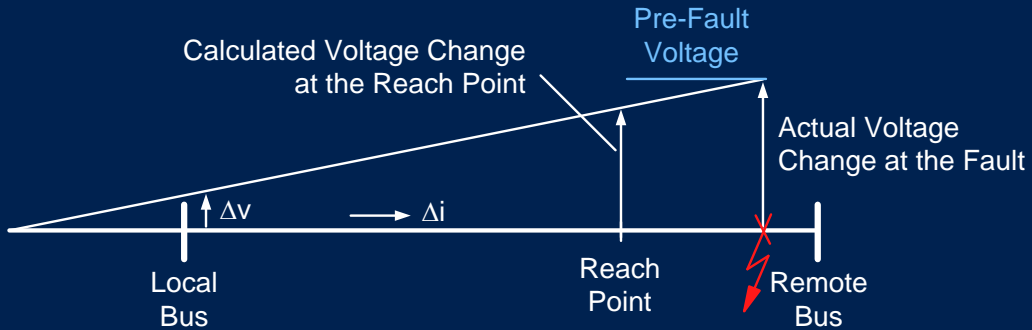


Internal Fault



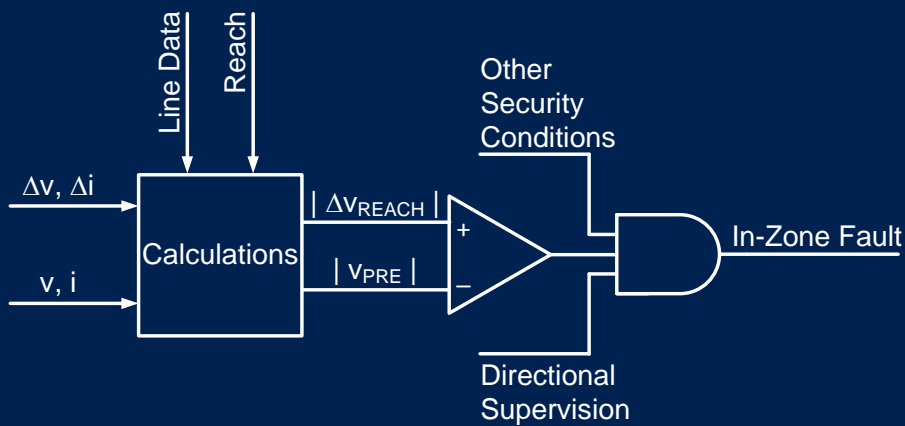
If calculated voltage change at the reach point is **Greater** than calculated pre-fault voltage at the reach point, then **OPERATE**

External Fault



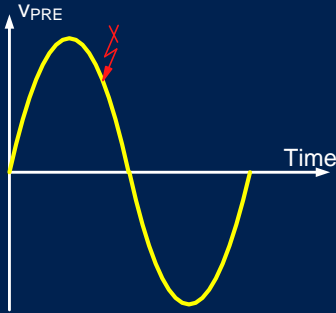
If calculated voltage change at the reach point is **Lower** than calculated pre-fault voltage at the reach point, then **RESTRAIN**

General Implementation

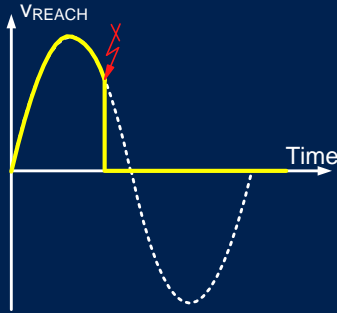


Implementation Considerations

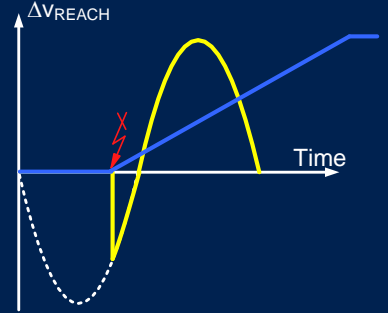
Pre-Fault Voltage



Reach Point Voltage



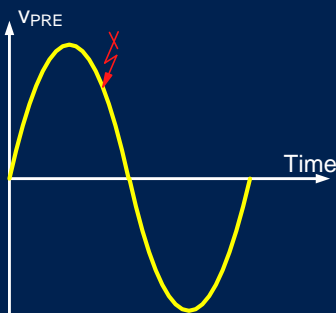
Change in Voltage



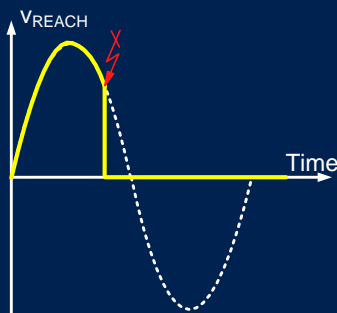
Calculated voltage change can be the **magnitude of a phasor** (hypothetical)

Implementation Considerations

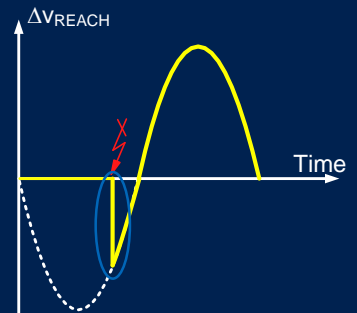
Pre-Fault Voltage



Reach Point Voltage



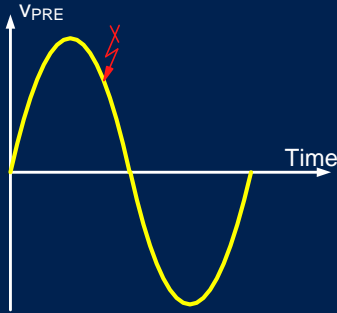
Change in Voltage



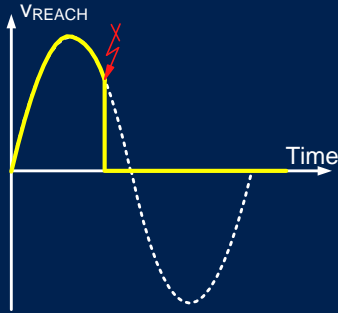
Calculated voltage change can be **an edge or a step** obtained with **a high-pass filter** (actual three-decade-old implementation)

Implementation Considerations

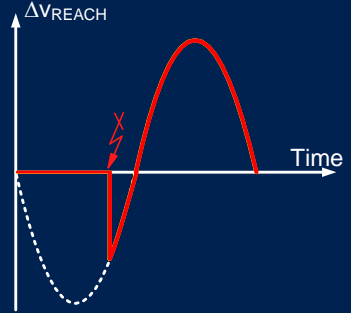
Pre-Fault Voltage



Reach Point Voltage

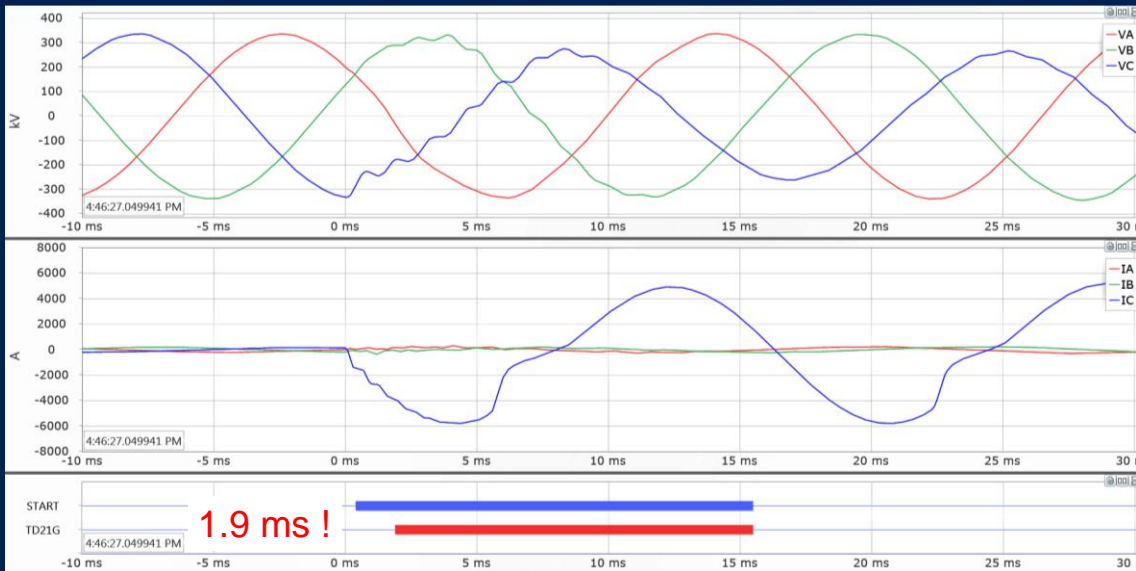


Change in Voltage

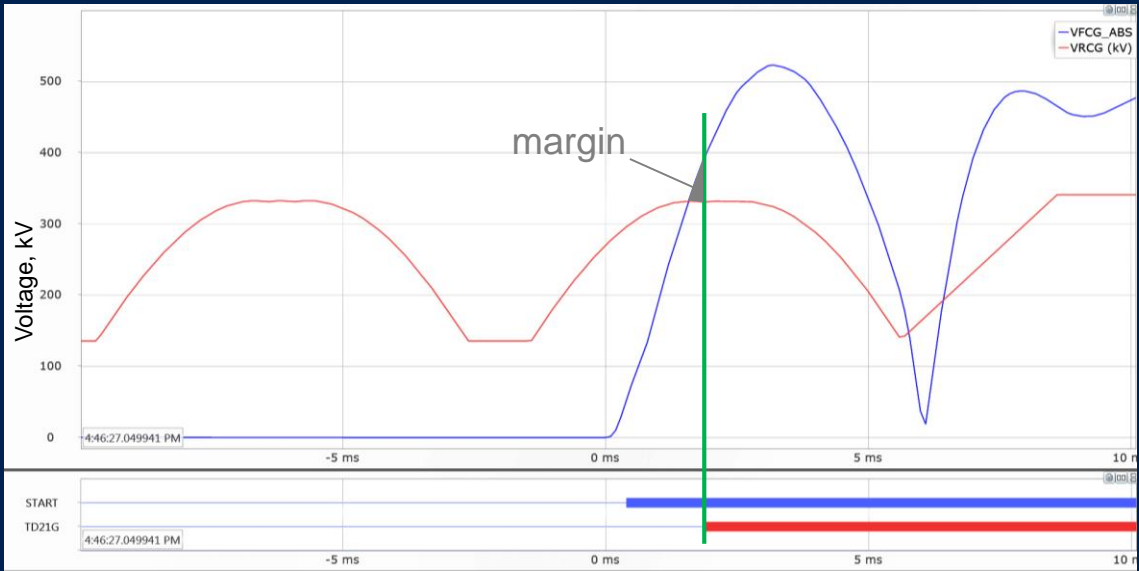


Calculated voltage change can be a **time-domain value** obtained via memory (actual modern implementation)

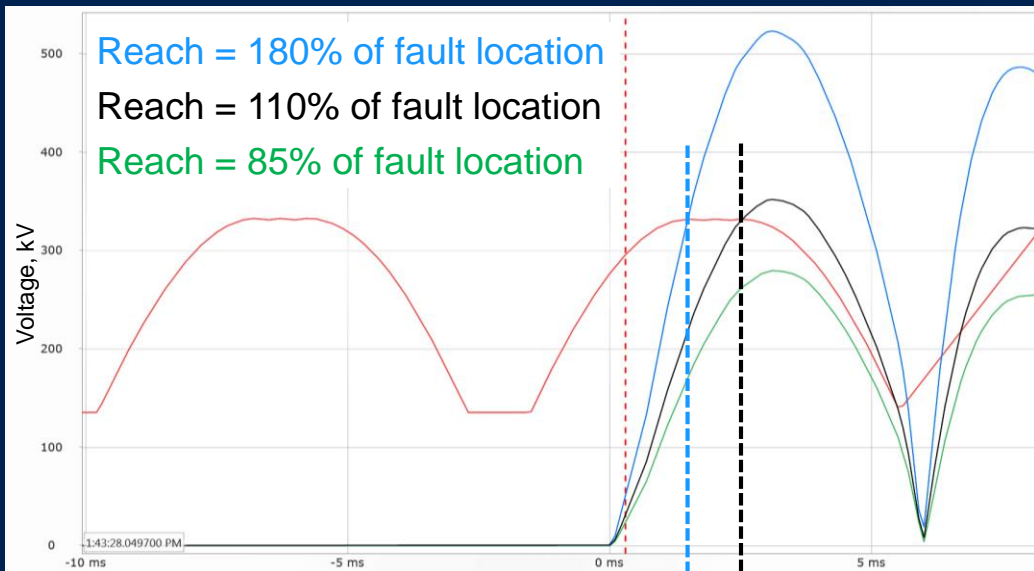
CG Fault at 57% of Zone 1 on a 400 kV, 224 km Line



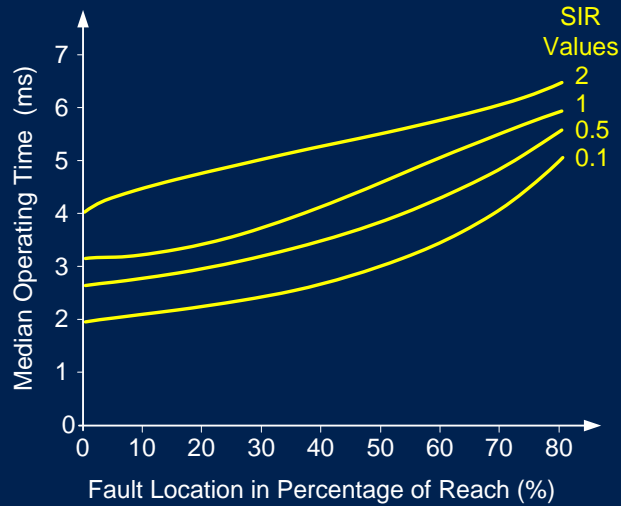
CG Fault at 57% of Zone 1 on a 400 kV, 224 km Line



CG Fault on a 400 kV, 224 km Line



Need for Speed, 2017

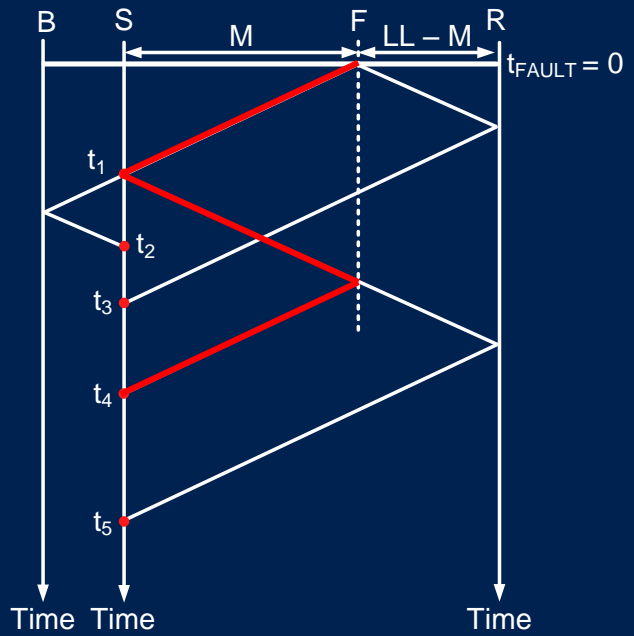


Traveling-Wave Distance Zone 1

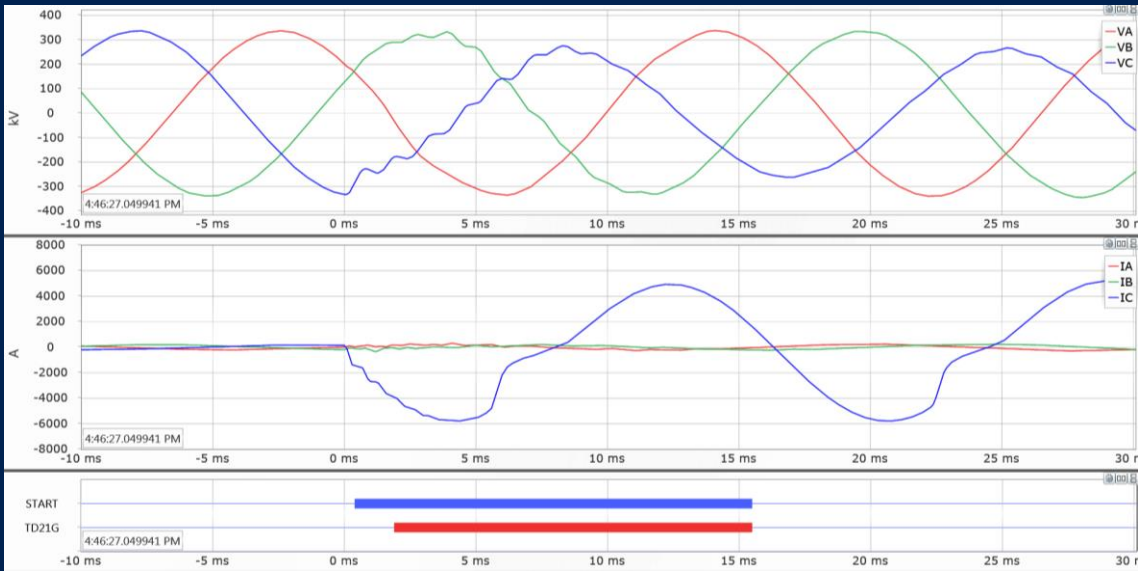
$$2 \cdot M = (t_4 - t_1) \cdot \frac{LL}{TWLPT}$$

$$M = \frac{LL}{2} \cdot \frac{t_4 - t_1}{TWLPT}$$

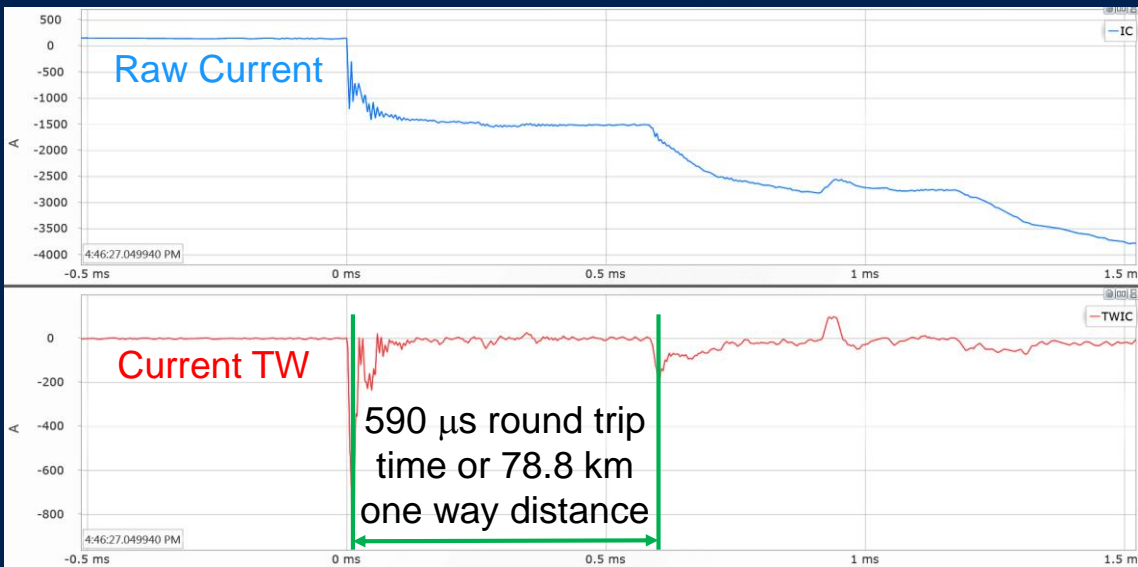
$$\frac{1}{2} \cdot \frac{t_4 - t_1}{TWLPT} < 0.99 \text{ pu} \rightarrow \text{TRIP}$$



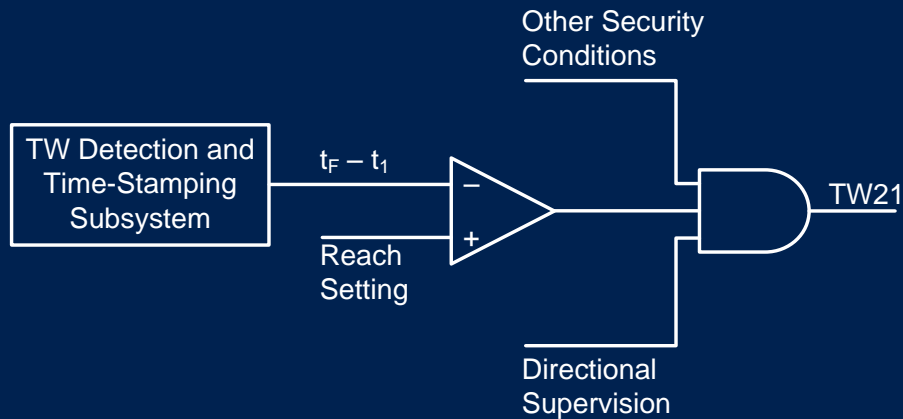
CG Fault at 78.8 km on a 400 kV, 224 km Line



CG Fault at 78.8 km on a 400 kV, 224 km Line



General Implementation

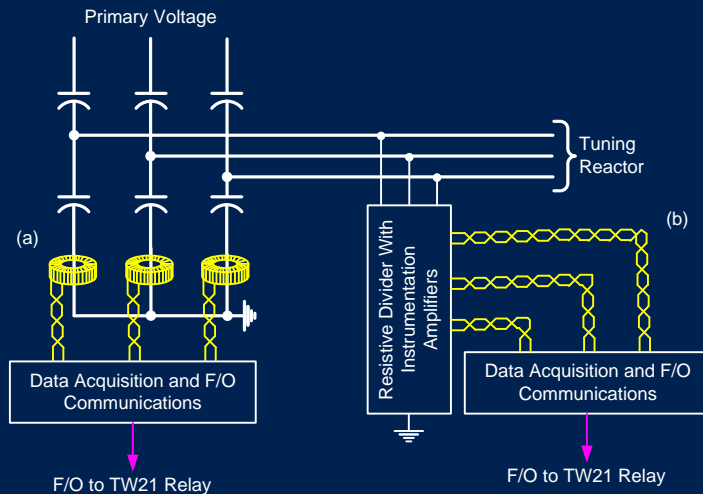


Challenges

- Identifying the first return from the fault
- Faults close to either of the buses
- In-zone switching events
- TW attenuation and dispersion
- Same TW timing and polarity patterns at multiple buses

Measuring Voltage Traveling Waves

Ideas for Retrofitting CCVTs



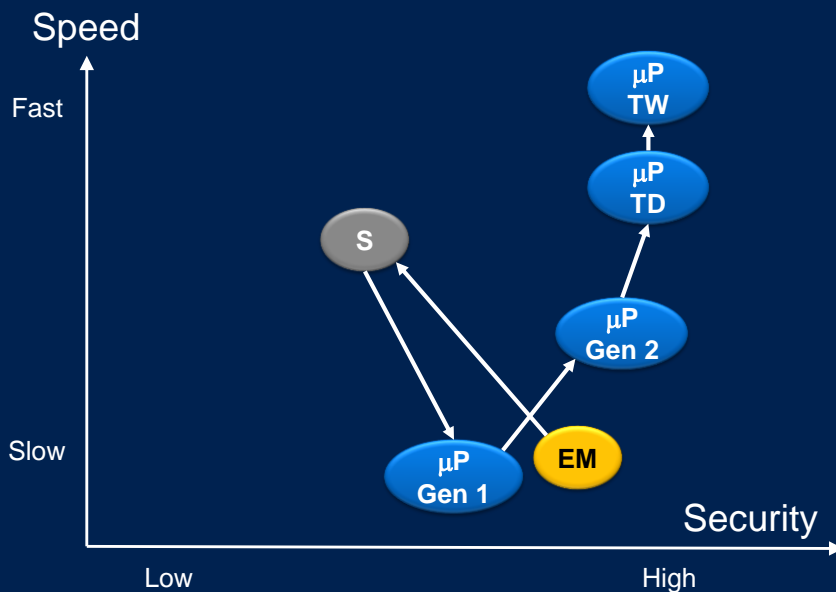
History of Distance Elements

- Electromechanical technology shaped the characteristics we use today
- Static technology introduced wide design choices
- Initially limited by processing power, μP technology reverted to speed of electromechanical relays
- Today's μP relays with very fast sampling and vast processing can implement any distance principle

Three Types of Distance Principles

- Apparent impedance elements: 1 cycle
- Incremental quantity elements: 2 ms – 0.5 cycle
- Traveling-wave elements: 1 – 2 ms

Progress in Distance Element Performance



Conclusions

- Distance elements are a cornerstone of line protection
- We have not reached performance limits yet
- Today we have access to a phenomenal relay technology (μs sampling and processing)
- We have an obligation to continue to innovate

