

Protection Challenges for North America's First Combined Cable / Overhead Double-Circuit 500 kV Transmission Line With Mutual Coupling

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Project Background

- New 75-mile 500 kV transmission line
- Single-circuit and double-circuit construction
- Protection package
 - System A – Line current differential
 - System B – Directional comparison blocking
 - System C – Permissive overreaching transfer trip

Decreasing Land Availability...



From Overhead...



To Underground



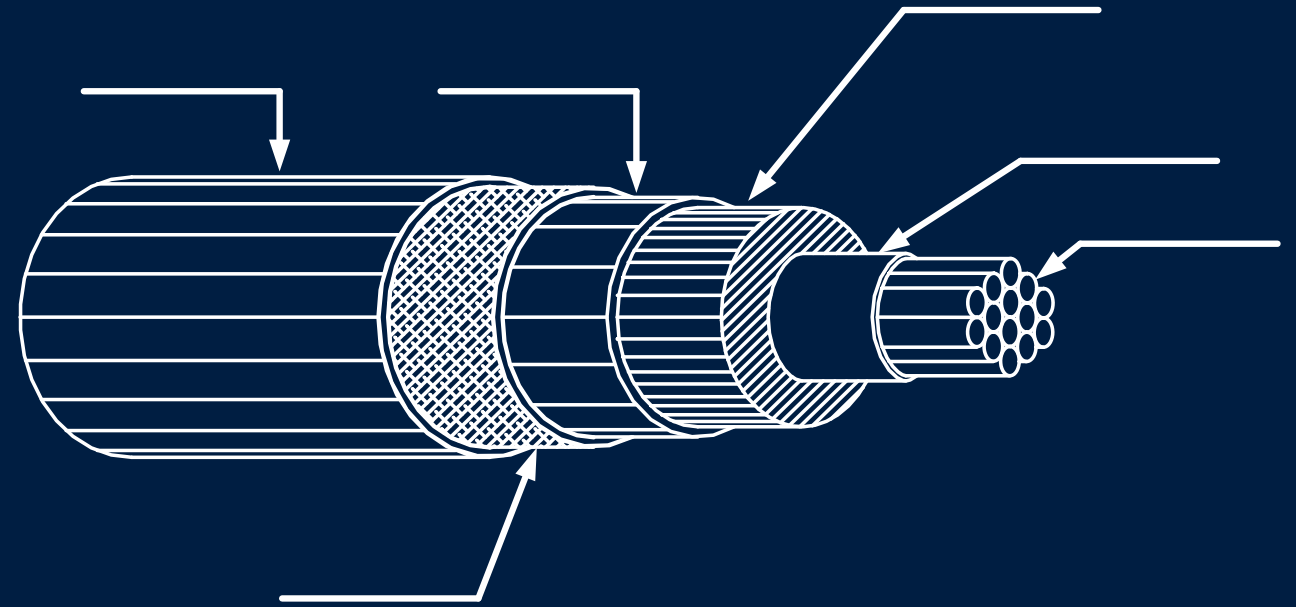
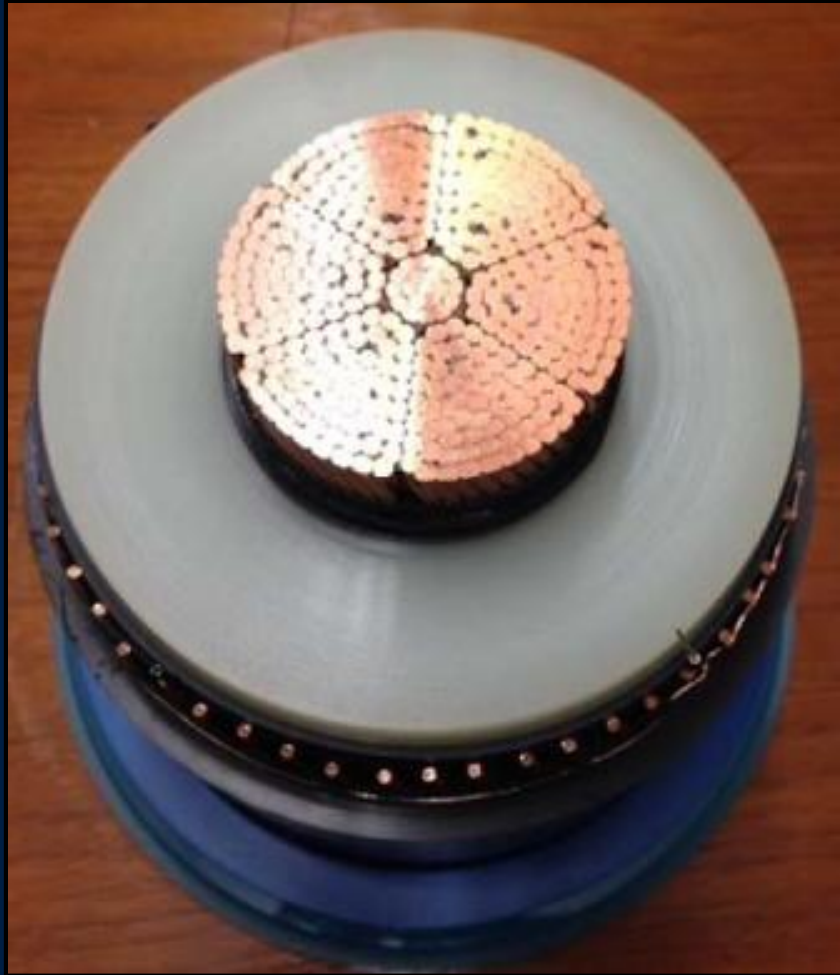
Transition Towers

West



East

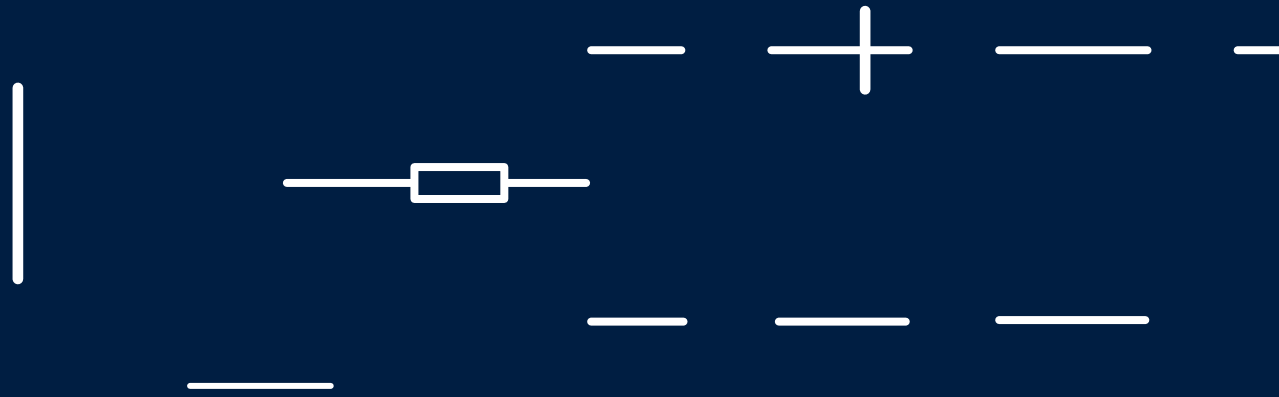
Cable Layout



Vaults and Terminations



Overall Line Composition



Line Section 1: 33 Miles

- Two conductors per phase
- Segmented ground wires

Line Section 2: 28 Miles

- Two conductors per phase
- Segmented ground wires

Line Section 3: 4 Miles

- Underground
- Two cables per phase

Line Section 4: 8 Miles

- Line 1: 500 kV line
- Line 2: Future 500 kV line

Impedance Comparison

Overhead

$$Z_1 = 0.05 + j0.58 = 0.58 \angle 85^\circ \text{ ohms / mile}$$

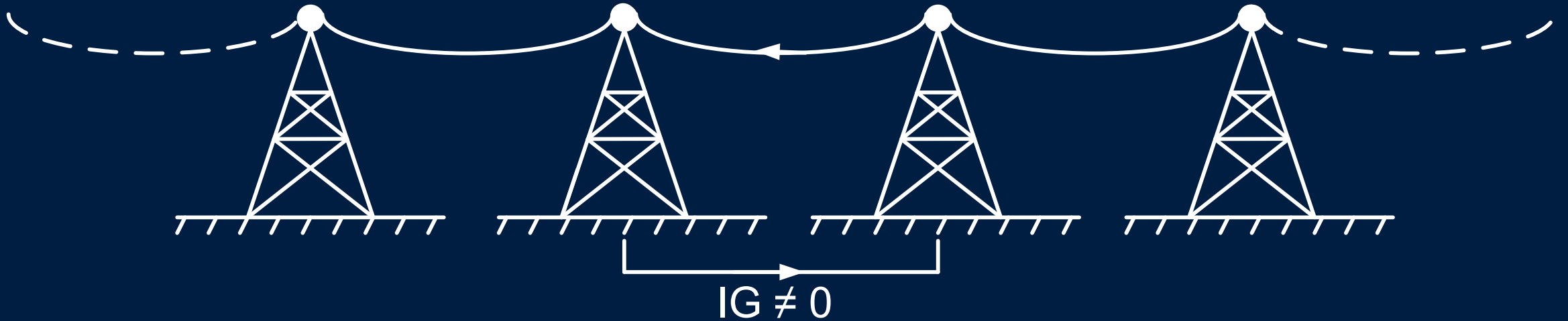
$$Z_0 = 0.44 + j2.13 = 2.17 \angle 78^\circ \text{ ohms / mile}$$

Underground

$$Z_1 = 0.02 + j0.31 = 0.31 \angle 86^\circ \text{ ohms / mile}$$

$$Z_0 = 0.20 + j0.13 = 0.24 \angle 33^\circ \text{ ohms / mile}$$

Ground Wire Segmentation



- Phase conductors induce voltage in ground wire
- Induced voltage leads to circulating current and losses
- Segmenting ground wires prevents circulating current

Line Impedance Calculation

$$V_{A_DROPP} = Z_{AA} \cdot I_A + Z_{AB} \cdot I_B + Z_{AC} \cdot I_C + \dots \\ Z_{AA'} \cdot I_{A'} + Z_{AB'} \cdot I_{B'} + Z_{AC'} \cdot I_{C'}$$

Where:

Z_{AA} = Self impedance

Z_{AB} and Z_{BC} = Mutual impedance between phases

$Z_{AA'}$, $Z_{AB'}$, and $Z_{AC'}$ = Mutual impedance between the A-phase conductor Line 1 and ϕ -phase conductor Line 2

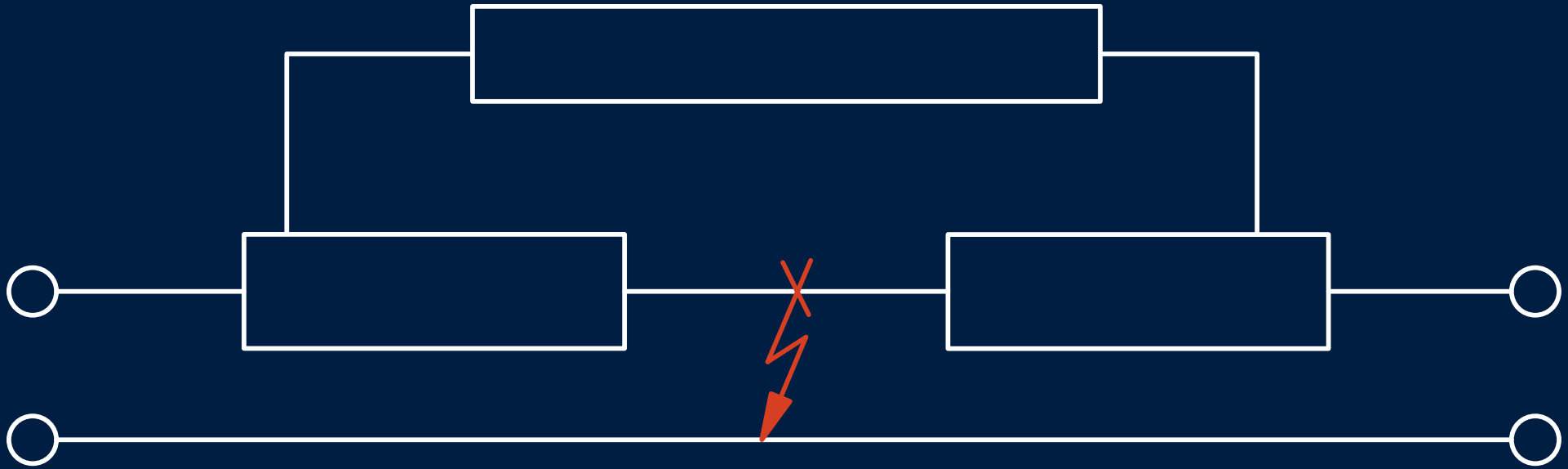
Put in Matrix Form...

$$\begin{bmatrix} V_{A_{\text{DROP}}} \\ V_{B_{\text{DROP}}} \\ V_{C_{\text{DROP}}} \\ V_{A'_{\text{DROP}}} \\ V_{B'_{\text{DROP}}} \\ V_{C'_{\text{DROP}}} \end{bmatrix} = \begin{bmatrix} Z_{AA} & Z_{AB} & Z_{AC} & Z_{AA'} & Z_{AB'} & Z_{AC'} \\ Z_{BA} & Z_{BB} & Z_{BC} & Z_{BA'} & Z_{BB'} & Z_{BC'} \\ Z_{CA} & Z_{CB} & Z_{CC} & Z_{CA'} & Z_{CB'} & Z_{CC'} \\ Z_{A'A} & Z_{A'B} & Z_{A'C} & Z_{A'A'} & Z_{A'B'} & Z_{A'C'} \\ Z_{B'A} & Z_{B'B} & Z_{B'C} & Z_{B'A'} & Z_{B'B'} & Z_{B'C'} \\ Z_{C'A} & Z_{C'B} & Z_{C'C} & Z_{C'A'} & Z_{C'B'} & Z_{C'C'} \end{bmatrix} \cdot \begin{bmatrix} I_A \\ I_B \\ I_C \\ I_{A'} \\ I_{B'} \\ I_{C'} \end{bmatrix}$$

...Then Sequence Domain

$$(Z_{012}) = \begin{array}{c} \text{Line 1} \qquad \qquad \text{Mutual} \\ \left(\begin{array}{ccc|ccc} \color{red}{Z_0} & w & x & \color{red}{Z_{0M}} & w_m & x_m \\ w & \color{red}{Z_1} & y & w_m & z_{1m} & y_m \\ x & y & z_2 & x_m & y_m & z_{2m} \\ \hline \color{red}{Z_{0M}} & w_m & x_m & \color{red}{Z_{0'}} & x' & y' \\ w_m & z_{1m} & y_m & x' & \color{red}{Z_{1'}} & z' \\ x_m & y_m & z_{2m} & y' & z' & z_{2'} \end{array} \right) \\ \text{Mutual} \qquad \qquad \text{Line 2} \end{array}$$

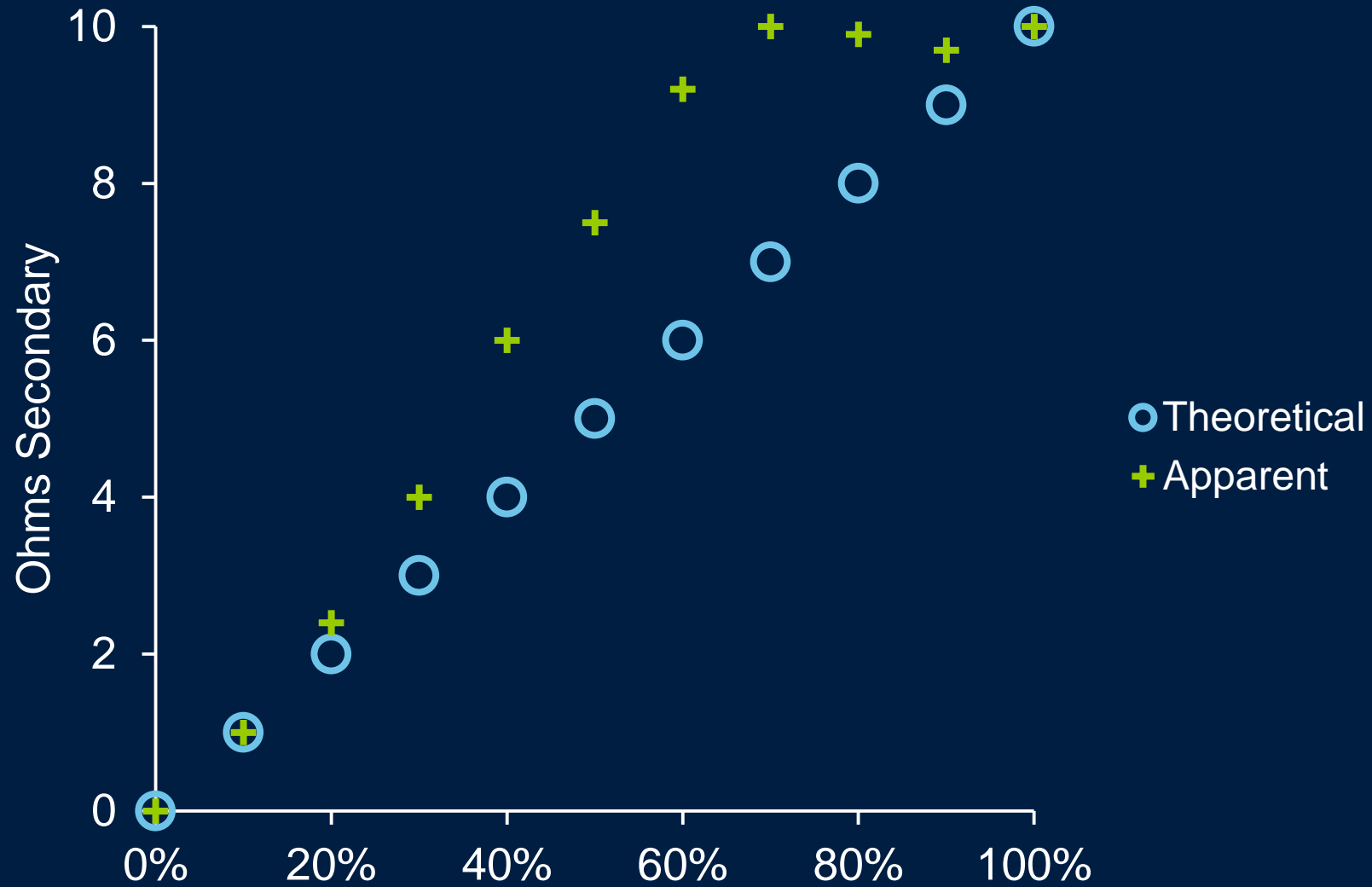
Parallel Line Apparent Impedance



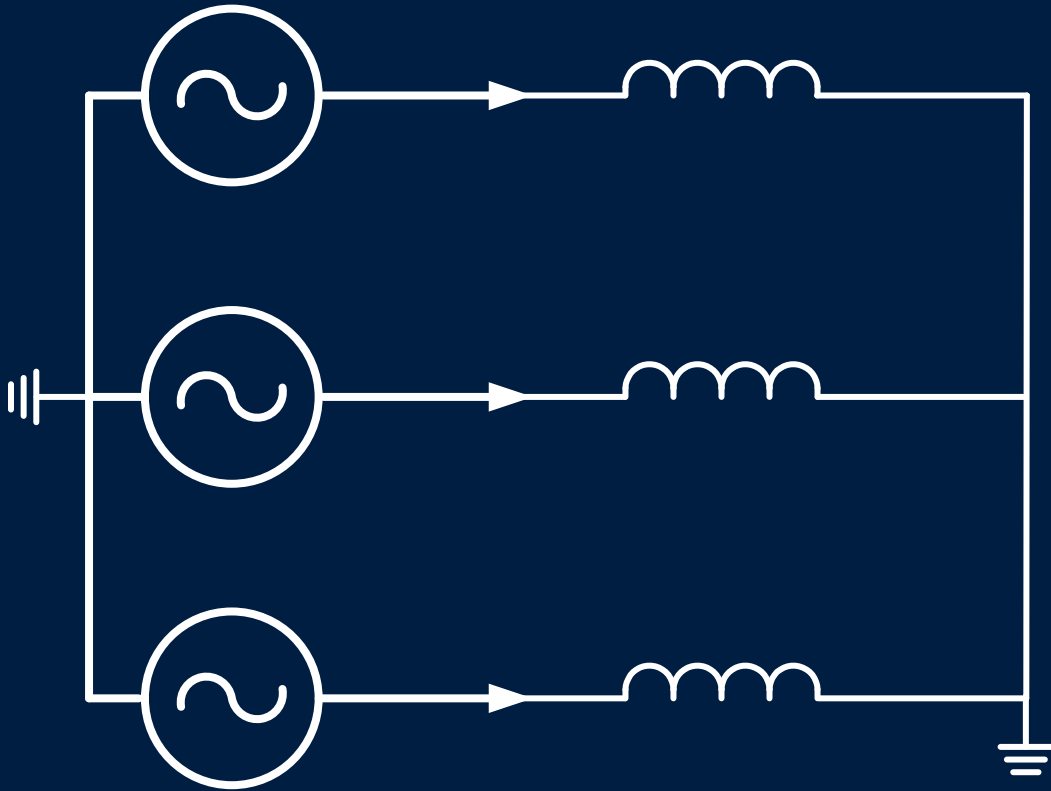
$$Z_{S_TERM} = m \cdot Z_{L1} (1 - \frac{1}{2} m)$$

$$Z_{T_TERM} = \frac{1}{2} \cdot Z_{L1} \cdot (1 - m^2)$$

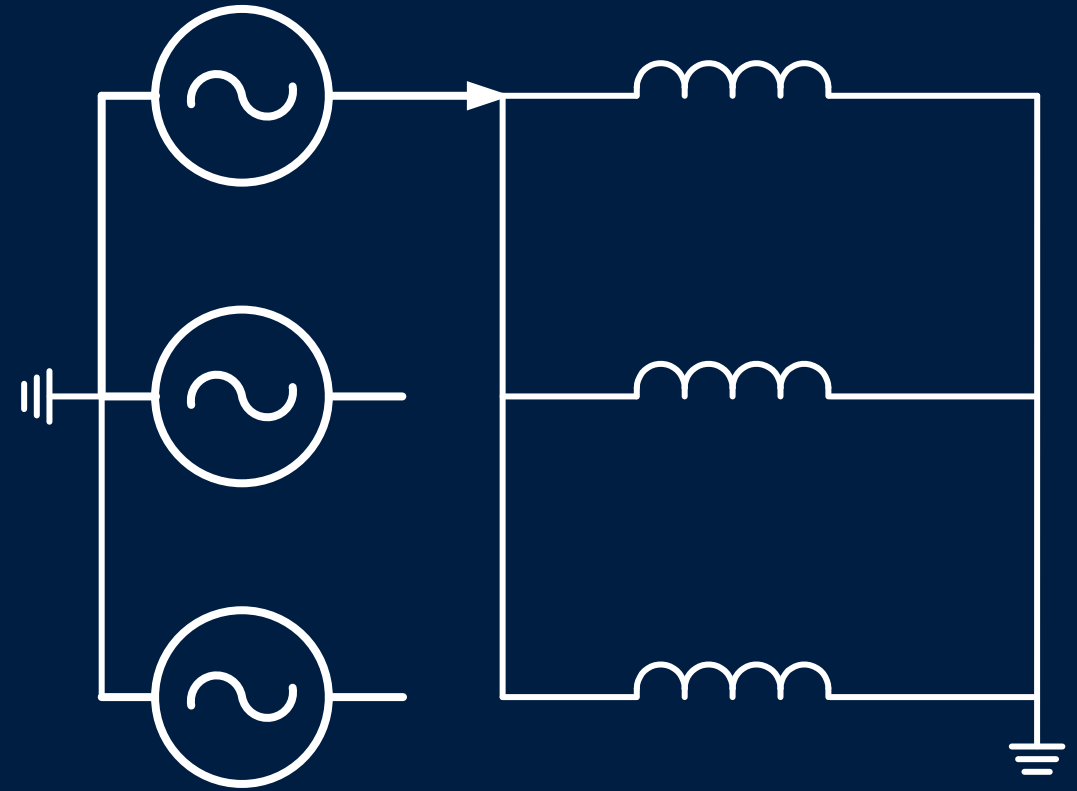
Double-Circuit Apparent Impedance



Sequence Impedance Through Energization



Positive-sequence



Zero-sequence

Impedance Calculation

Matrix calculation

$$Z_1 = 3.26 + j33.32 \Omega$$

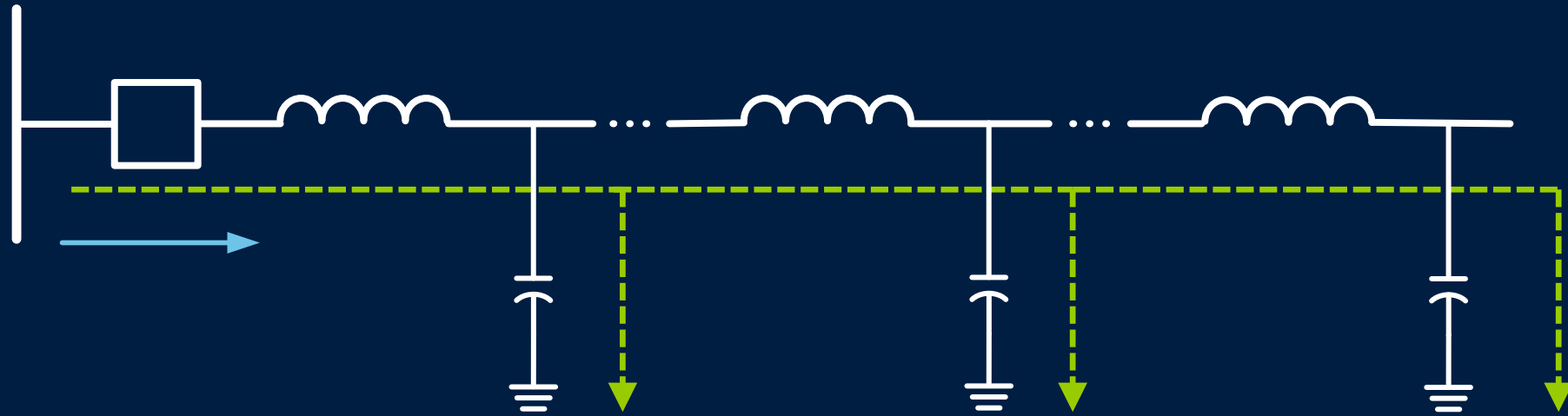
$$Z_0 = 24.73 + j142.65 \Omega$$




Energization

$$Z_1 = 3.56 + j33.92 \Omega$$

$$Z_0 = 25.30 + j144.80 \Omega$$

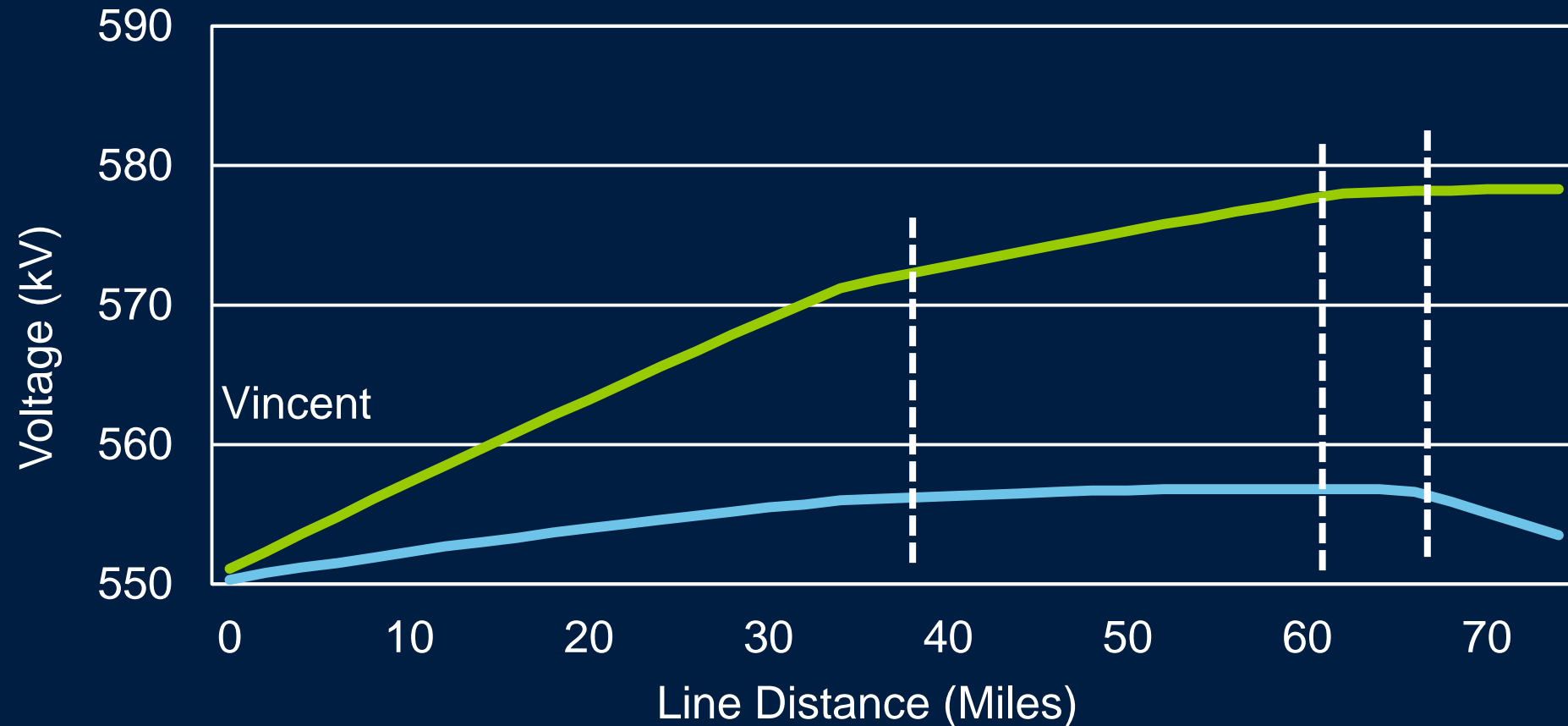
Charging Current Leads to High Voltage



-  Voltage rise
-  Distributed capacitance charging current
-  Total charging current

Charging Current Leads to High Voltage

$$I_{1_CHRG} = j\omega C_1 \frac{V_{Ph-Ph}}{\sqrt{3}} \approx 2 \text{ amperes per mile overhead} \\ \approx 40 \text{ amperes per mile underground}$$



Protection System Validation

- Reduce short-circuit model to area of interest
- Maintain 500 kV system with boundary equivalents
- Build model in real-time digital simulator
- Choose realistic operating conditions
- Integrate physical relays with simulation

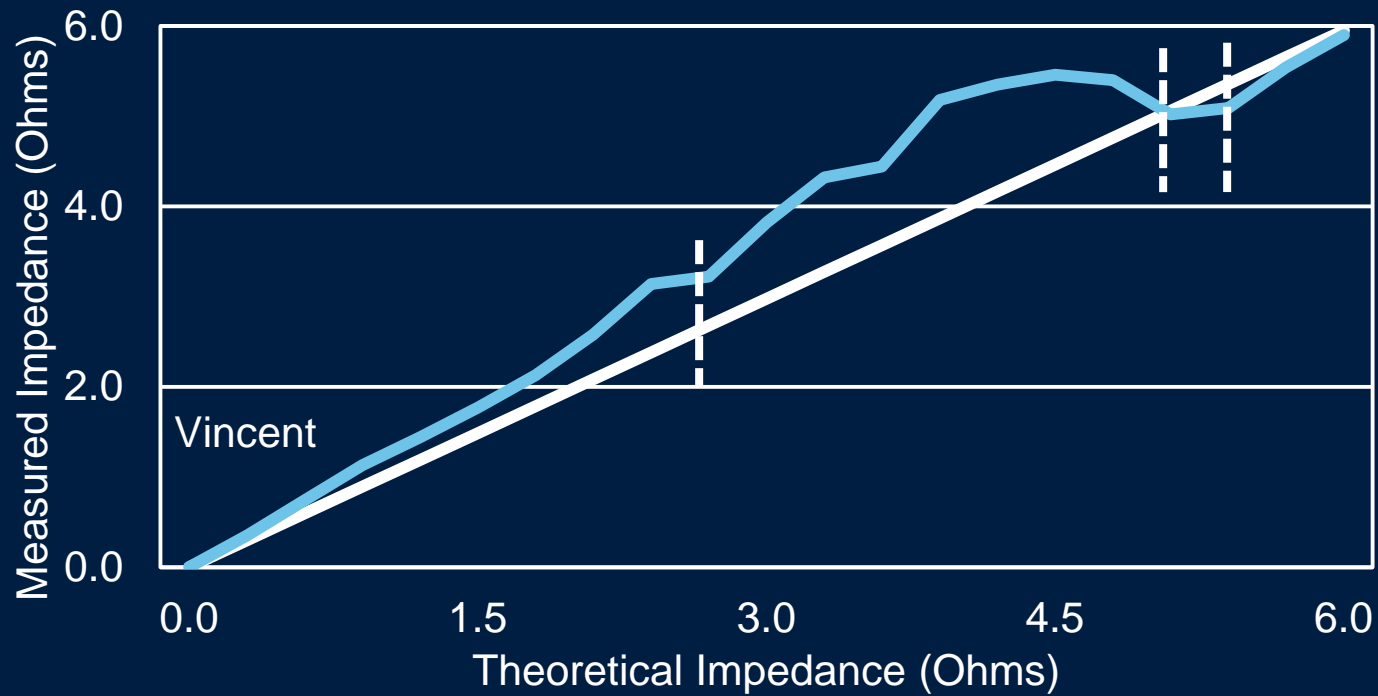
Protection System Validation

Test Plan

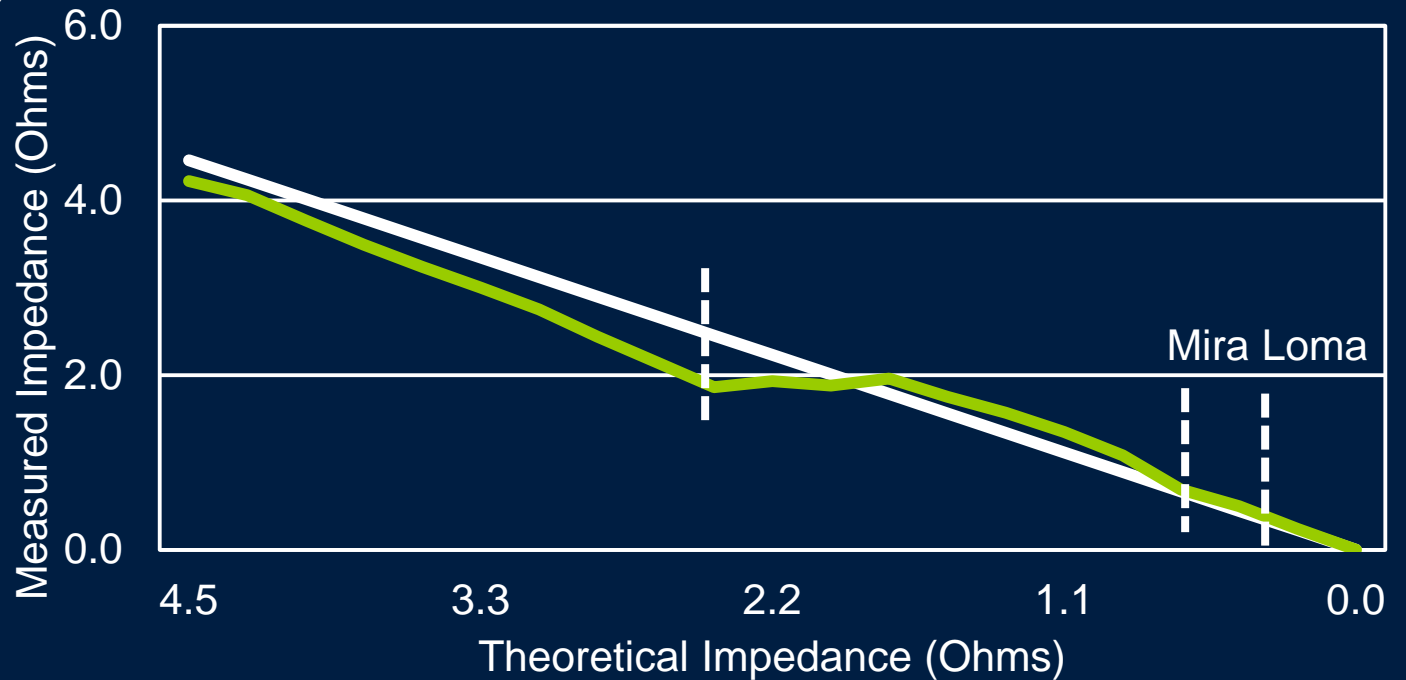
- Basic internal and external faults
- Line energization and load pickup
- Zone 1 margin
- High-impedance faults
- Batch tests

Batch Tests

- All internal and external fault locations (21 internal and 10 external)
- Ten fault types (AG, BG, CG, ABG, BCG, CAG, AB, BC, CA, and ABCG)
- Four fault inception angles (0, 30, 60, and 90 degrees)
- All load flow cases

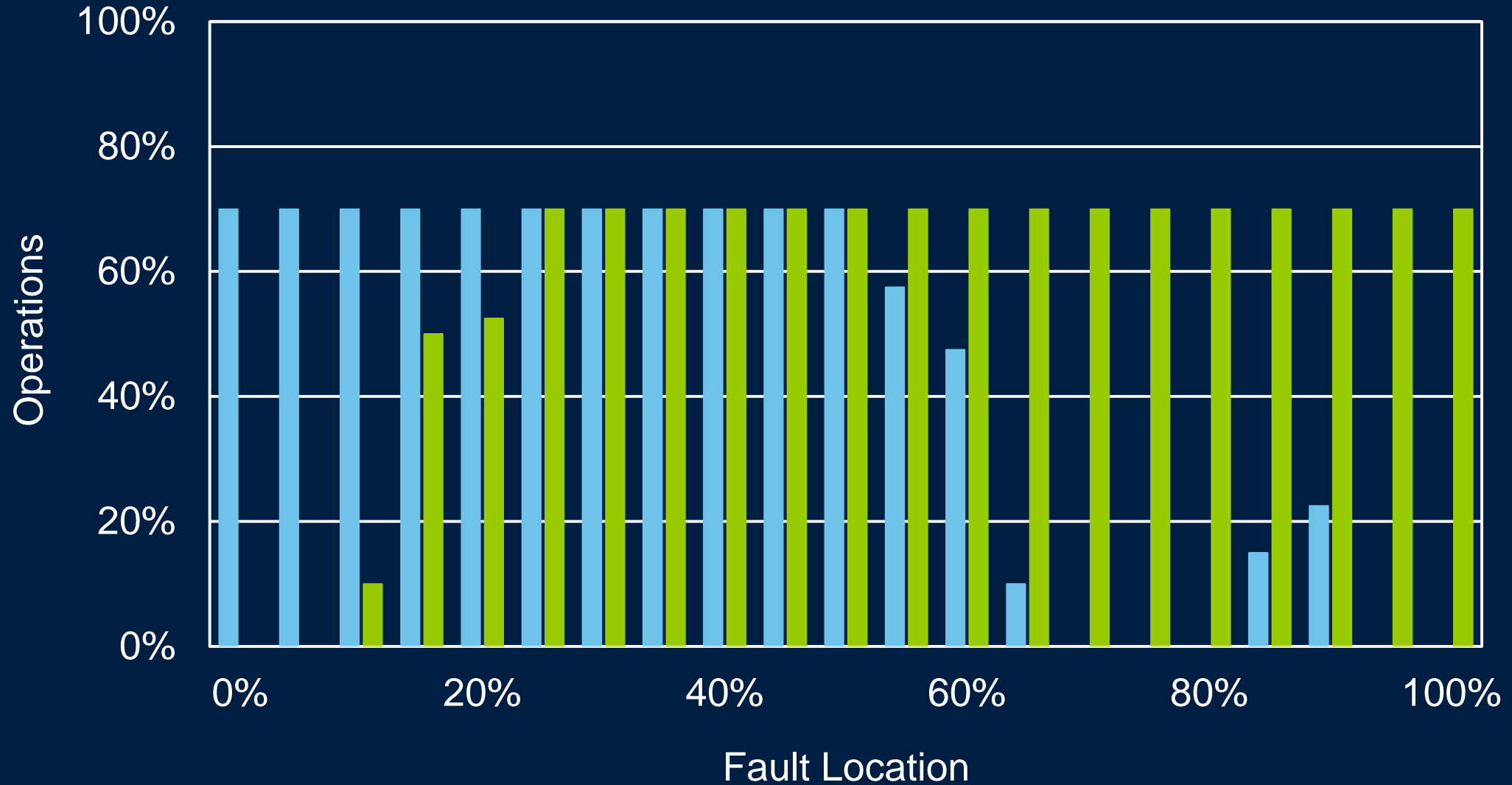


Distance Element Performance



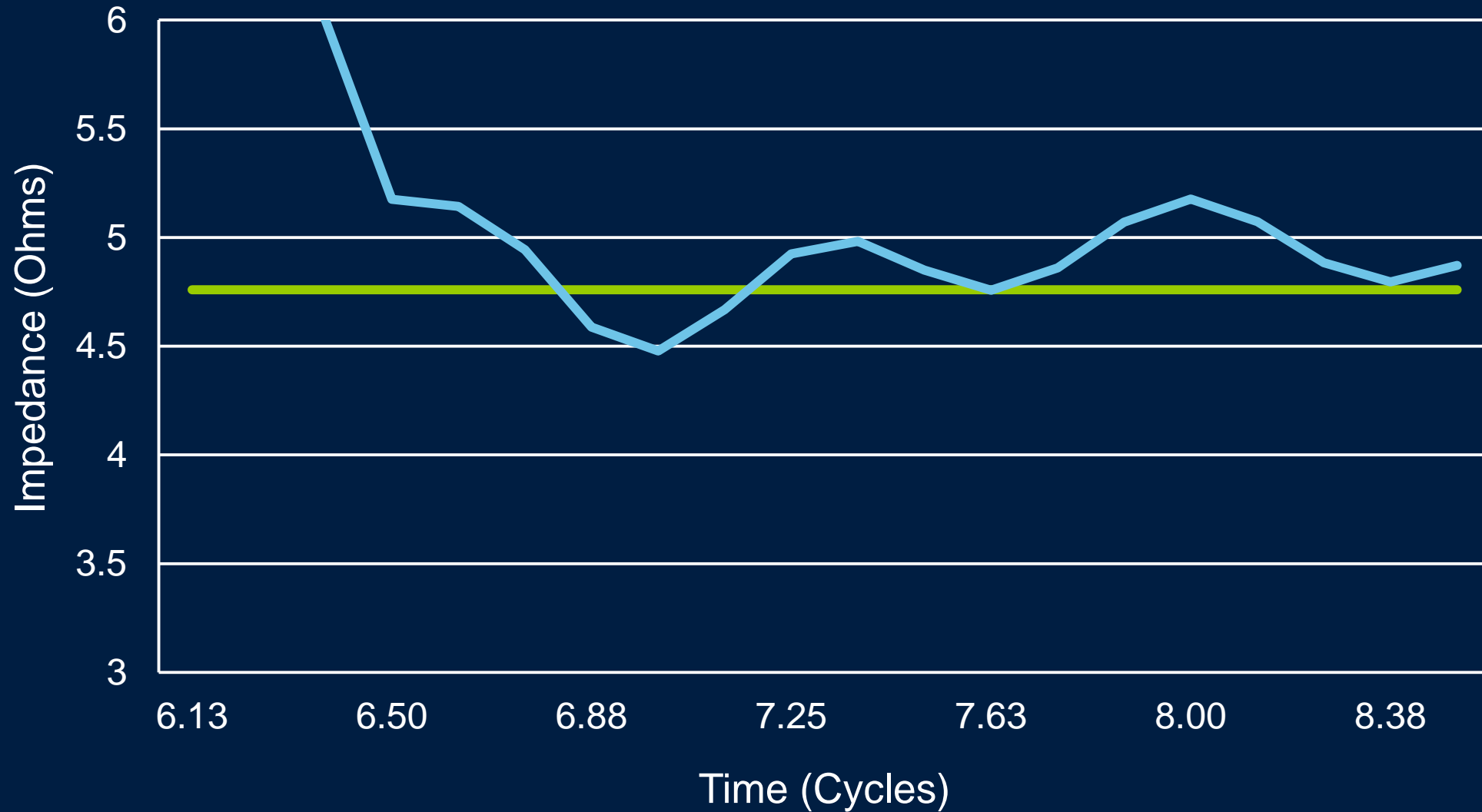
Zone 1 Performance

Manufacturer A

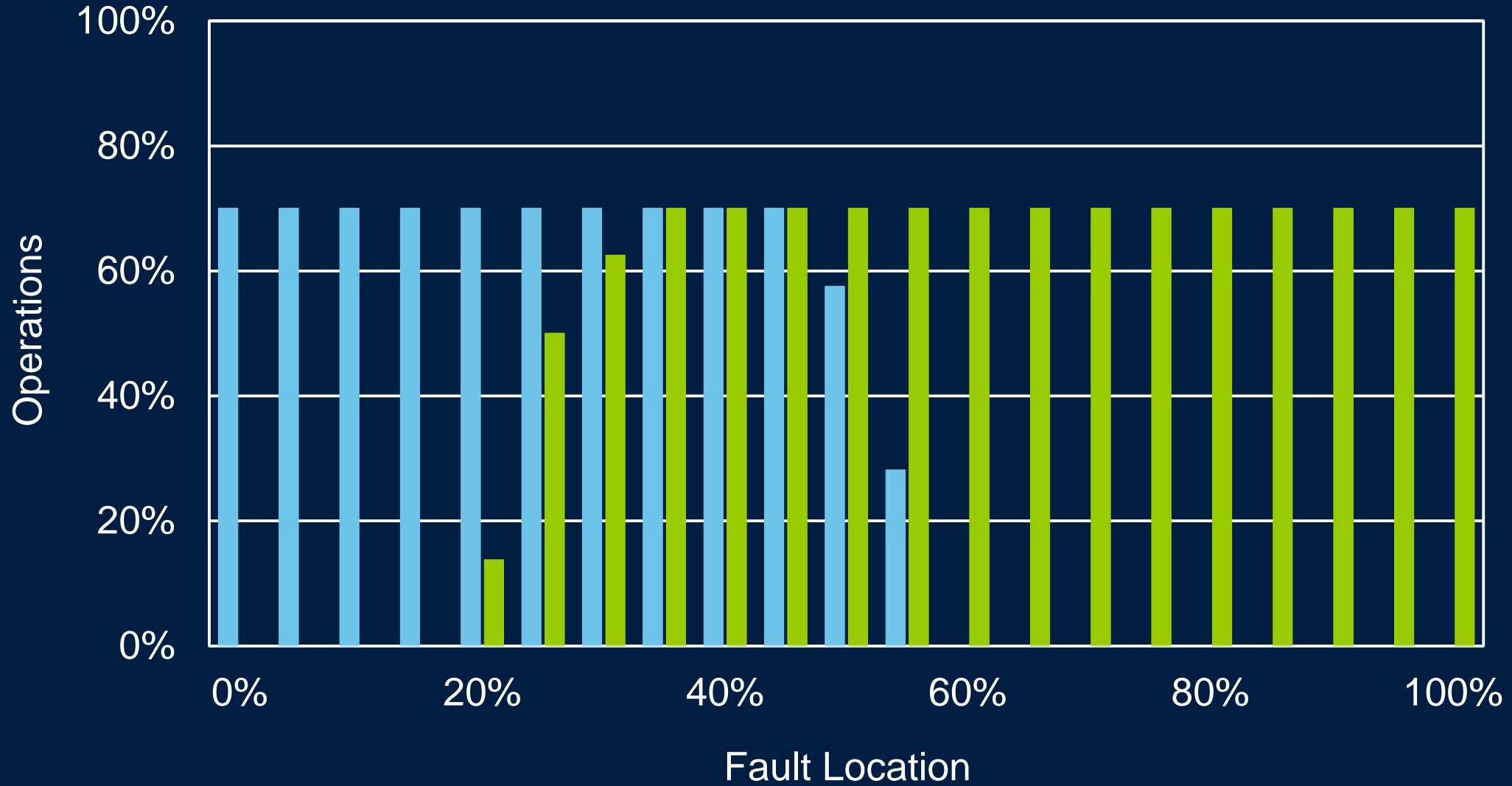


Zone 1 Performance

Manufacturer A

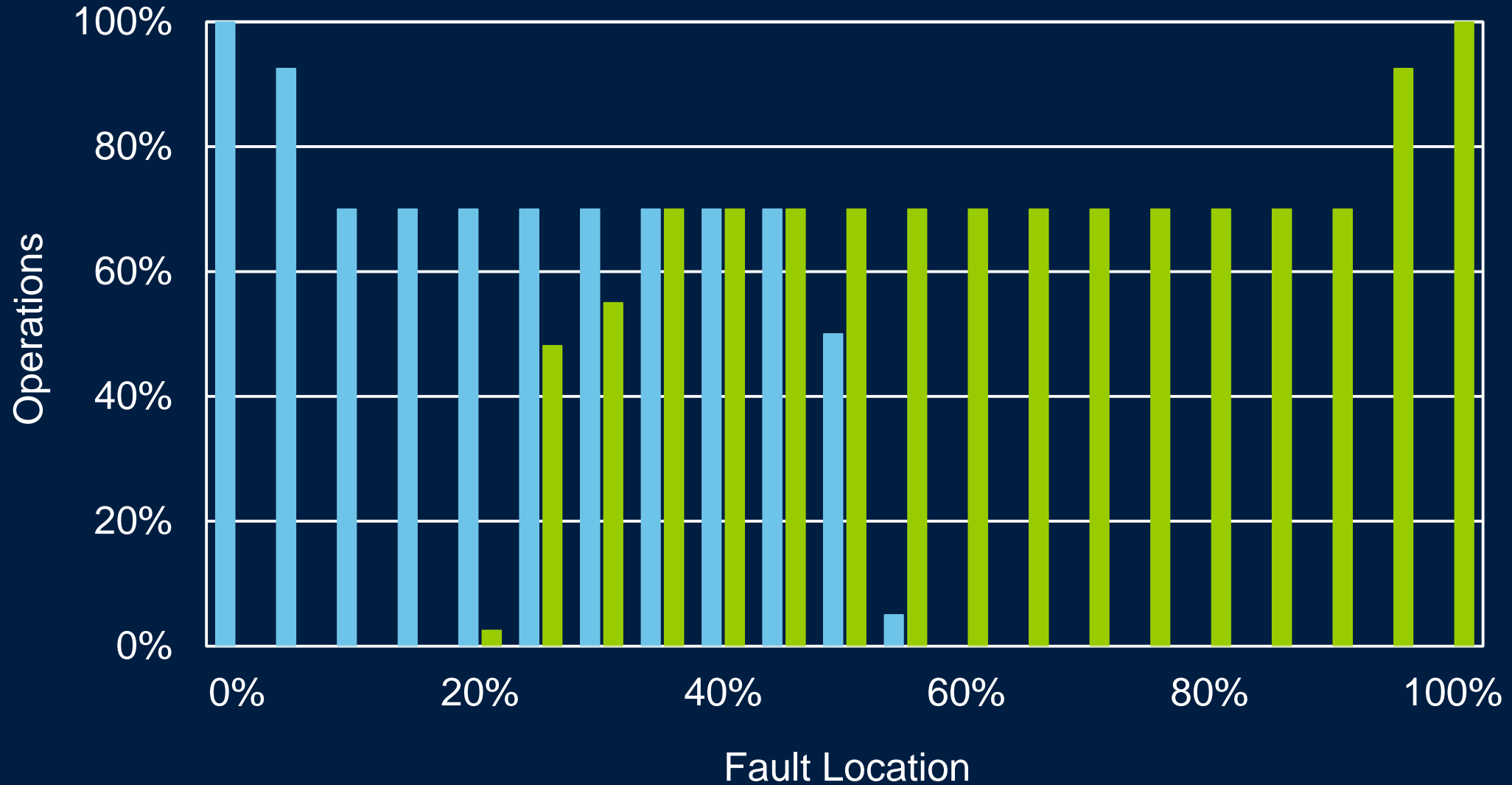


Modify Settings and Repeat Manufacturer A

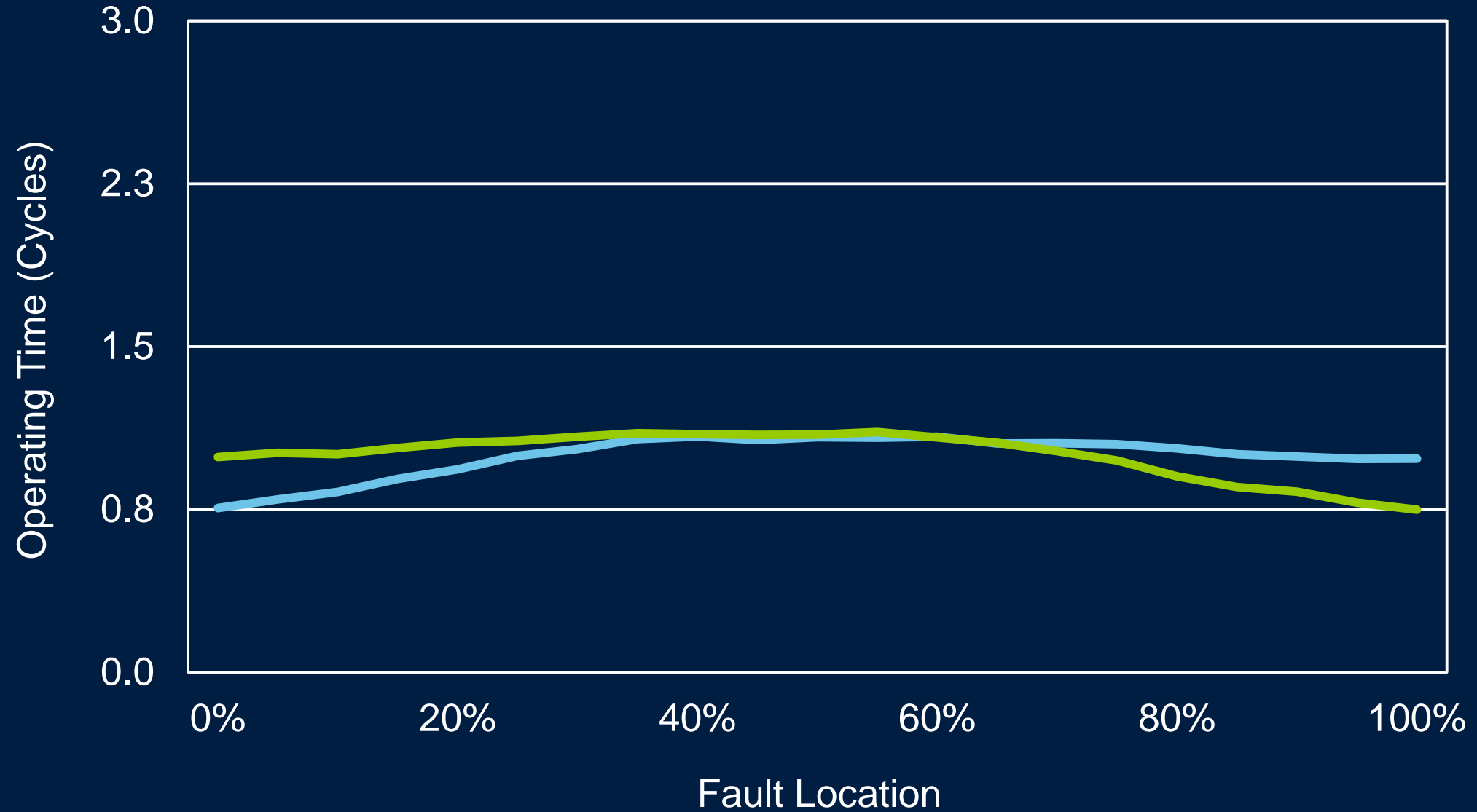


How Did the Other Relay Do?

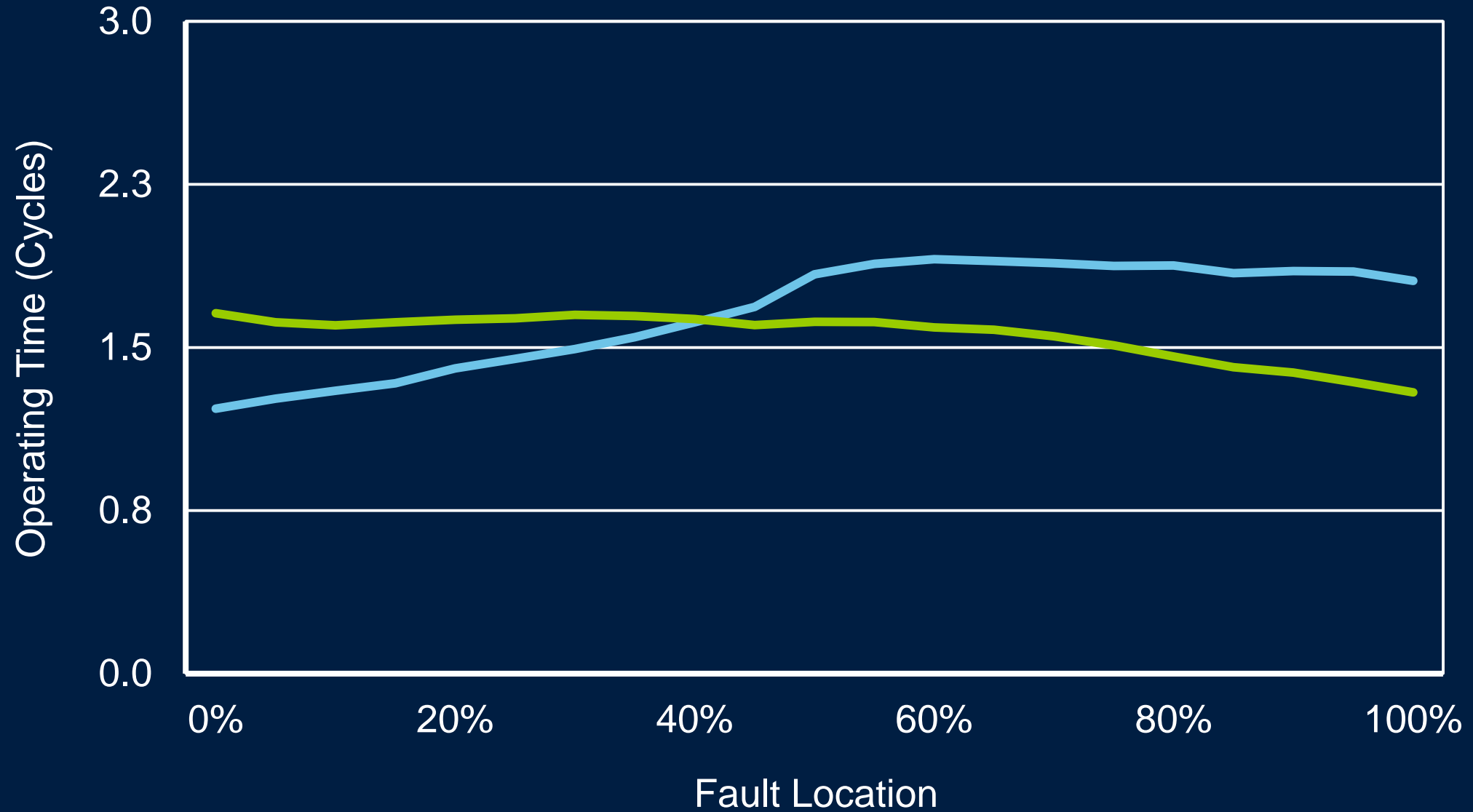
Manufacturer B



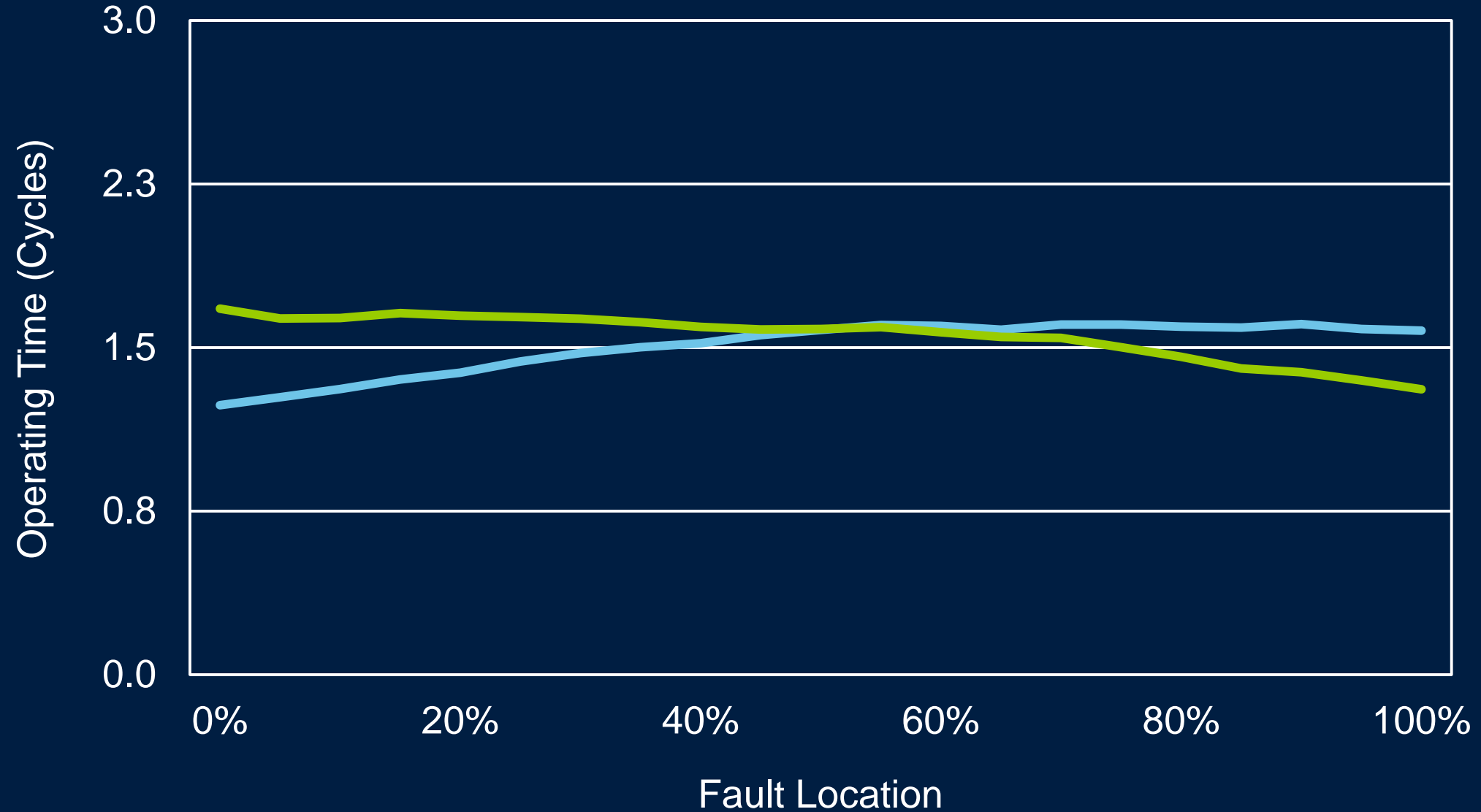
Manufacturer A Distance Performance



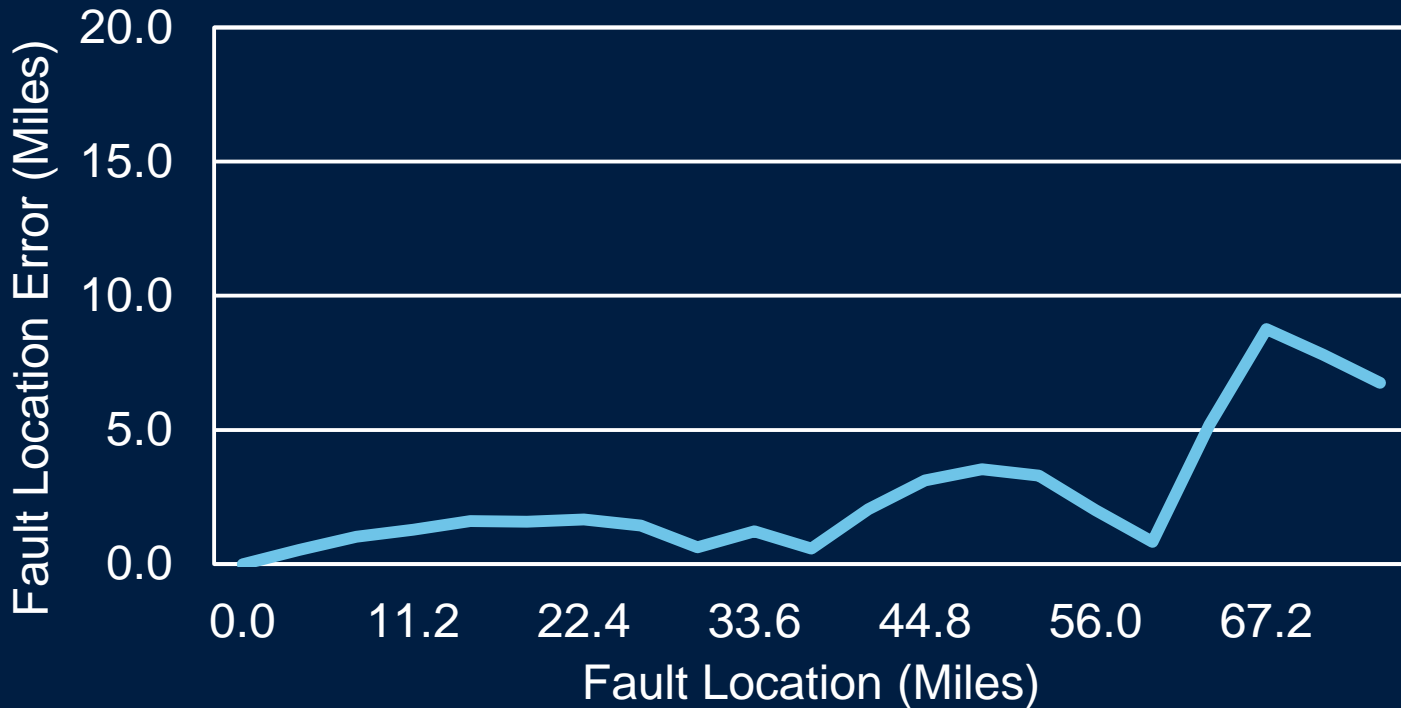
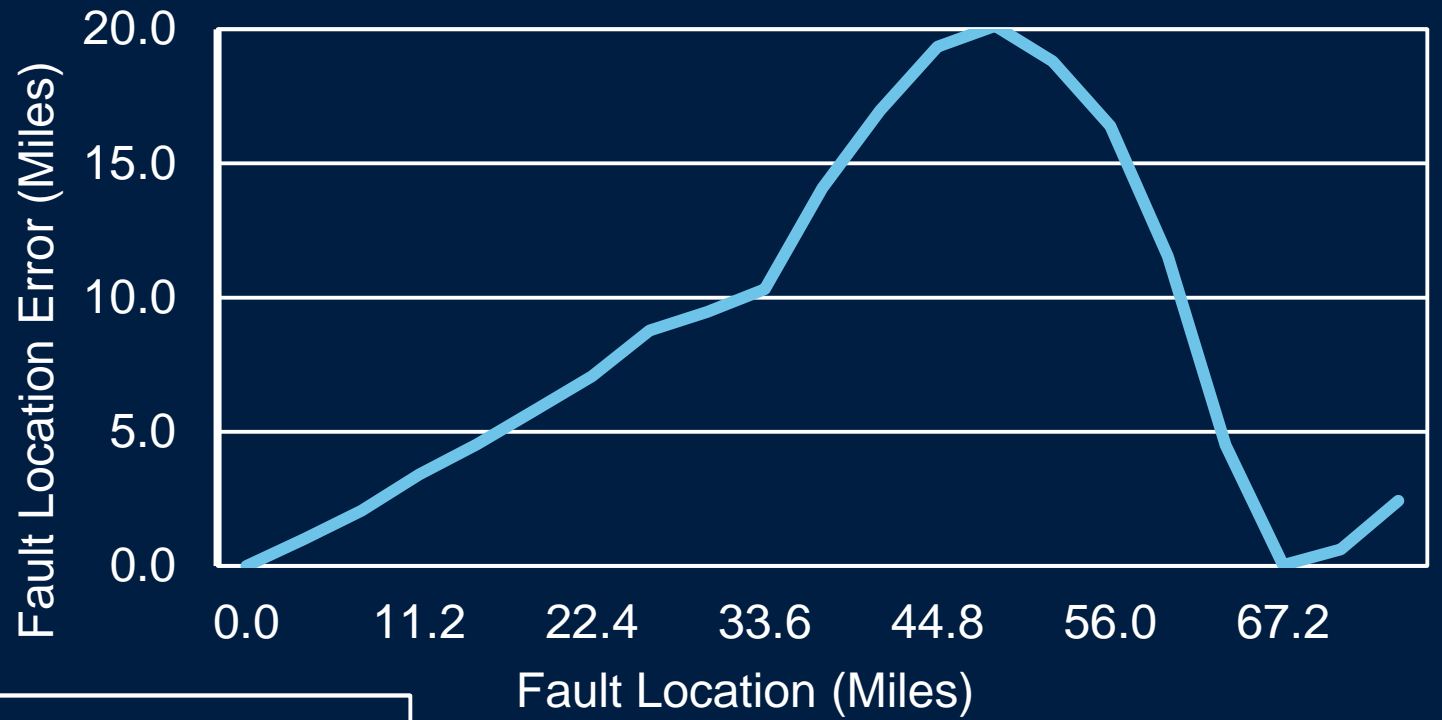
Manufacturer B Distance Performance



Manufacturer B Differential Performance



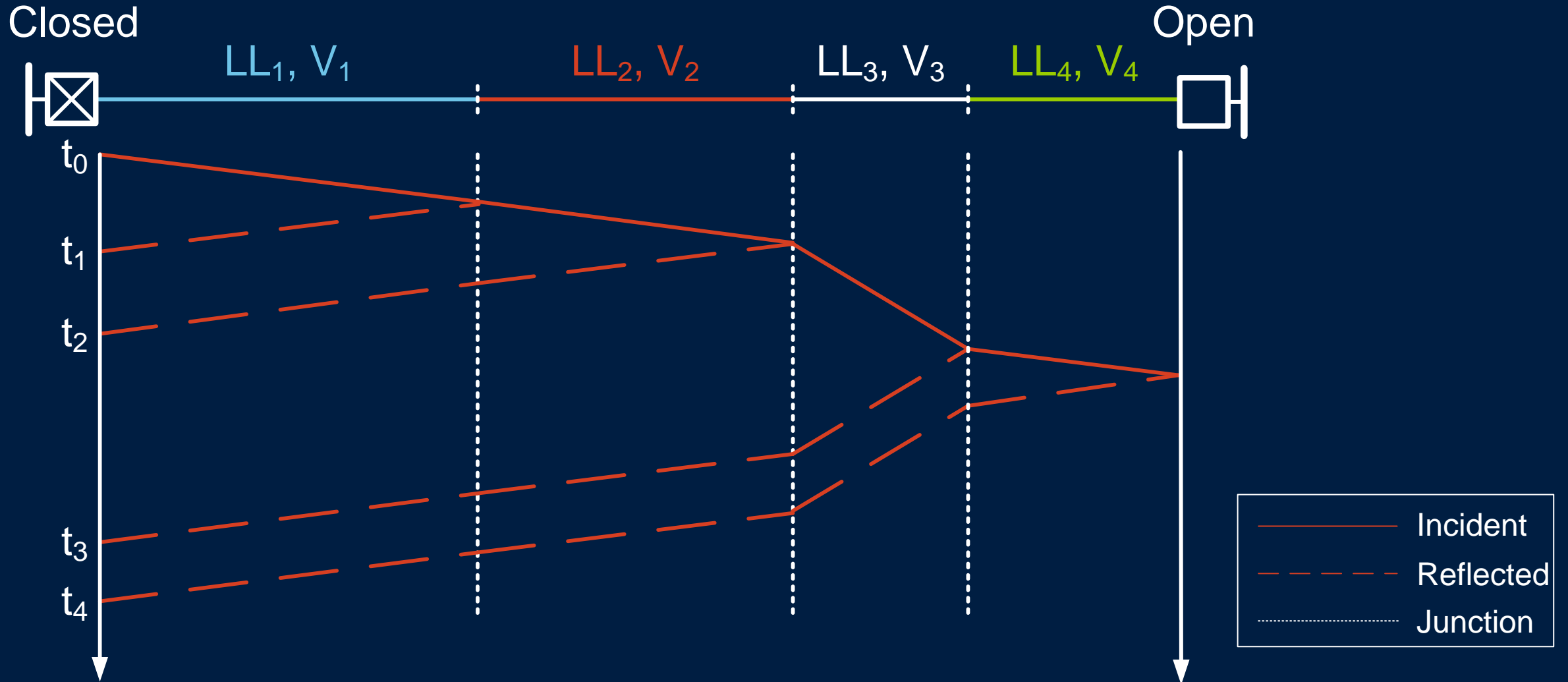
Impedance-Based Fault Locator Manufacturer A



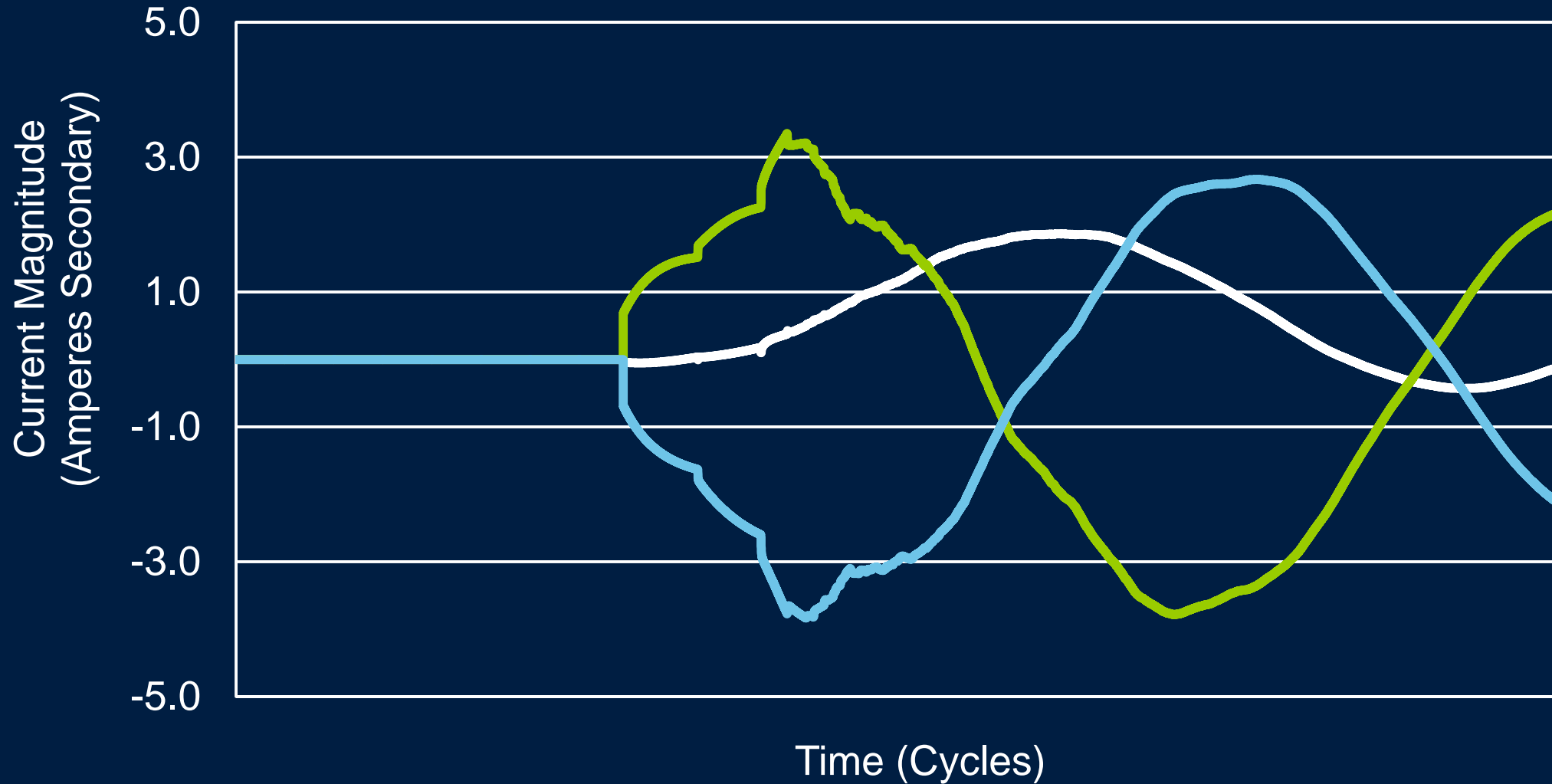
Traveling-Wave Fault Locator

- Explored to evaluate functionality on this composite line
- Simulated in non-real time
- Saved waveforms and replayed into the relays
- Evaluated the relay response

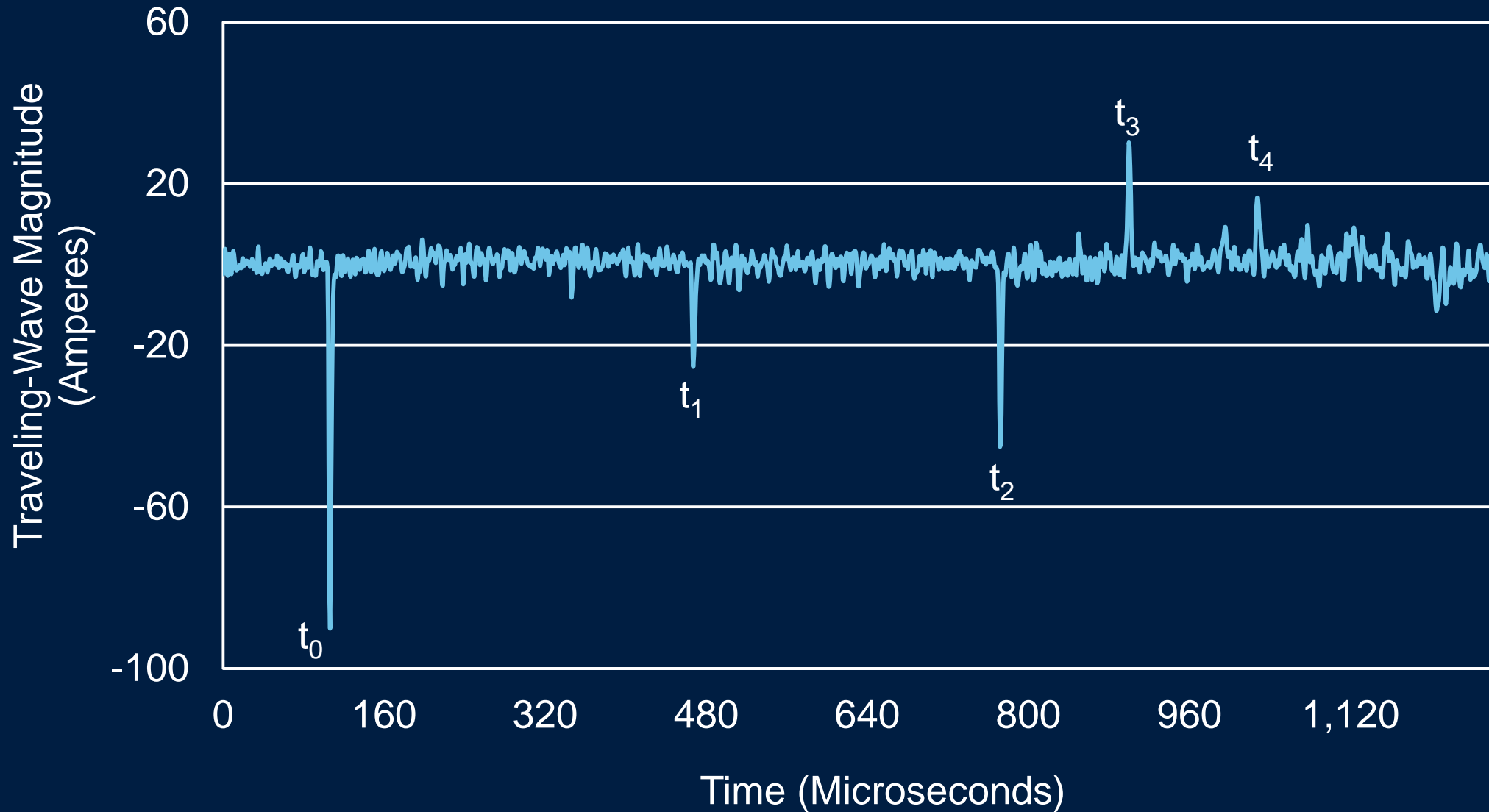
Traveling-Wave Reflections



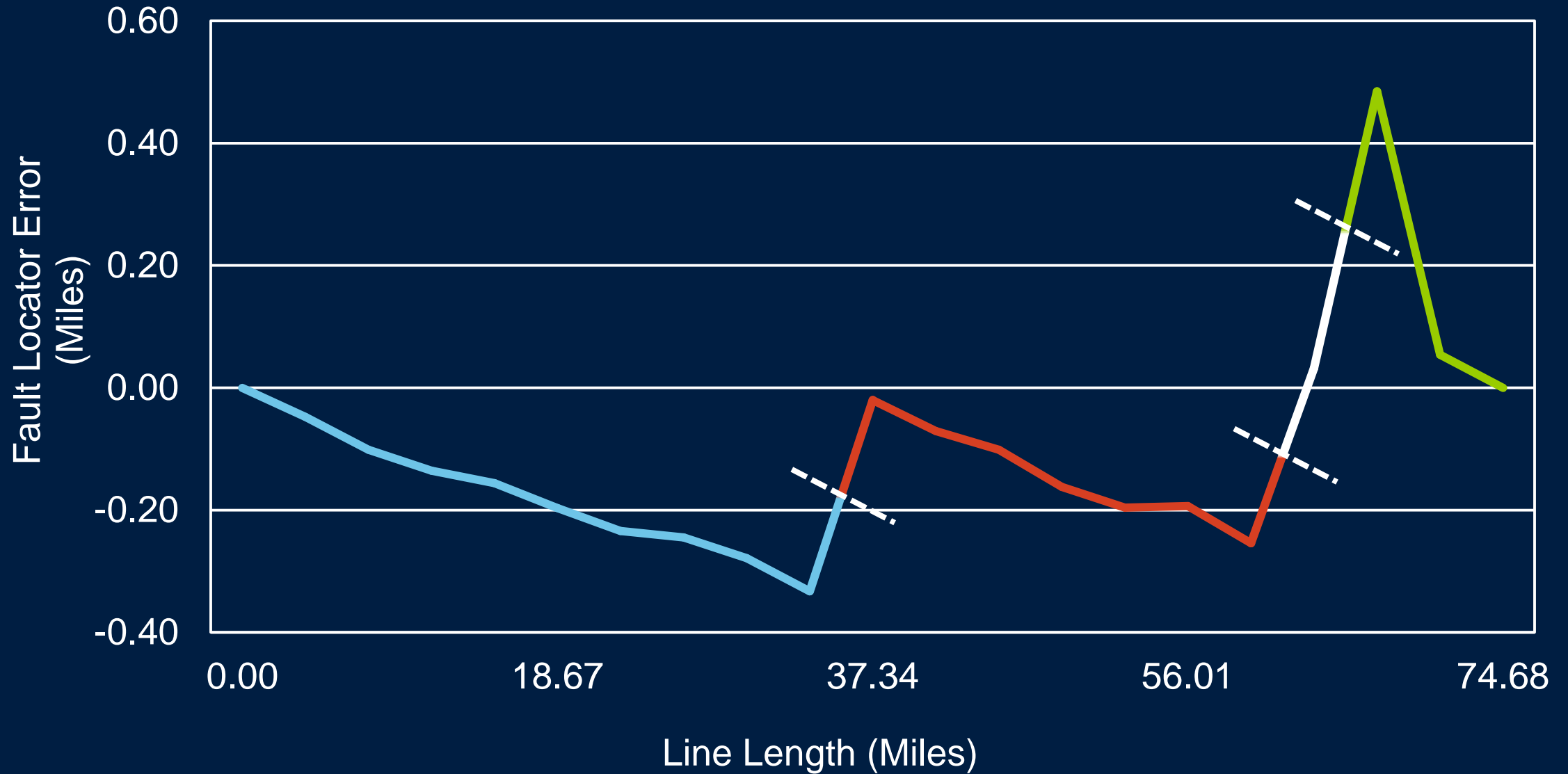
Traveling-Wave Waveform



Traveling-Wave Measurements



Traveling-Wave Fault Locator Accuracy



Summary

- Transmission line incorporated underground cables
- Protection scheme needed reevaluation to include multiple line current differential relays
- Real-time digital simulation validated relay performance



Questions?