

# Understanding Generator Stator Ground Faults and Their Protection Schemes

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# Overview

- Stator winding deterioration
- Fundamental neutral overvoltage
- Third-harmonic schemes
- Subharmonic injection

# Thermal Deterioration

Weakening of insulation when heated beyond its design temperature

Location	Cause
Overall	Overloading
	Cooling system failure
Local	High-resistance electrical connections

# Electrical Deterioration

Decomposition of insulation due to arcing

Location	Cause
Voids in the insulation	Partial discharge
Between groundwall and core	Slot discharge
End winding	Surface tracking

# Mechanical Deterioration

Insulation wear or cracking due to excessive movement or vibration

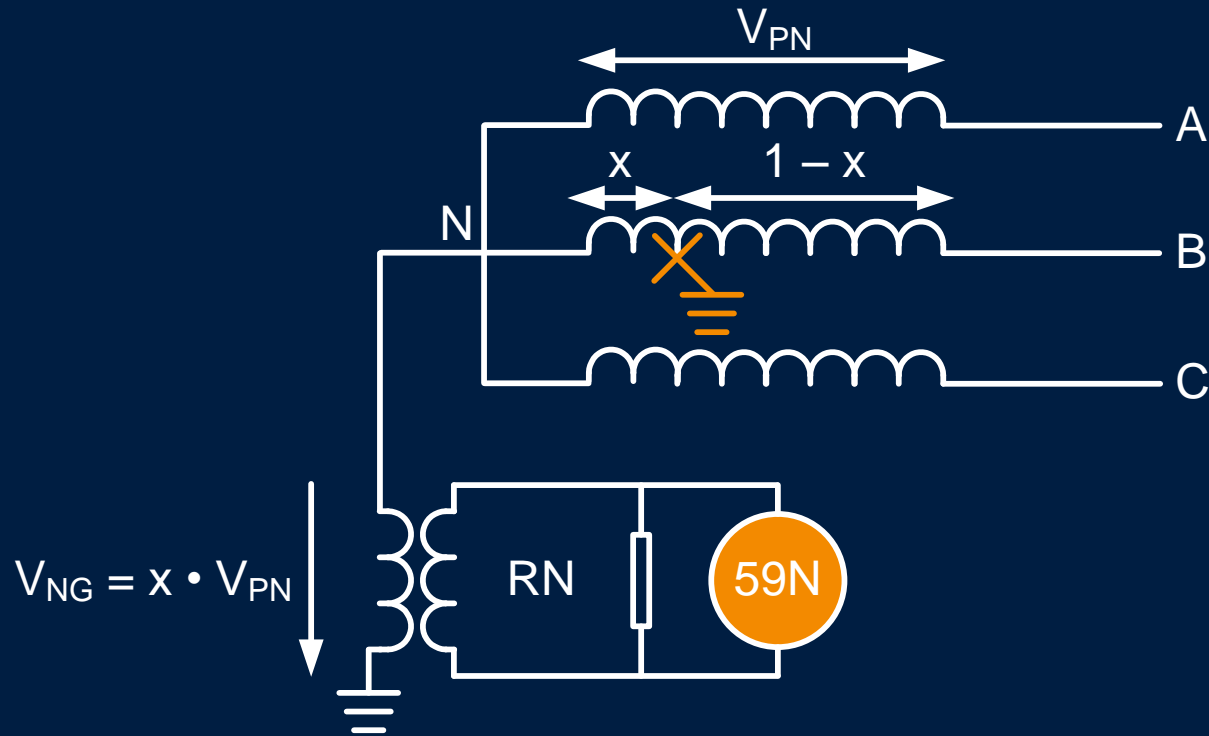
Location	Cause
Slot	Insulation shrinkage
	Poor construction
	Thermal cycling
End winding	Inadequate bracing
	Transient torque event

# Environmental Deterioration

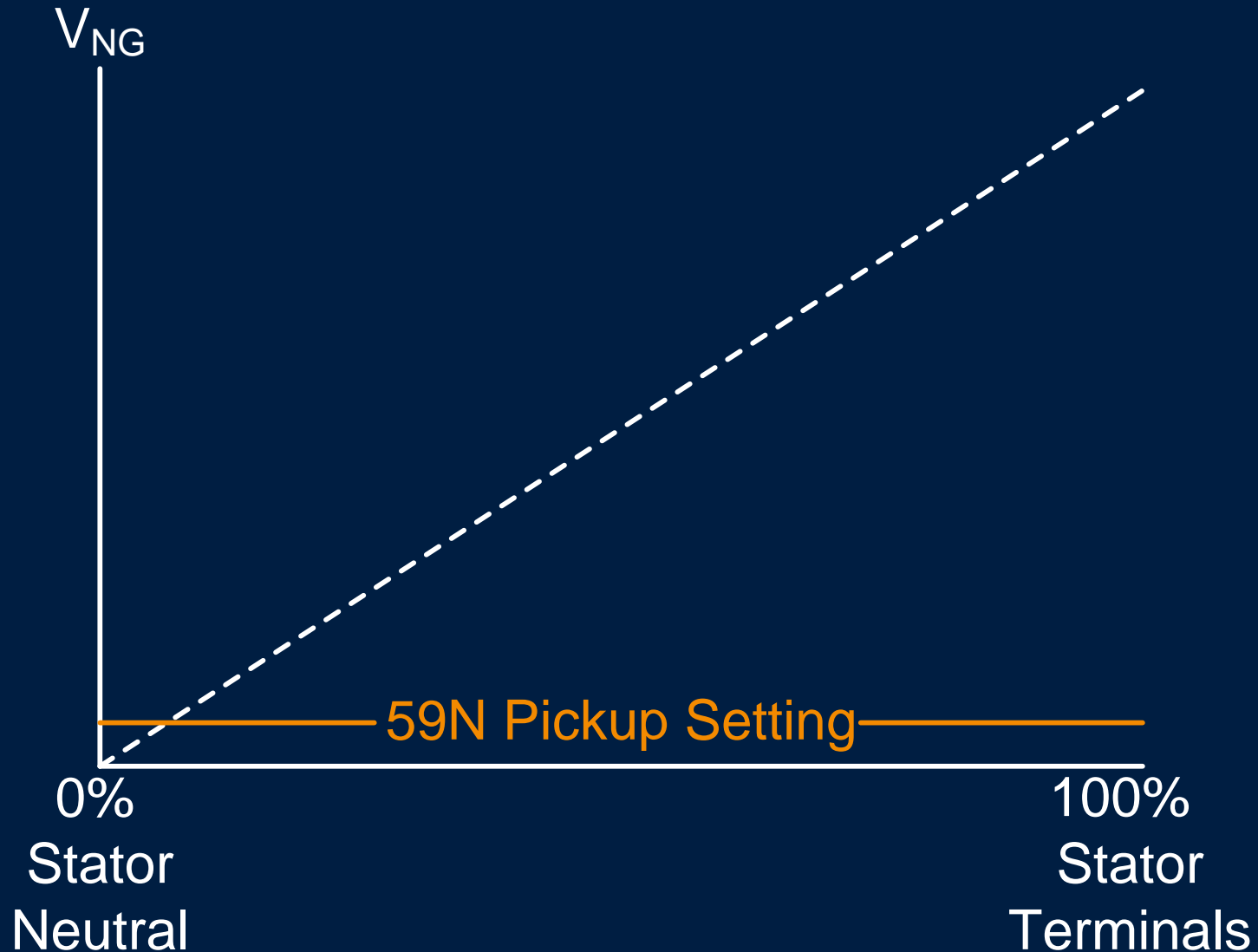
Reduces electrical or mechanical insulation strength, provides medium for surface tracking

Location	Cause
End Winding	Water
	Oil
	Dust

# Fundamental Neutral Overvoltage

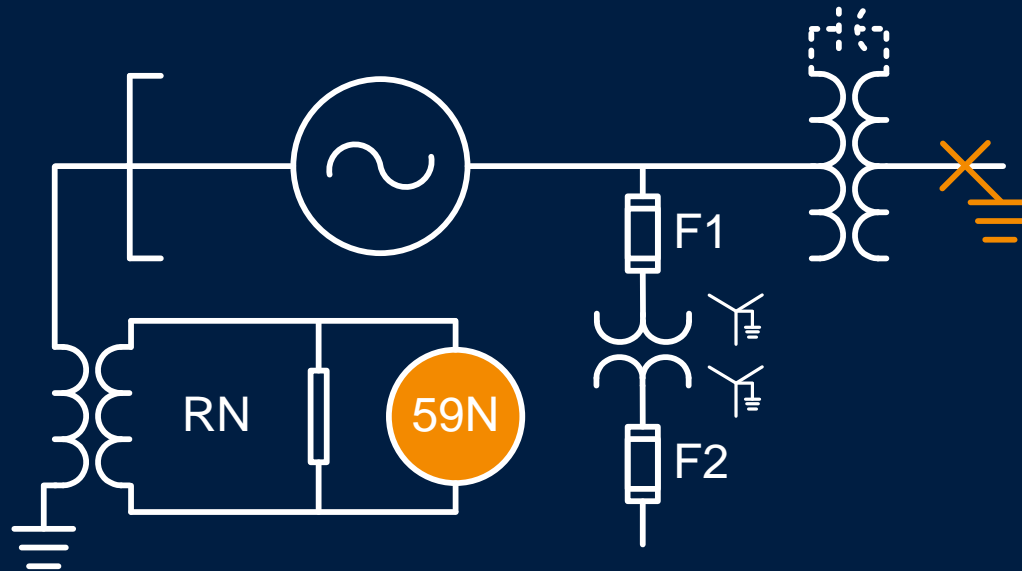


# Coverage Is Proportional to Location

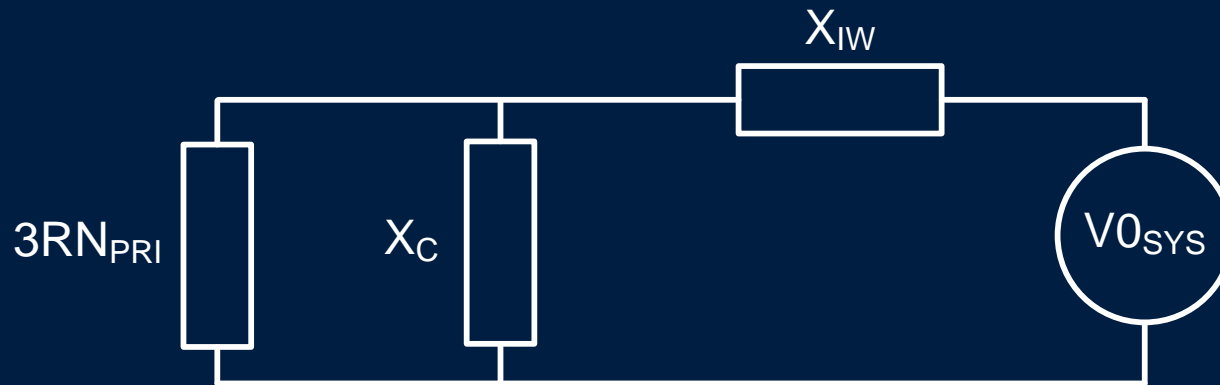




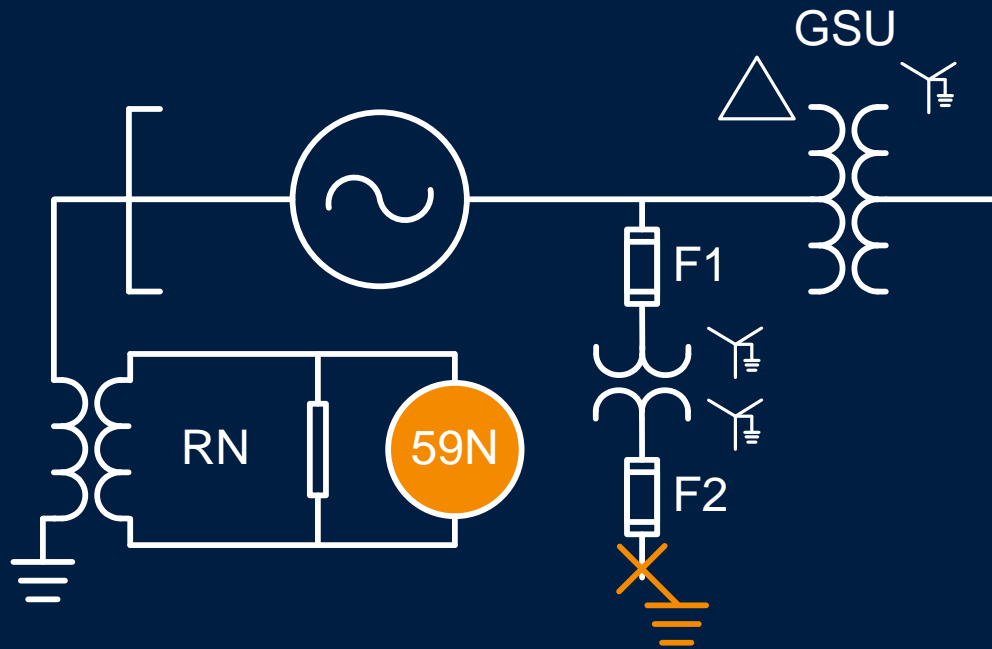
# Response to GSU High-Voltage Ground Fault



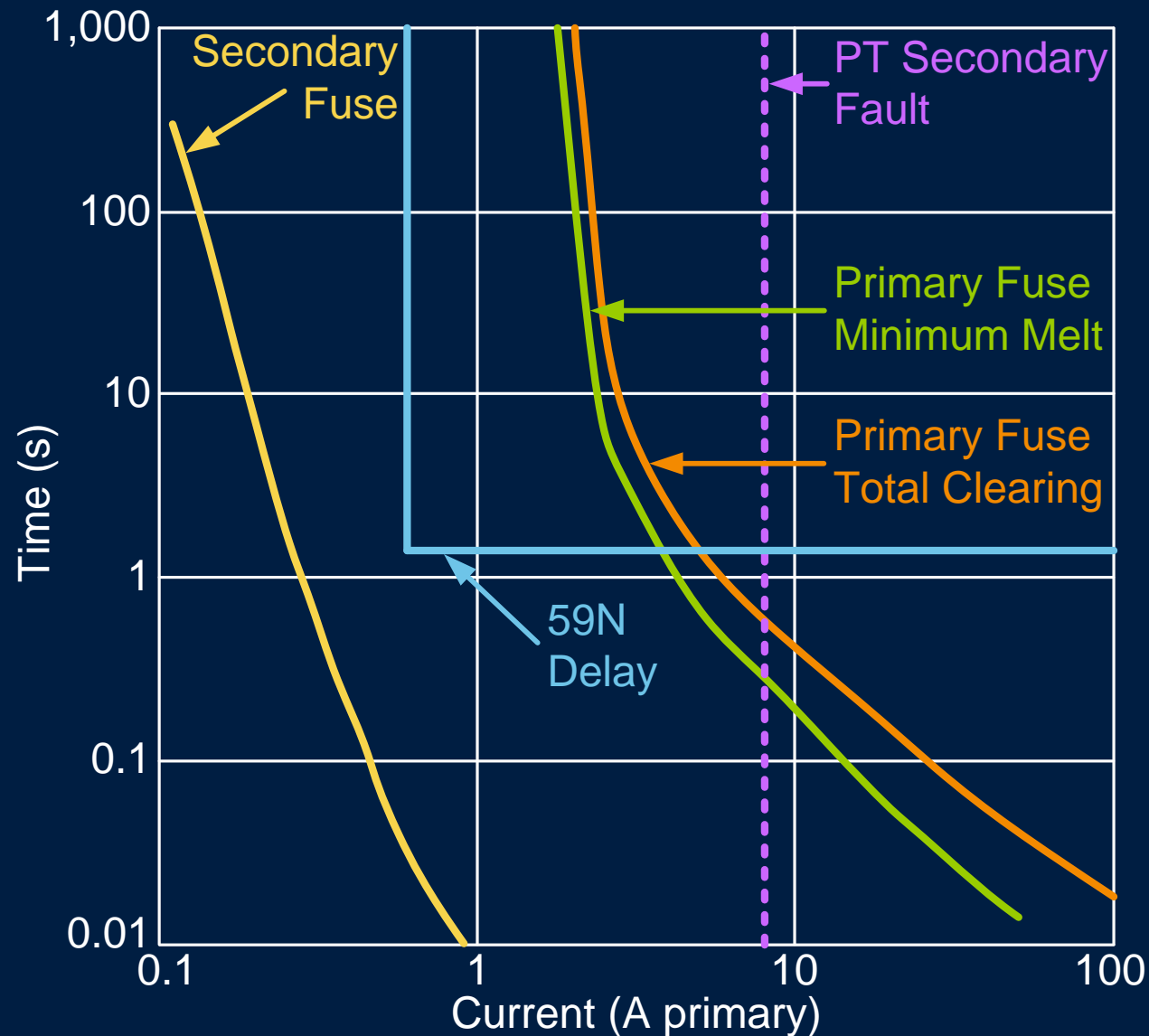
# GSU High-Voltage Ground Equivalent Circuit



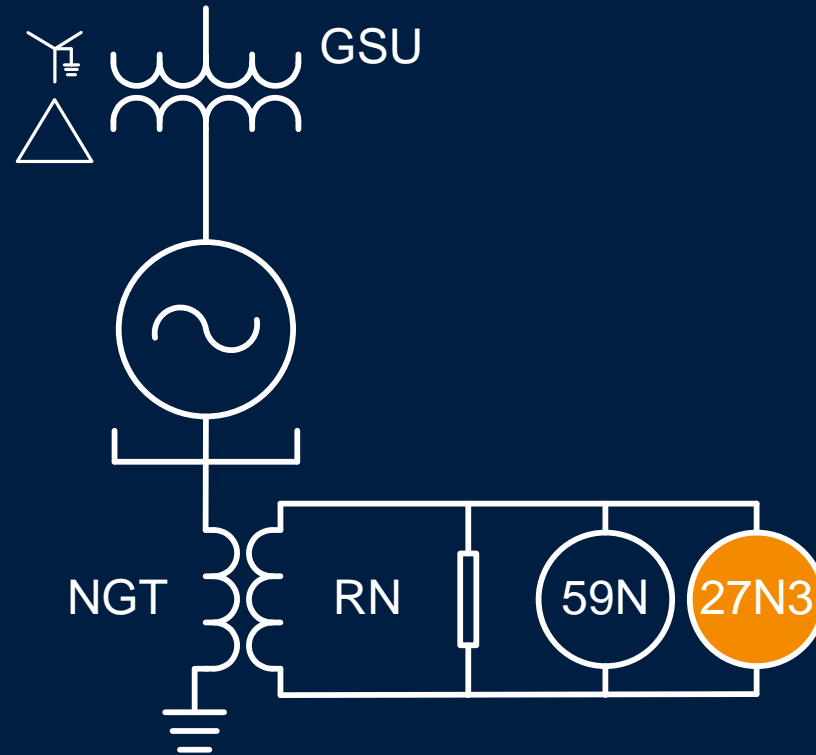
# PT Secondary Fault



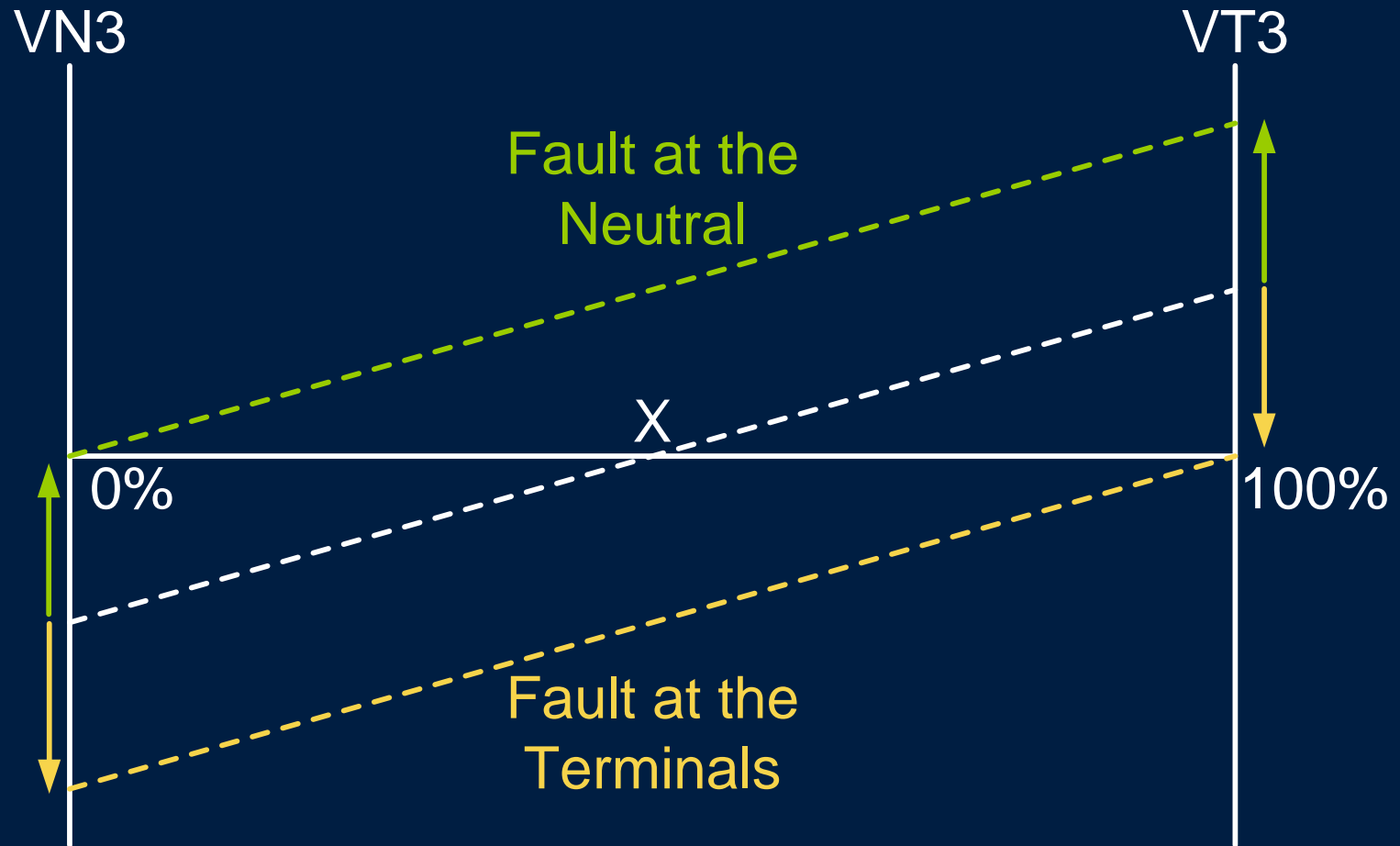
# Coordination of 59N With PT Fuses



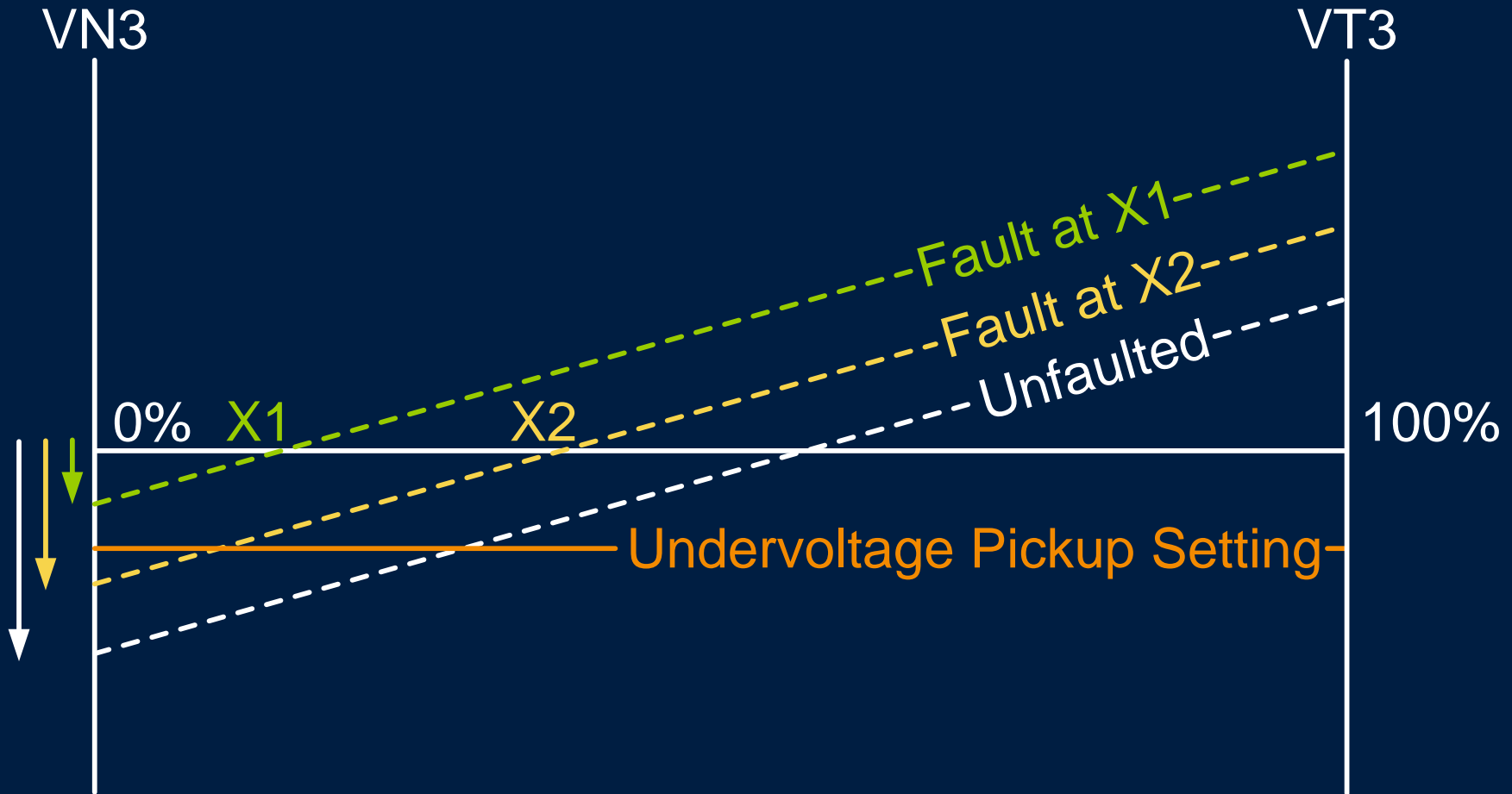
# Third-Harmonic Neutral Undervoltage



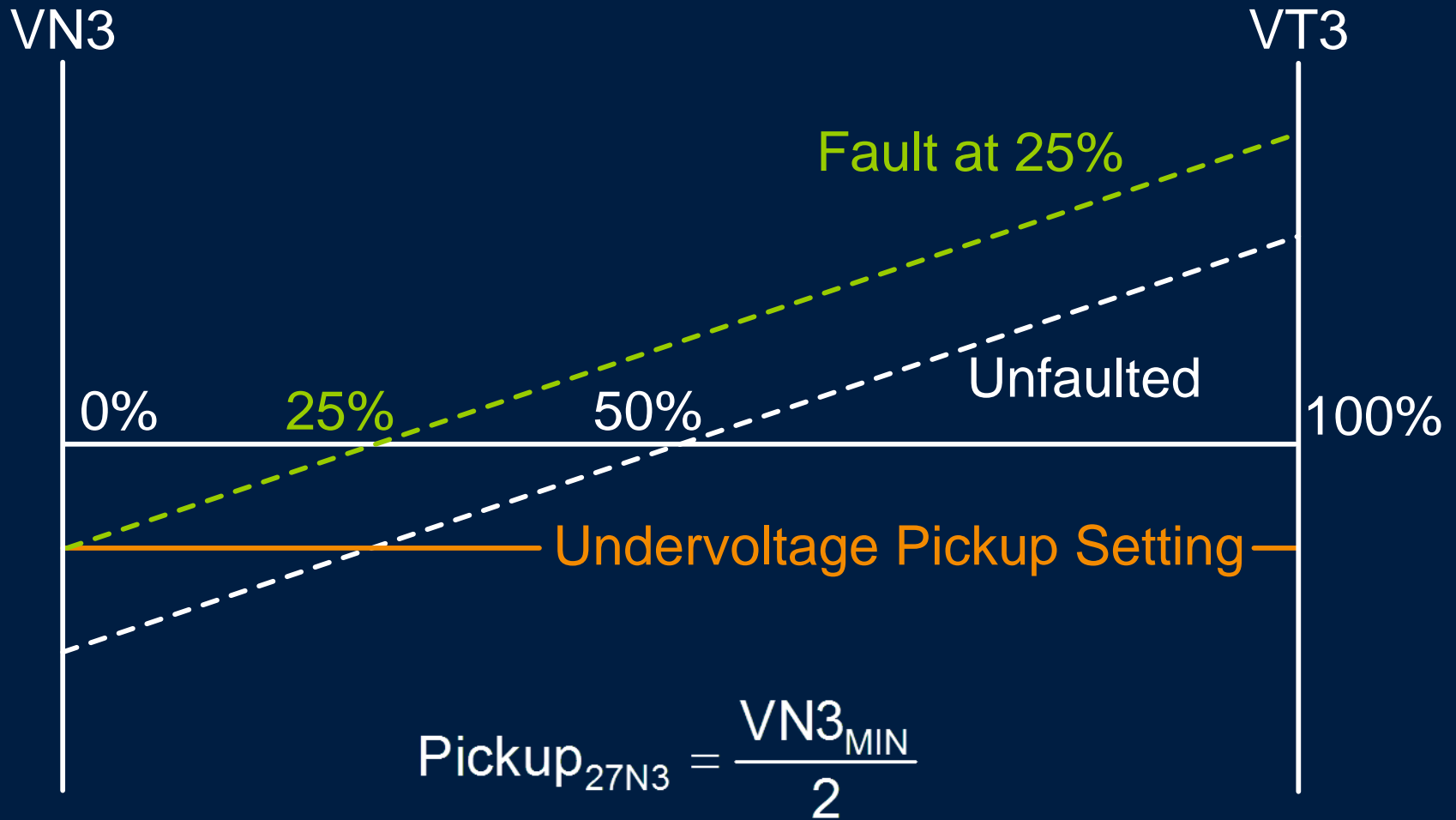
# Distribution of Third Harmonic



# VN3 for Faults at X1 and X2

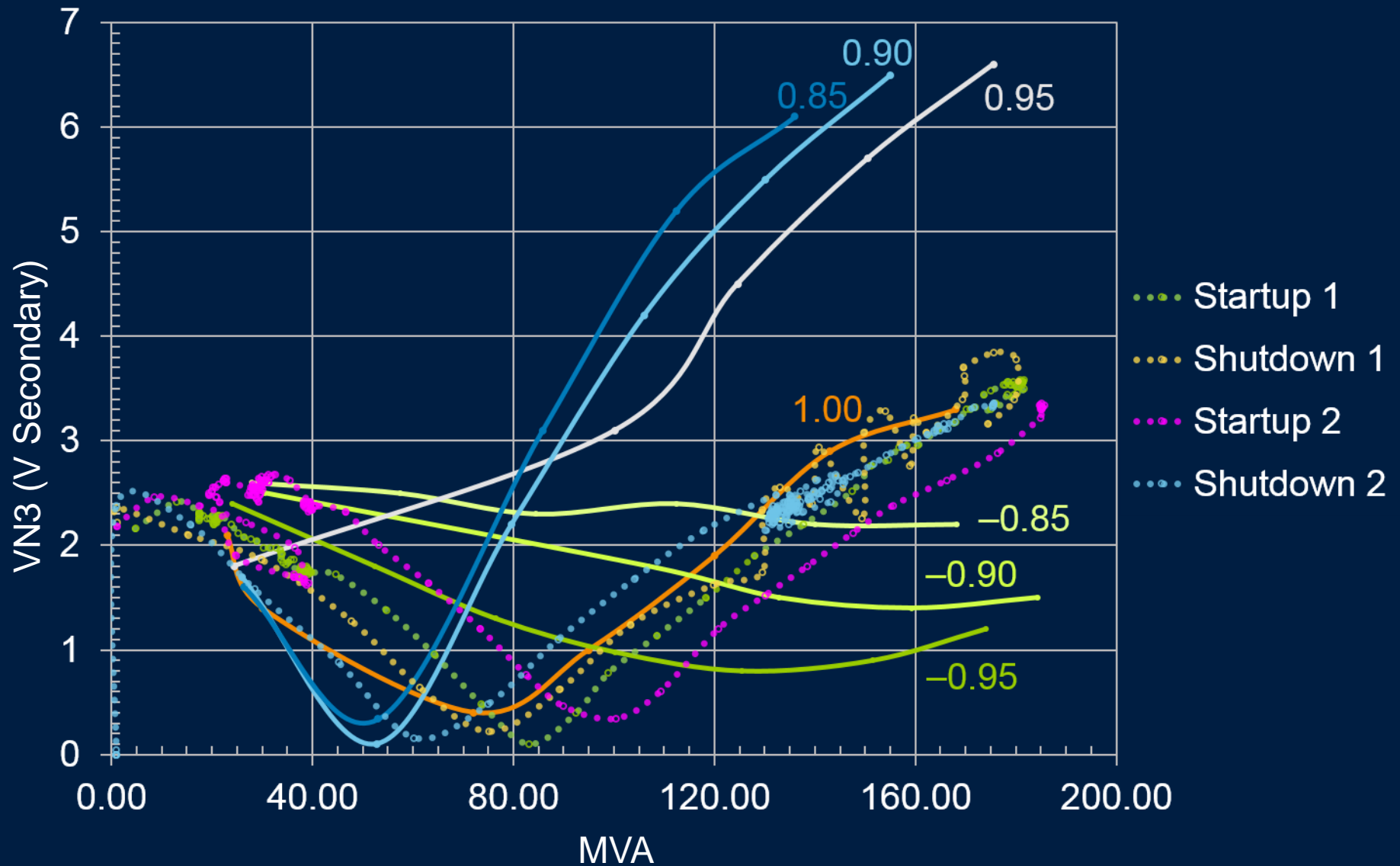


# Setting the 27N3 Pickup

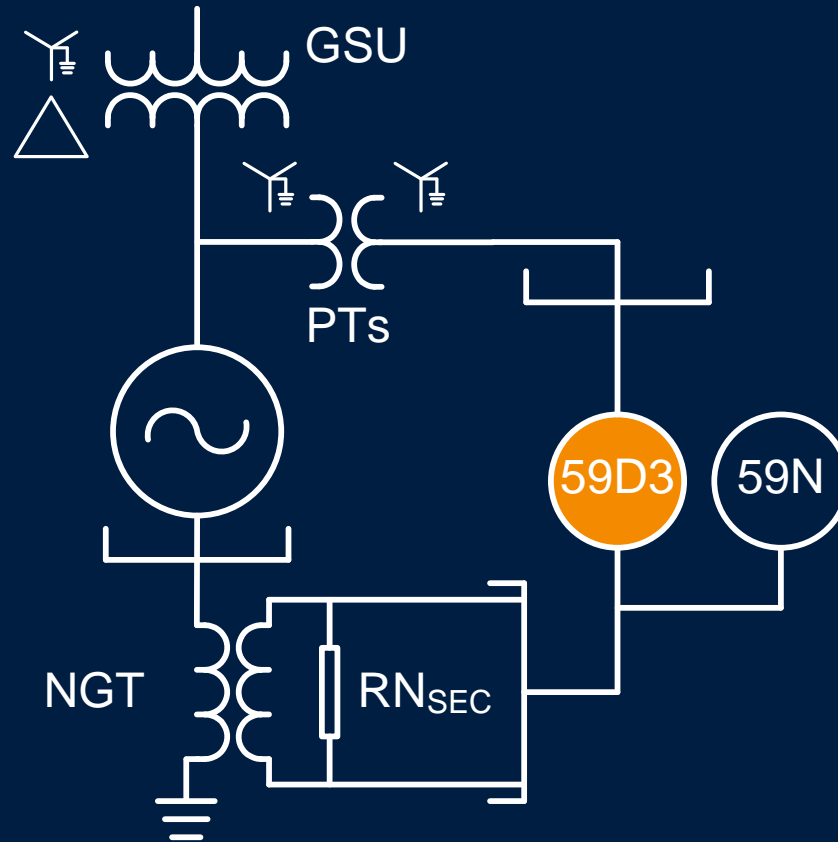




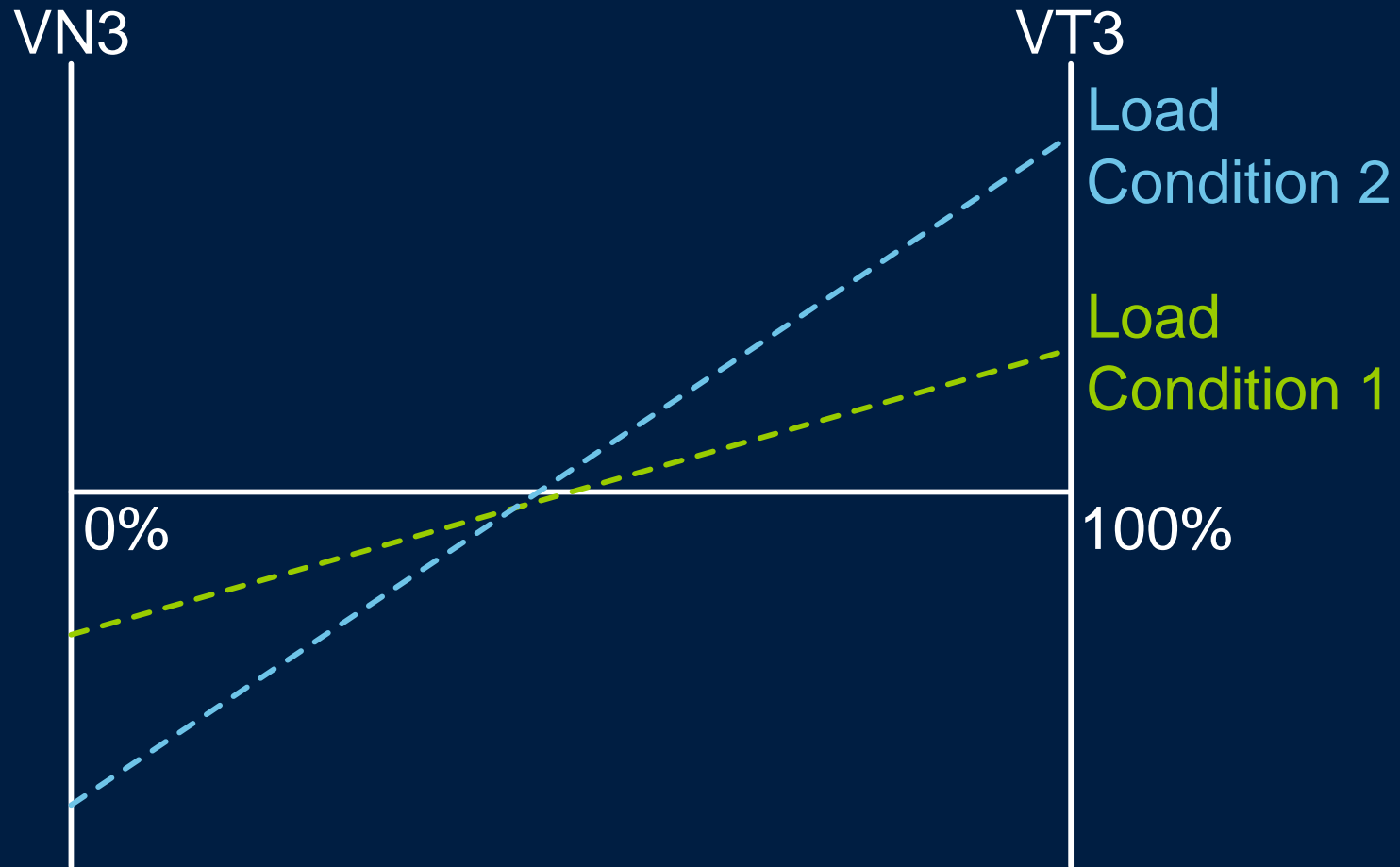
# Third-Harmonic Survey



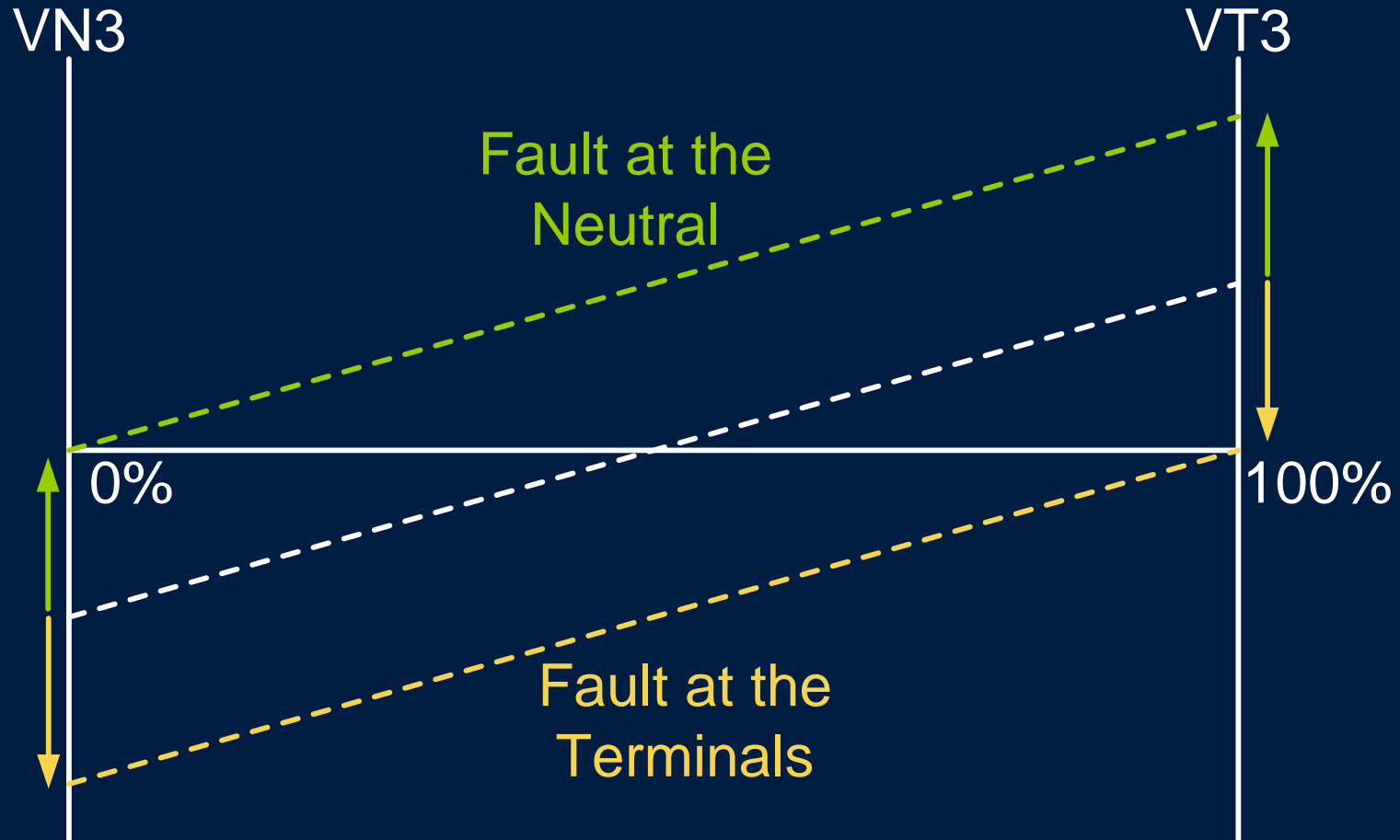
# Third-Harmonic Differential



# Third-Harmonic Ratio Is Not Sensitive to Load Changes



# Distribution Shift Due to Fault



# Setting the 59D3

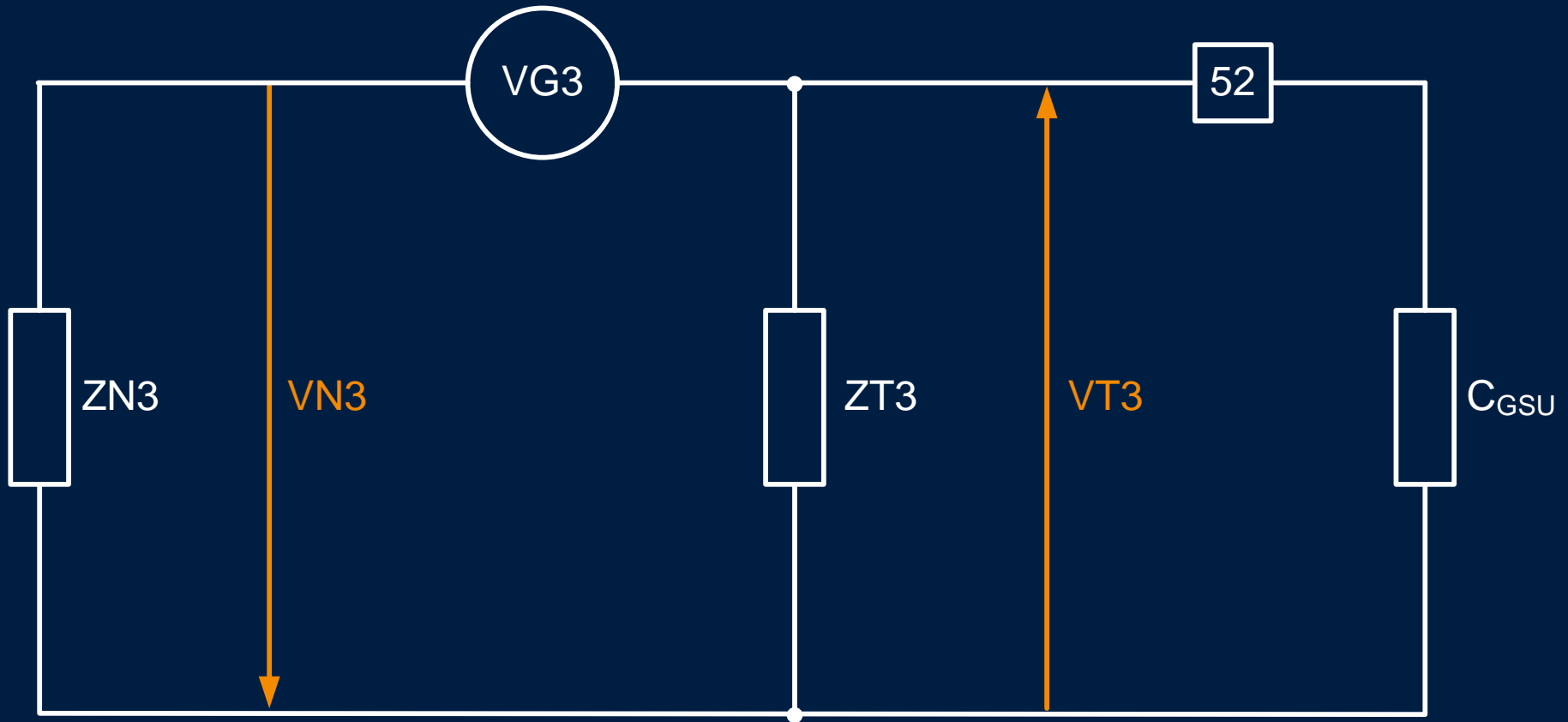
$$OP = \left\| VN3\_SEC - RAT \mid VT3\_SEC \right\| > PKP$$

$$RAT = \frac{\sum_{n=1}^N VN3\_SEC_n}{\sum_{n=1}^N VT3\_SEC_n}$$

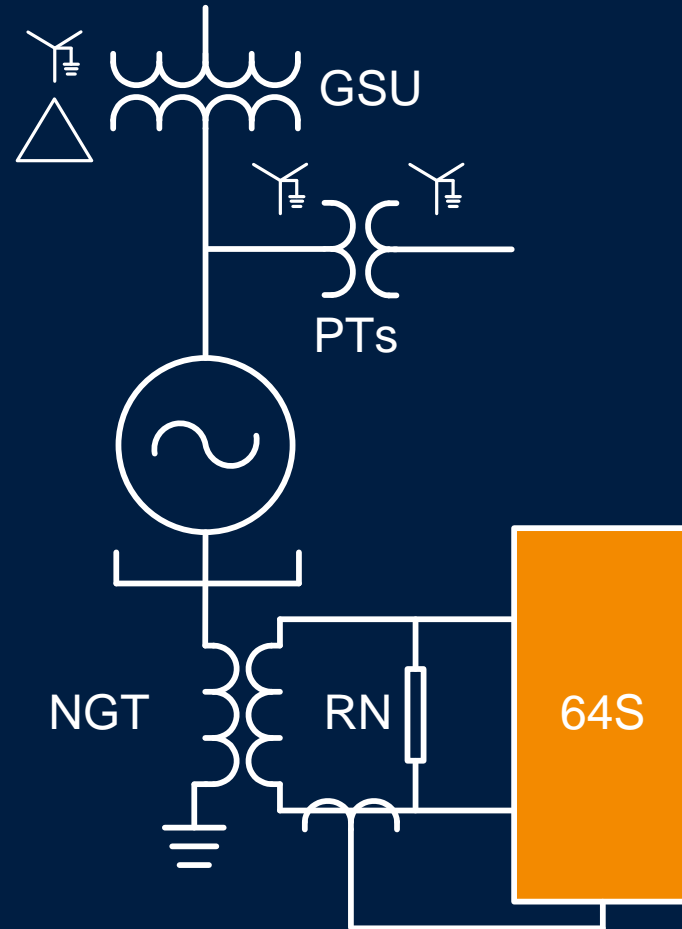
$$Pickup_{59D3} = 1.1 \left( 0.1 + MAX_n \left\{ \left\| VN3\_SEC_n - RAT \mid VT3\_SEC_n \right\| \right\} \right)$$

where N is the number of measurements

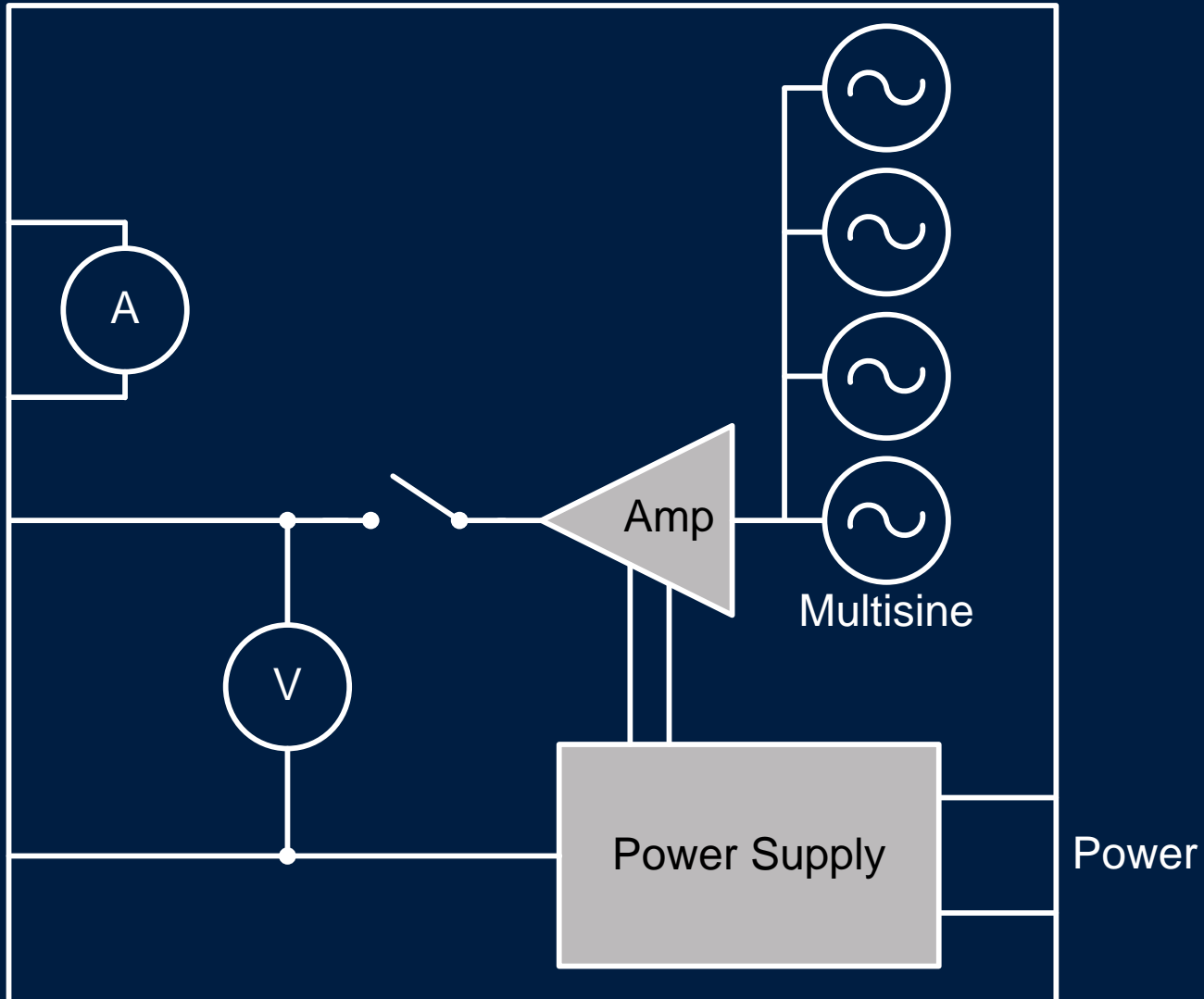
# Influence of Low-Side Breaker



# Subharmonic Injection

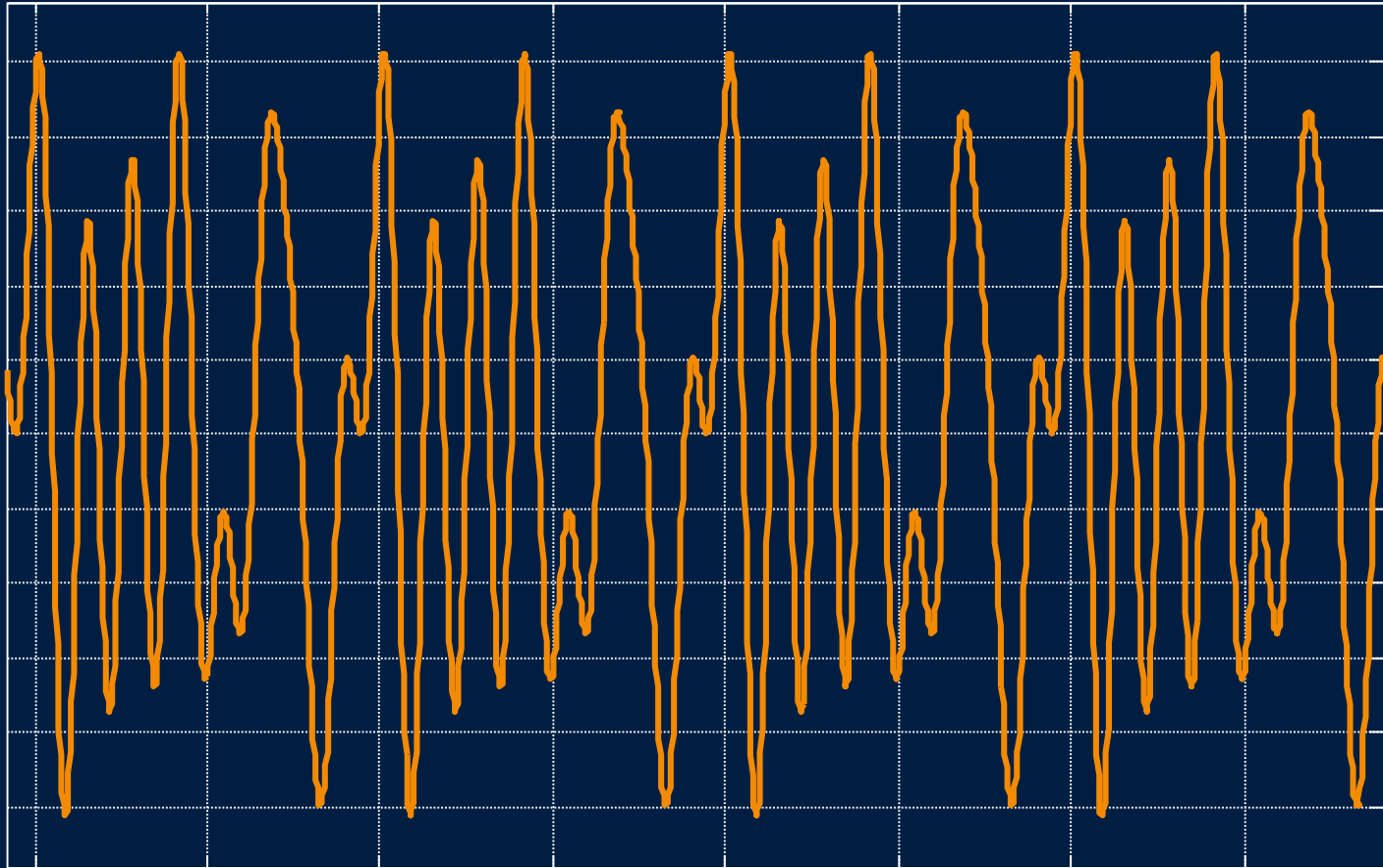


# Injection Source



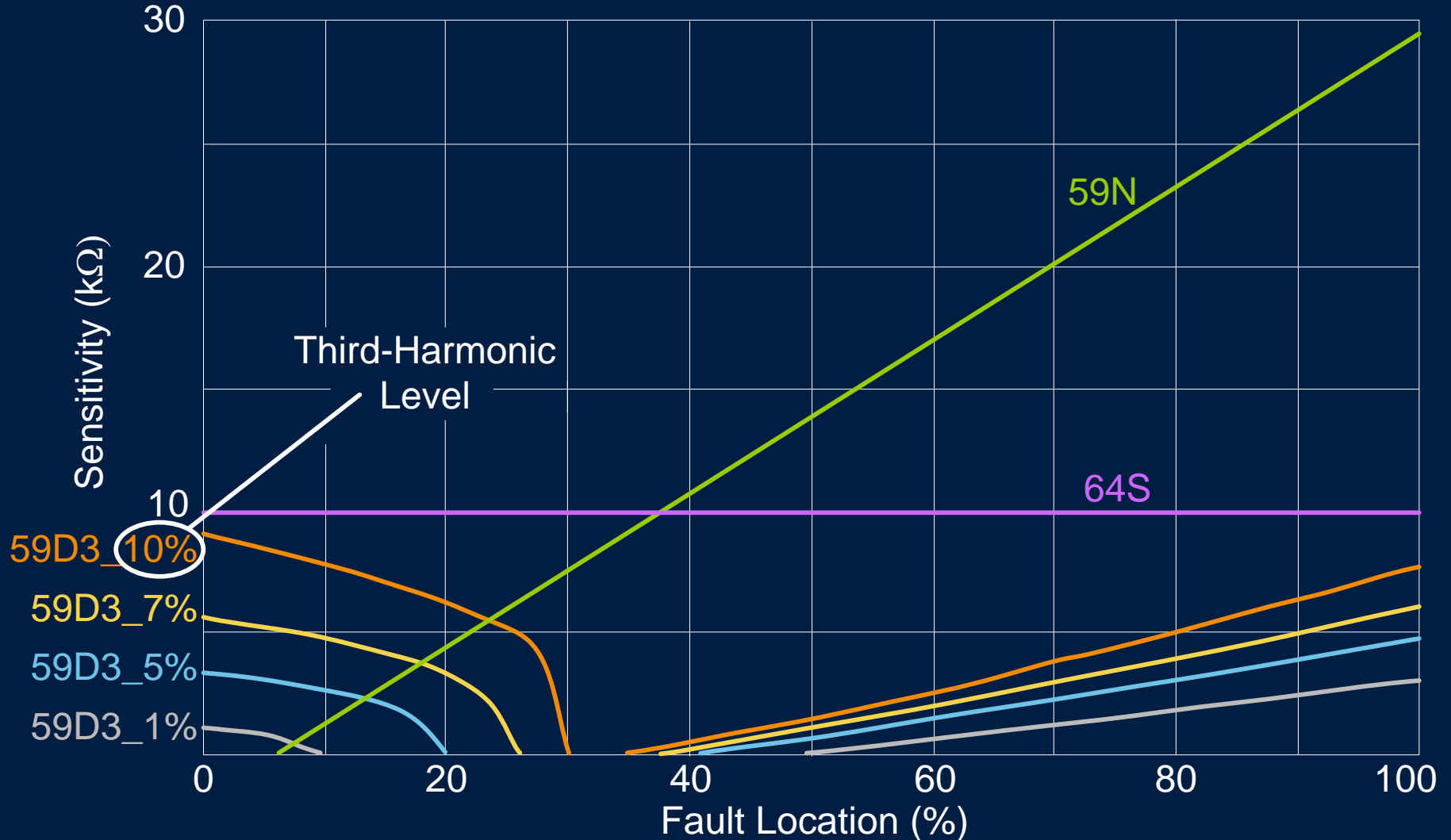


# Multisine

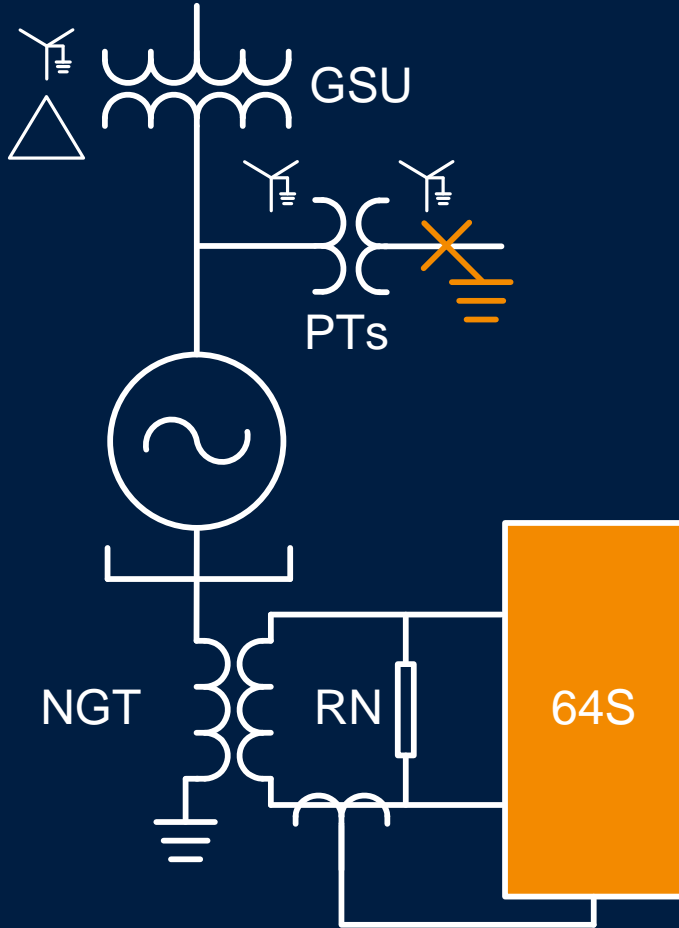


Injection of multiple sources allows  
application of redundant 64S units

# 64S Coverage Does Not Depend on Location



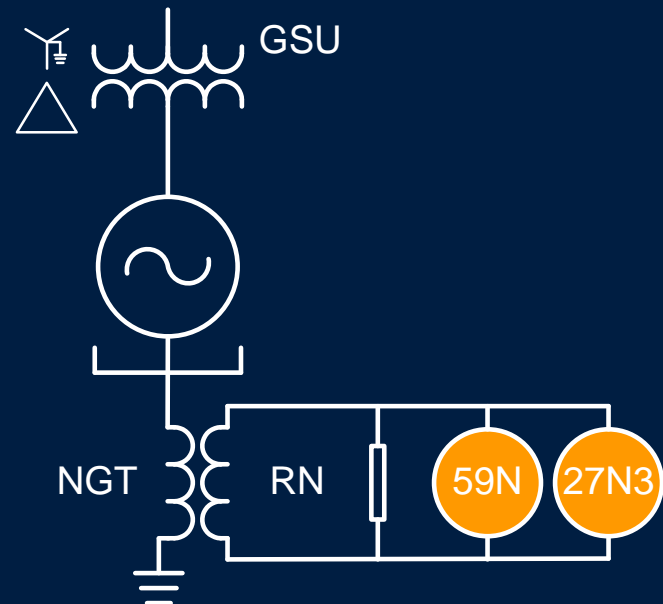
# PT Secondary Ground



Test	Insulation (kΩ)
Unit offline	59.2
PT ground, X phase	8.57
PT ground, Y phase	8.11
PT ground, Z phase	8.05

# Conclusions

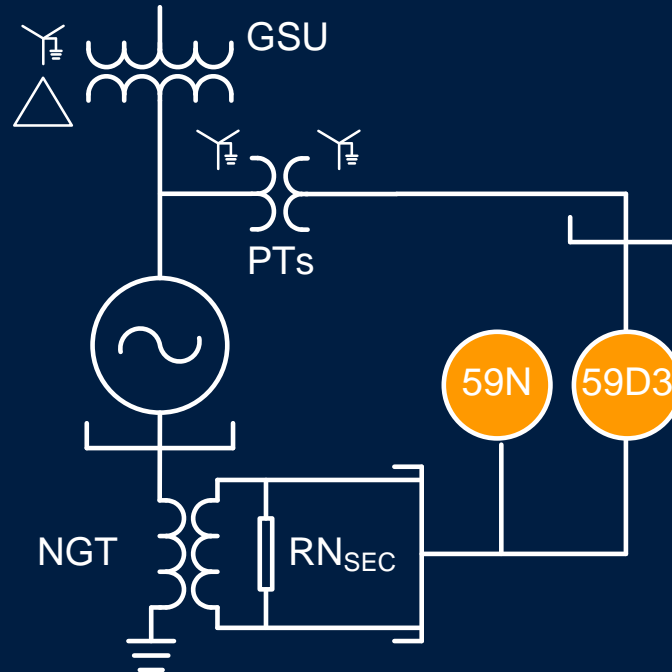
- 59N protects ~95% of winding (need to consider system and PT faults)
- 27N3 can protect remaining 5% (can be challenging to set)



# Conclusions

## 59N3 Can Protect Remaining 5%

- Requires grounded-wye PT
- Is easier to set



# Conclusions

## 64S Can Protect Entire Winding

- Requires extra hardware
- Is straightforward to set
- Works at standstill and starting
- Is applicable to parallel generators



# Questions?

