

Understanding Generator Stator Ground Faults and Their Protection Schemes

Nathan Klingerman
Duke Energy

Dale Finney, Satish Samineni,
Normann Fischer, and Derrick Haas
Schweitzer Engineering Laboratories, Inc.

Overview

- Stator winding deterioration
- Fundamental neutral overvoltage
- Third-harmonic schemes
- Subharmonic injection

Thermal Deterioration

Weakening of insulation when heated beyond its design temperature

Location	Cause
Overall	Overloading
	Cooling system failure
Local	High-resistance electrical connections

Electrical Deterioration

Decomposition of insulation due to arcing

Location	Cause
Voids in the insulation	Partial discharge
Between groundwall and core	Slot discharge
End winding	Surface tracking

Mechanical Deterioration

Insulation wear or cracking due to excessive movement or vibration

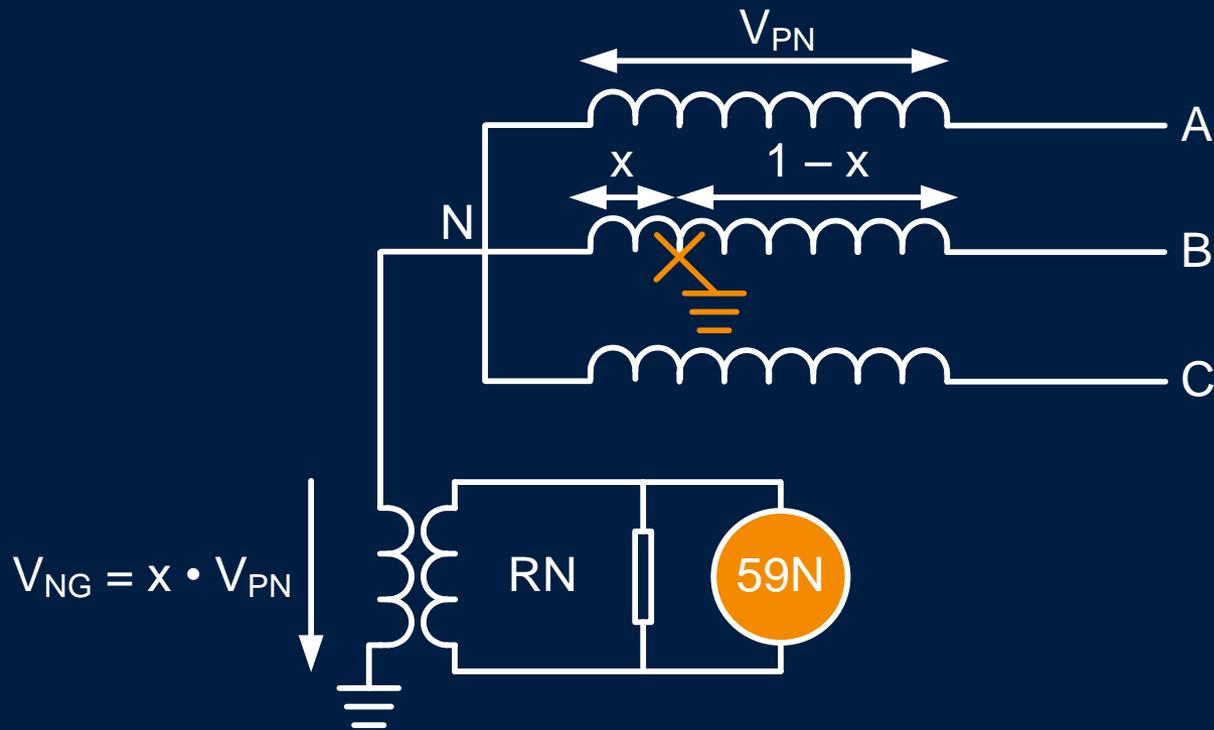
Location	Cause
Slot	Insulation shrinkage
	Poor construction
	Thermal cycling
End winding	Inadequate bracing
	Transient torque event

Environmental Deterioration

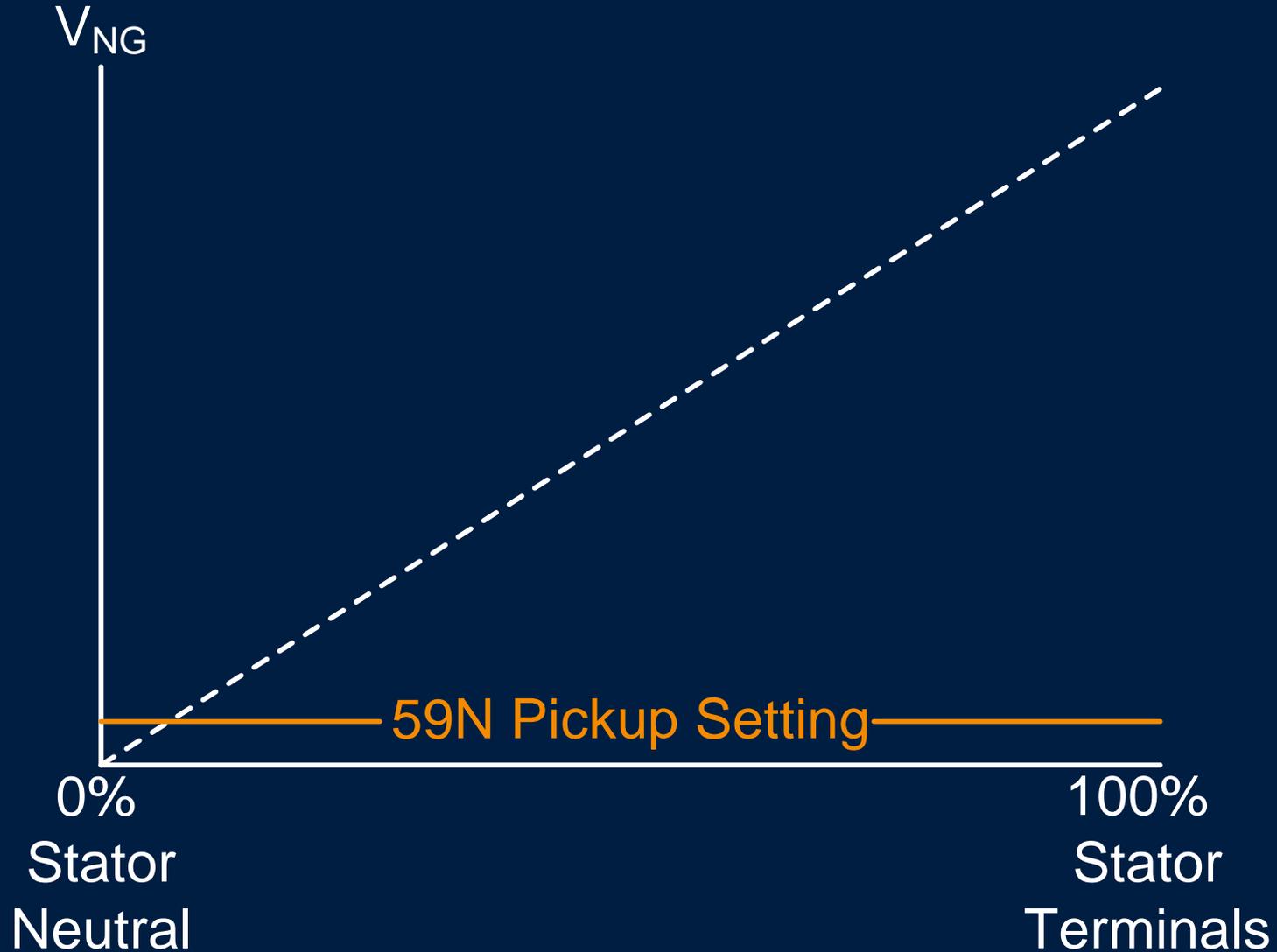
Reduces electrical or mechanical insulation strength, provides medium for surface tracking

Location	Cause
End Winding	Water
	Oil
	Dust

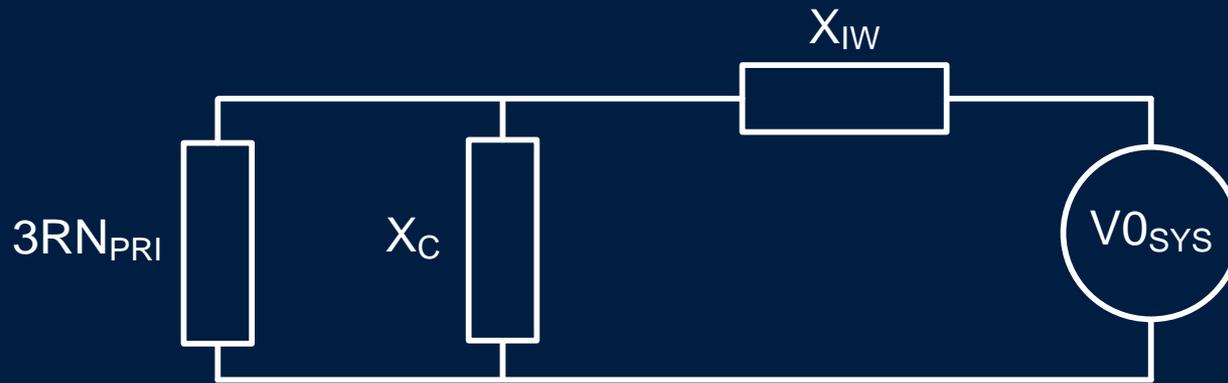
Fundamental Neutral Overvoltage



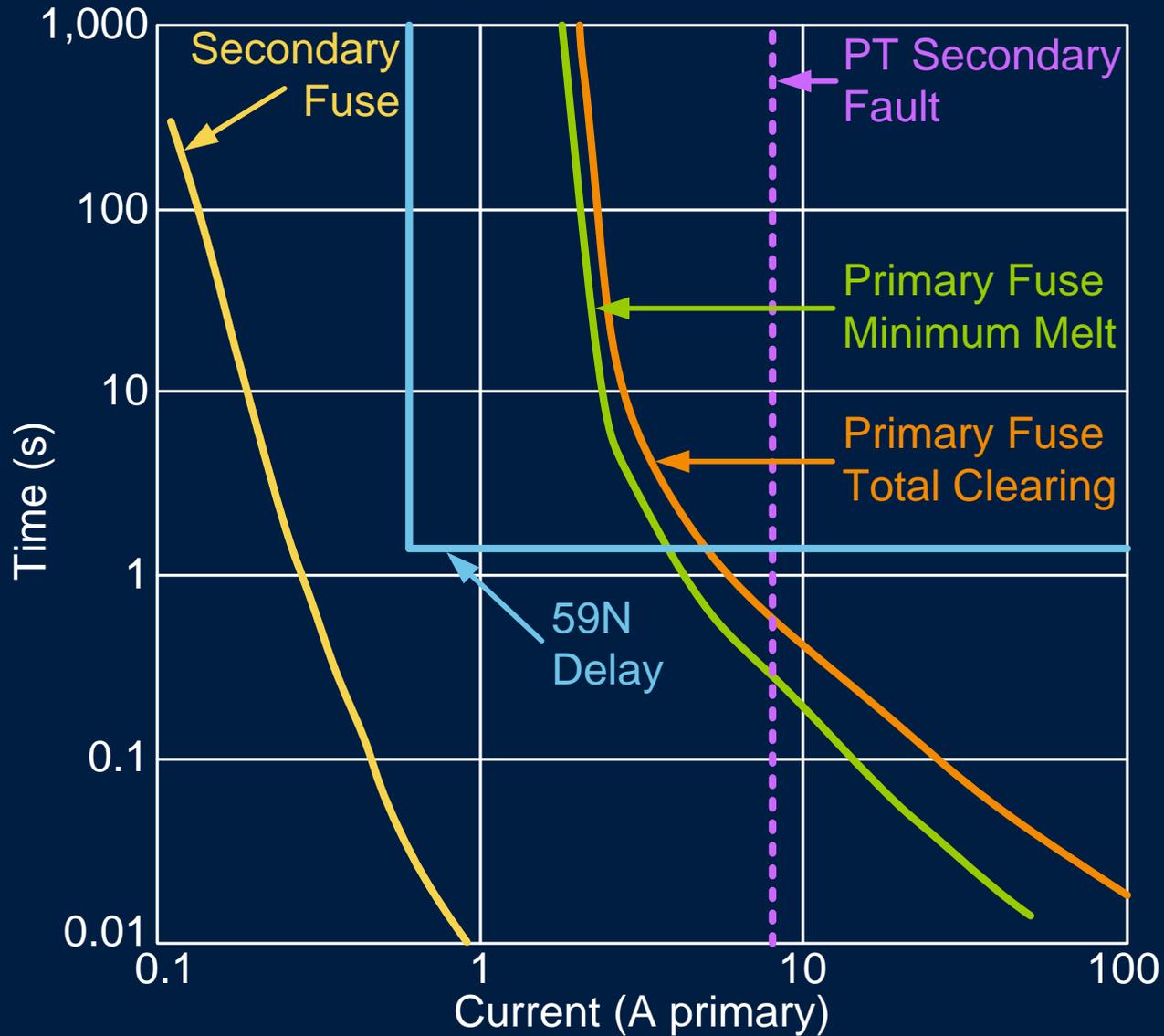
Coverage Is Proportional to Location



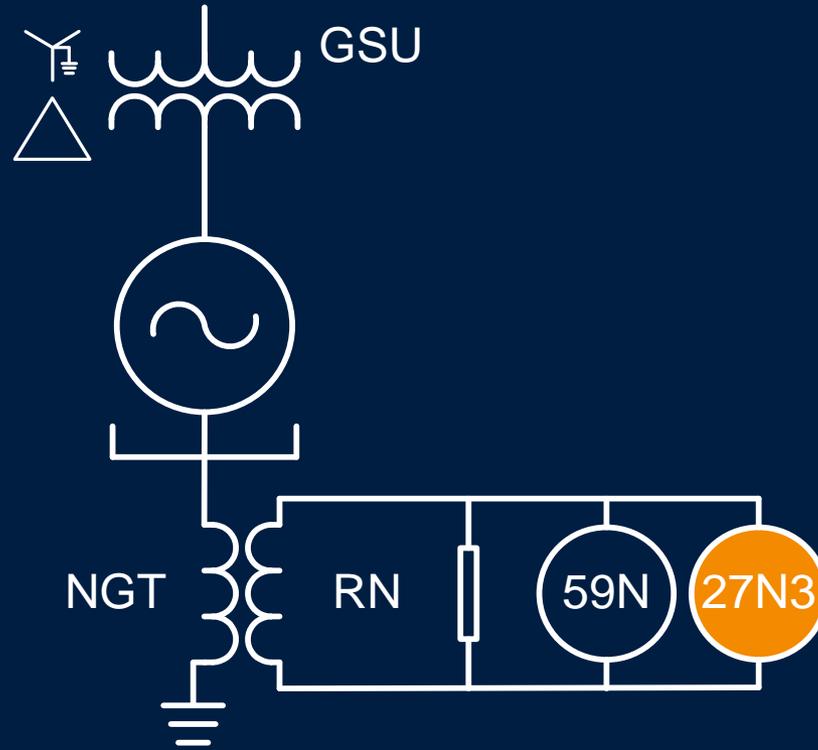
GSU High-Voltage Ground Equivalent Circuit



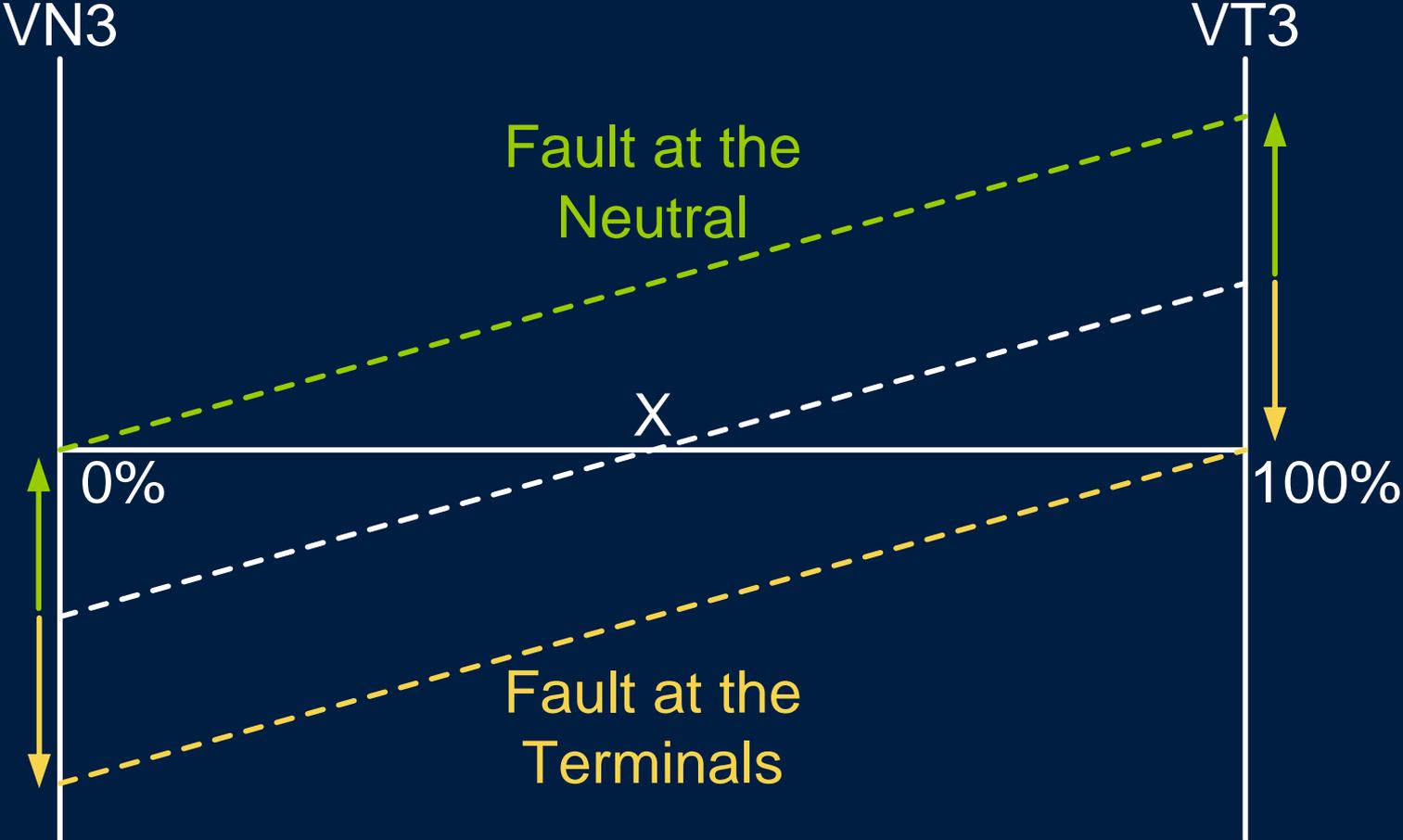
Coordination of 59N With PT Fuses



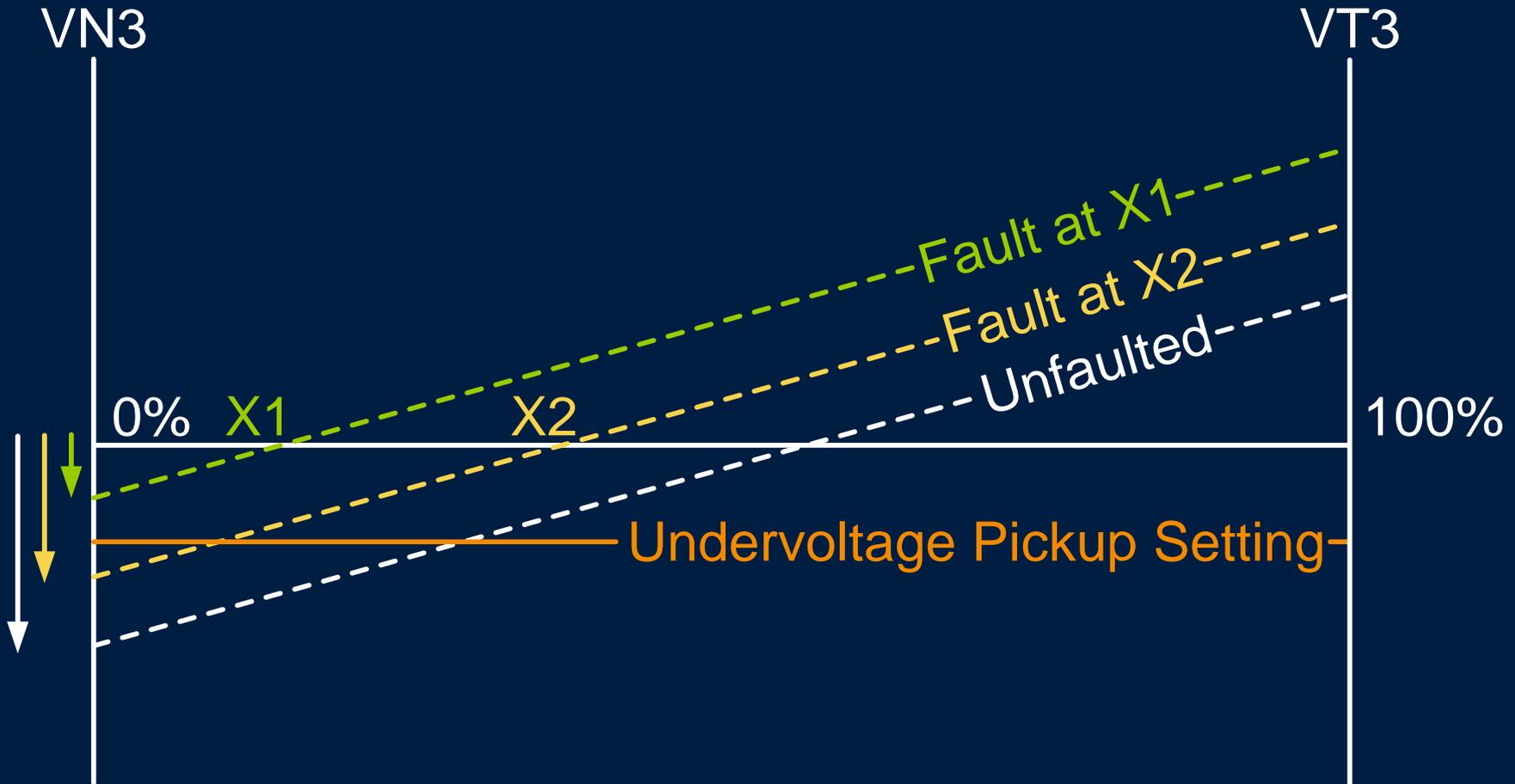
Third-Harmonic Neutral Undervoltage



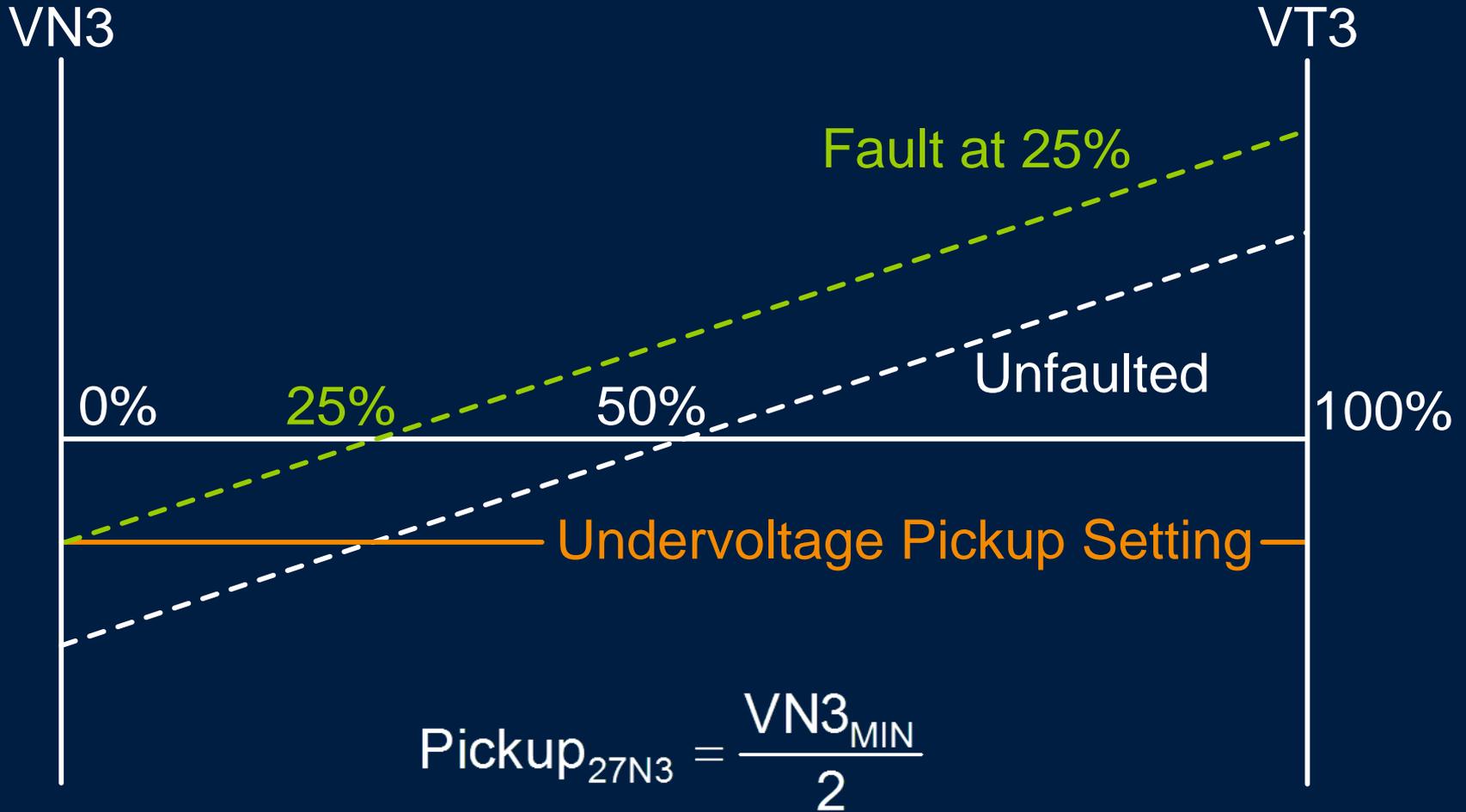
Distribution of Third Harmonic



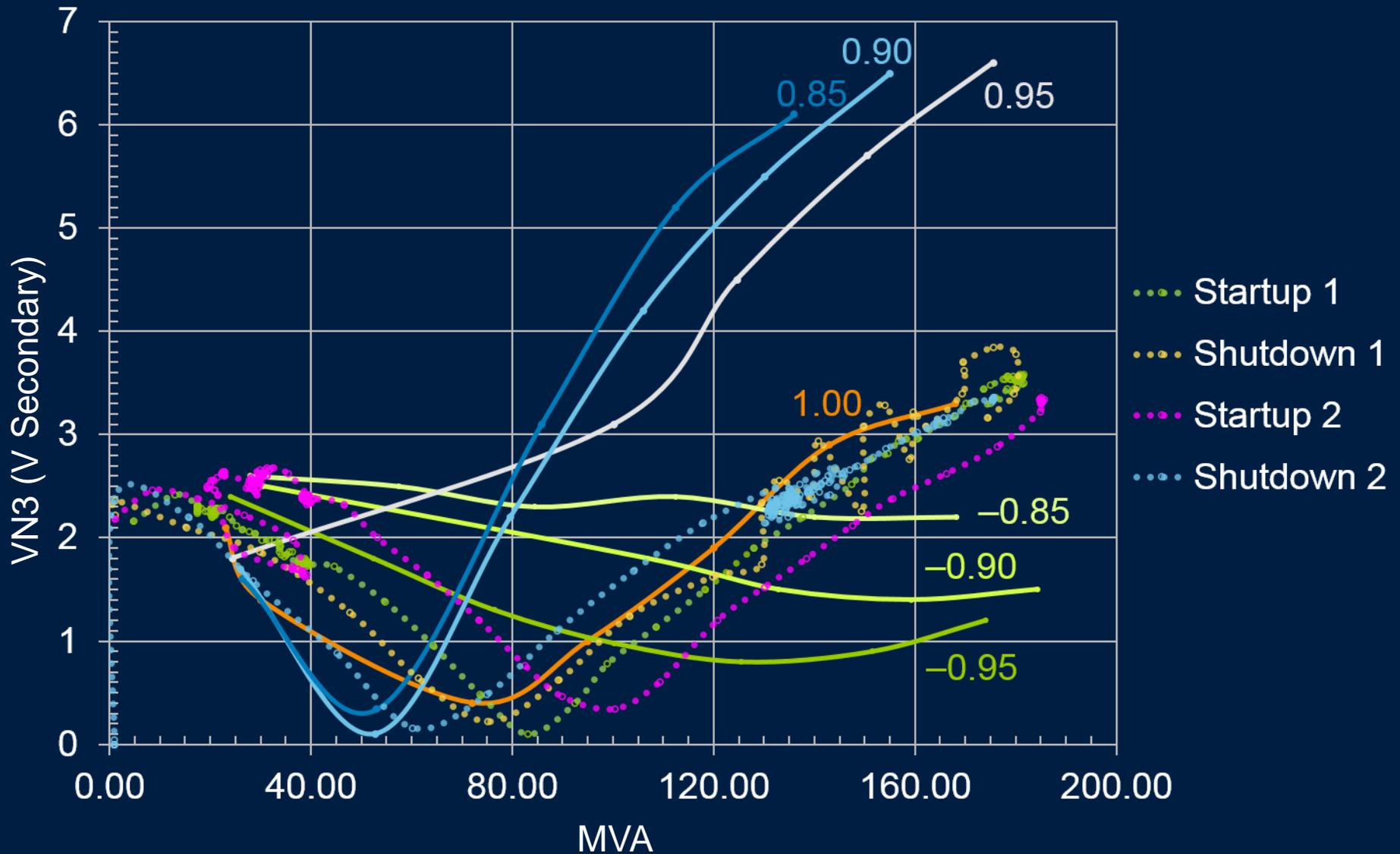
VN3 for Faults at X1 and X2



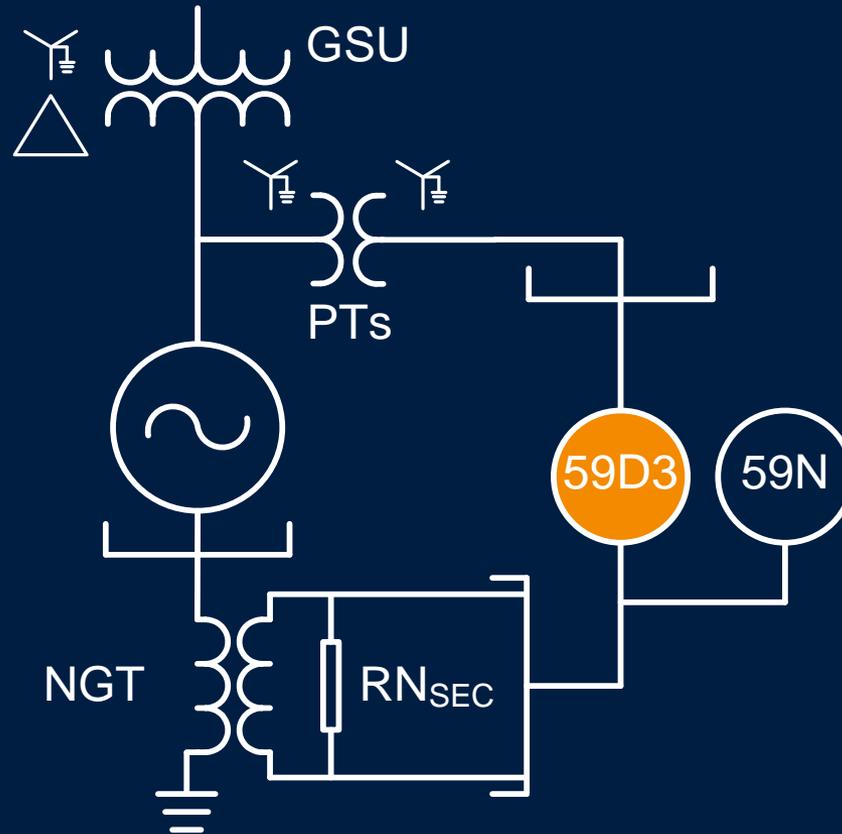
Setting the 27N3 Pickup



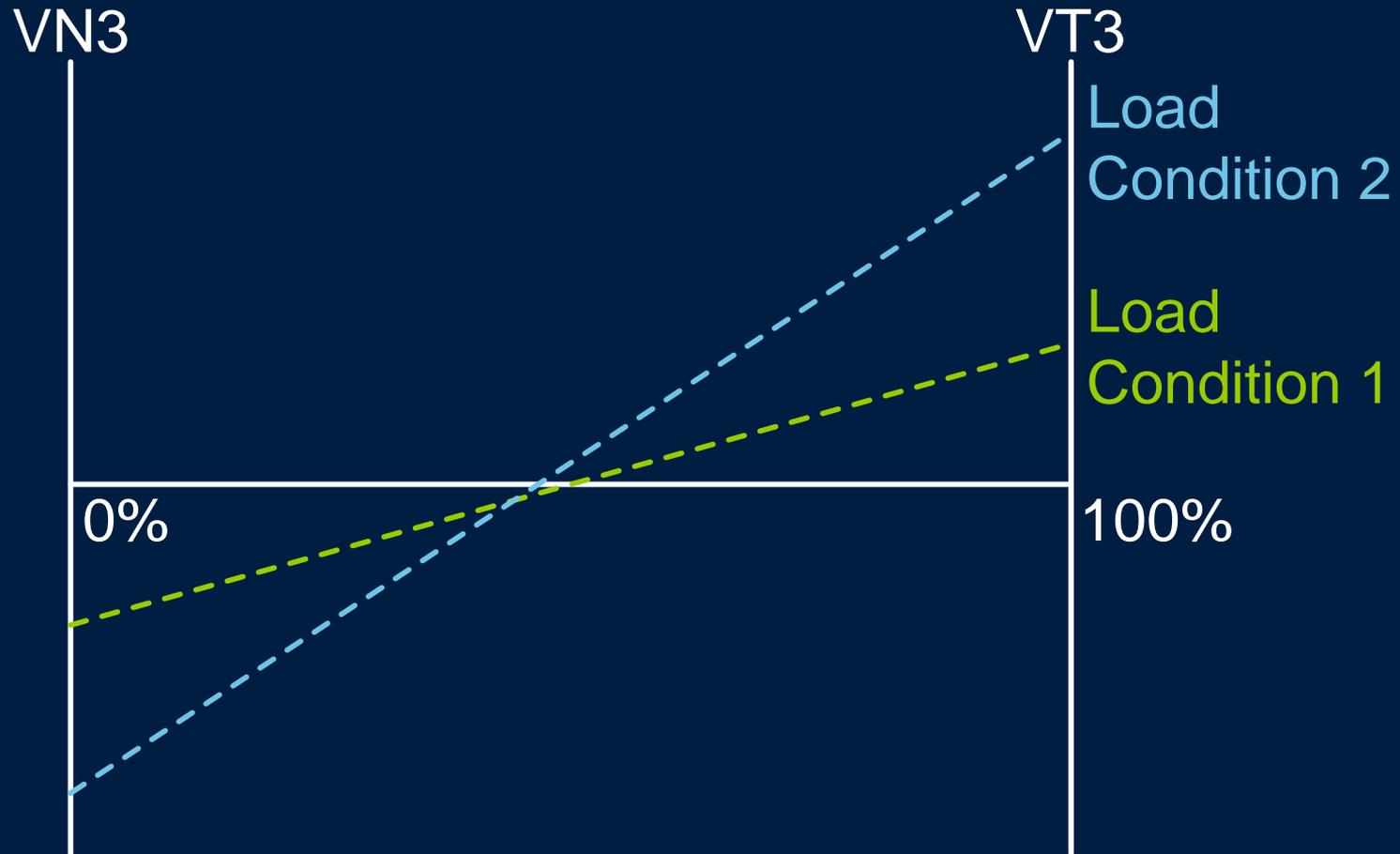
Third-Harmonic Survey



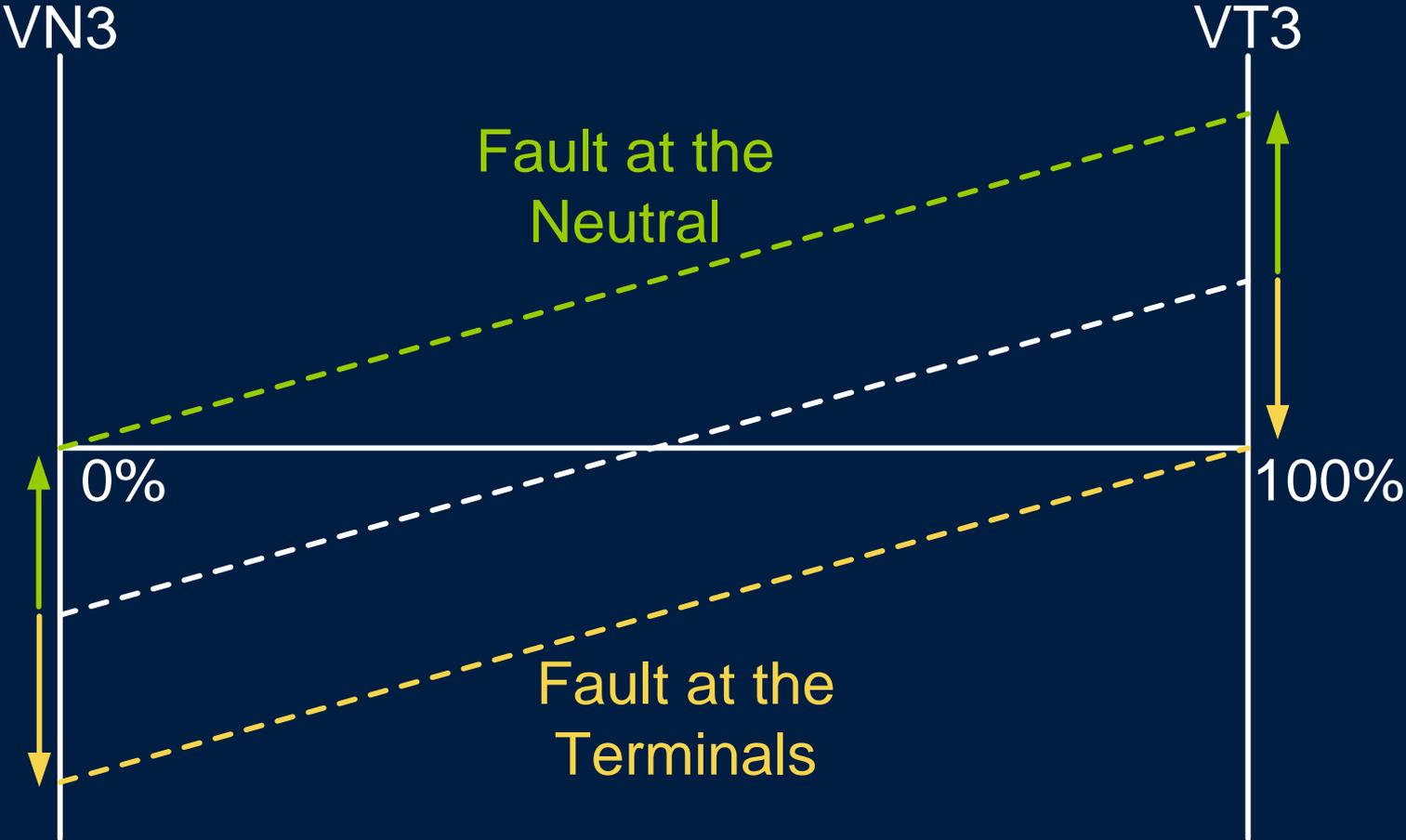
Third-Harmonic Differential



Third-Harmonic Ratio Is Not Sensitive to Load Changes



Distribution Shift Due to Fault



Setting the 59D3

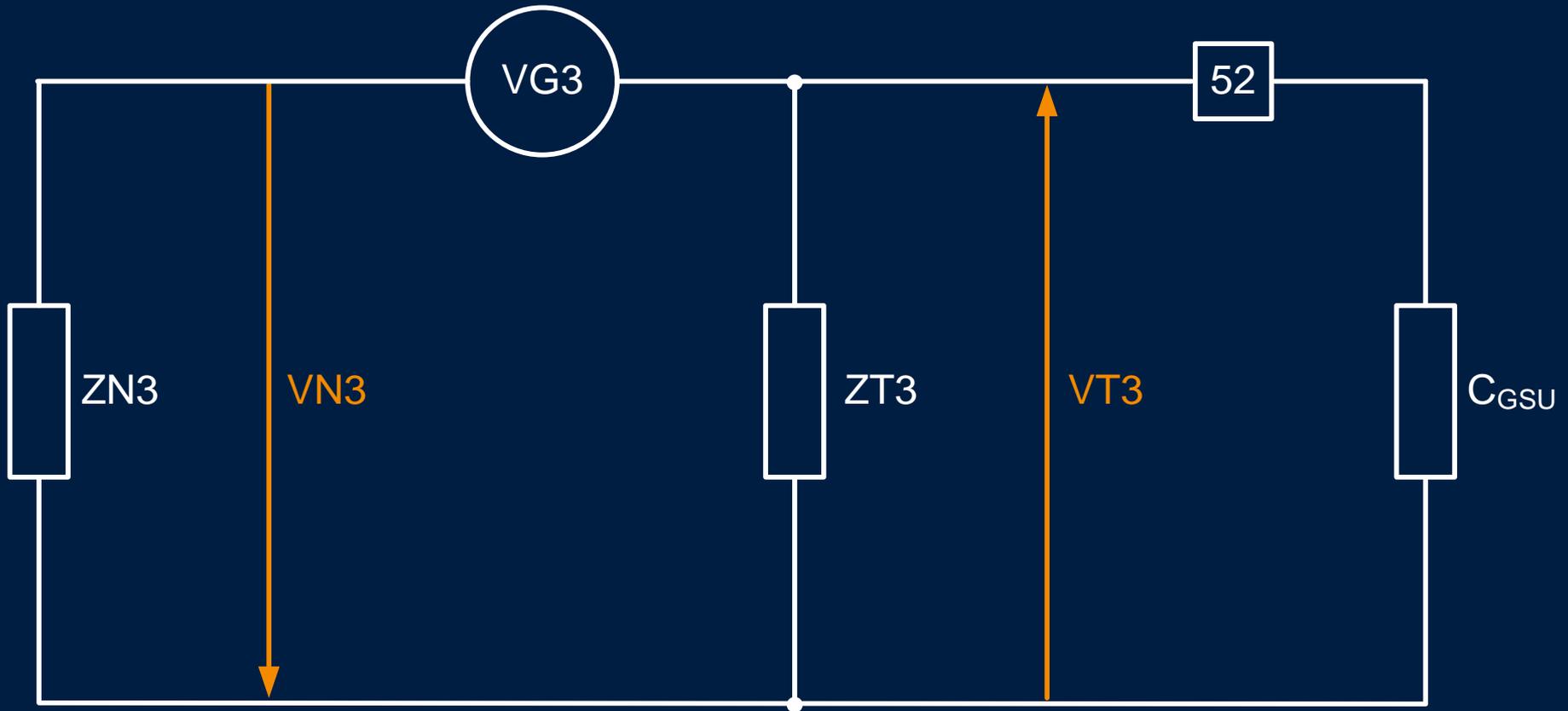
$$OP = \left\| |VN3_SEC| - RAT |VT3_SEC| \right\| > PKP$$

$$RAT = \frac{\sum_{n=1}^N VN3_SEC_n}{\sum_{n=1}^N VT3_SEC_n}$$

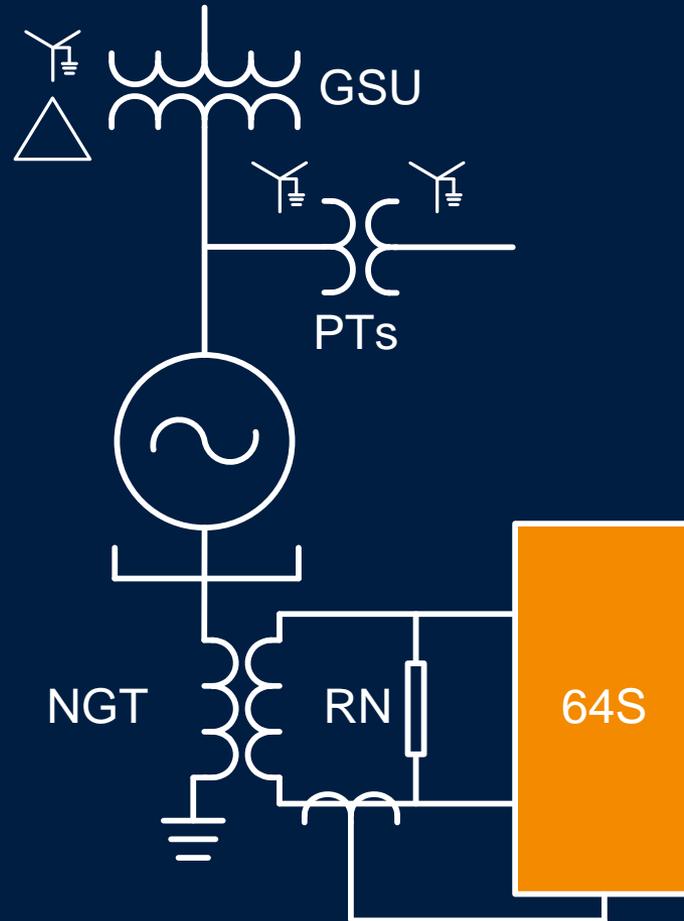
$$Pickup_{59D3} = 1.1 \left(0.1 + \text{MAX}_n \left\{ \left\| |VN3_SEC_n| - RAT |VT3_SEC_n| \right\| \right\} \right)$$

where N is the number of measurements

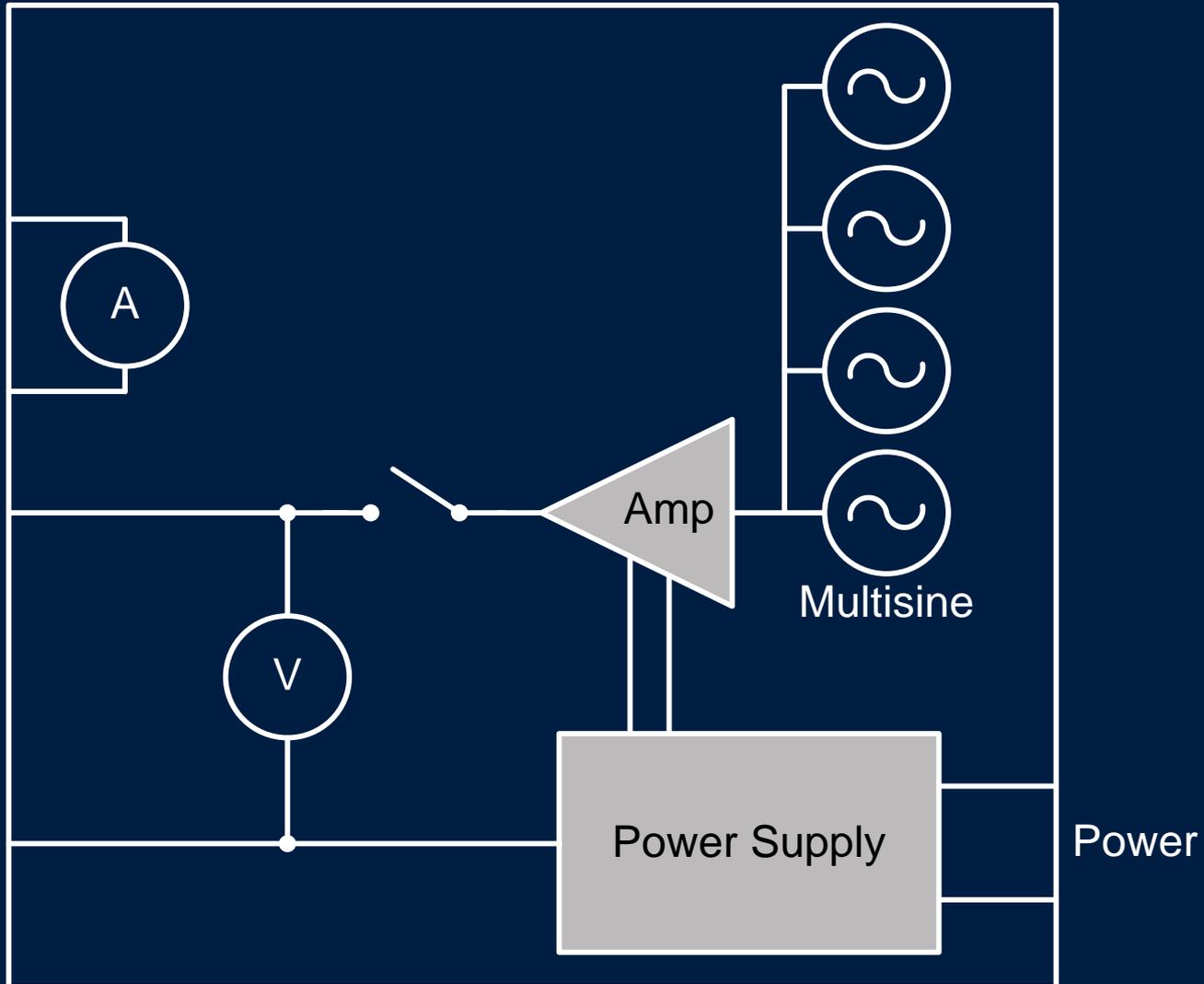
Influence of Low-Side Breaker



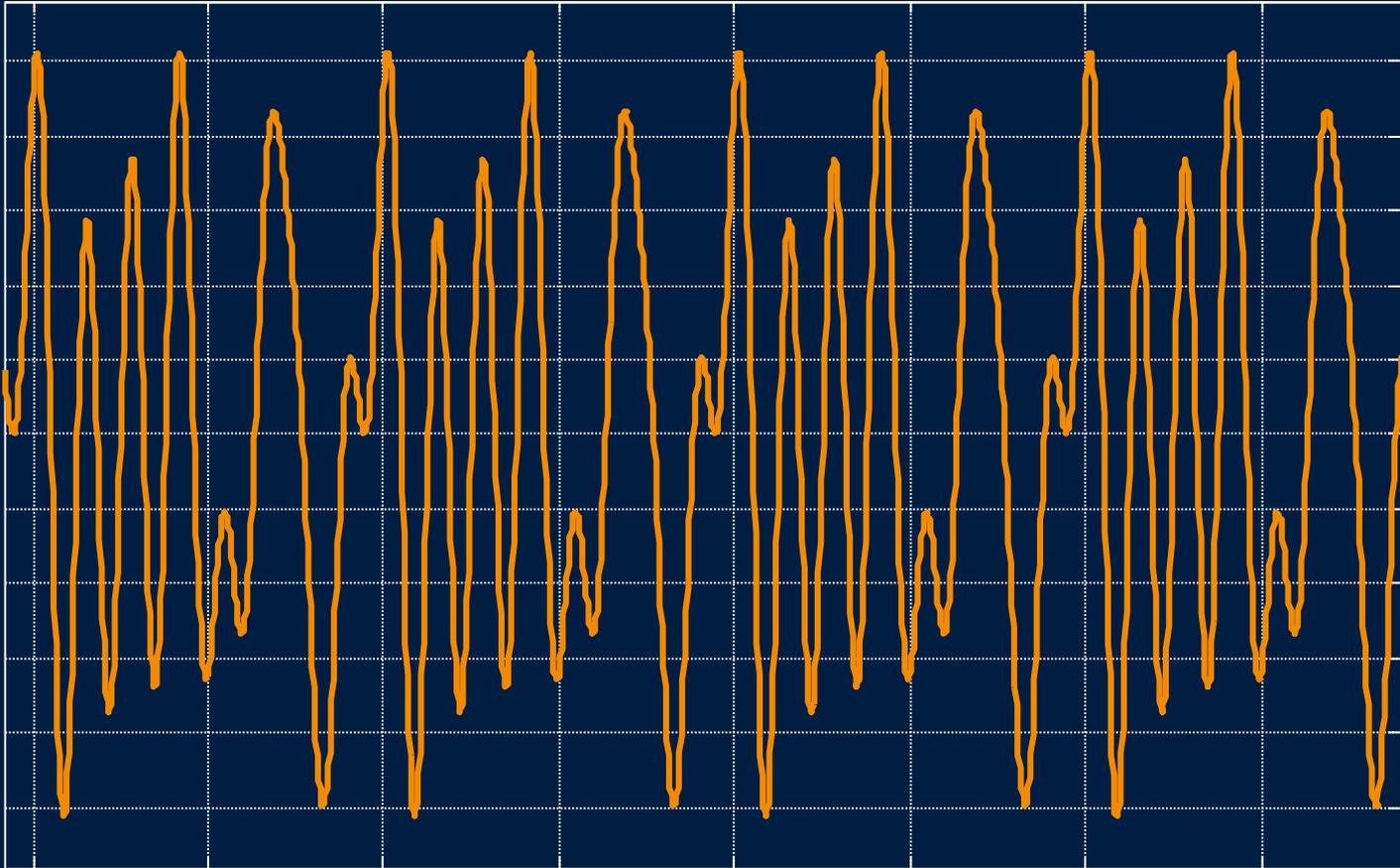
Subharmonic Injection



Injection Source

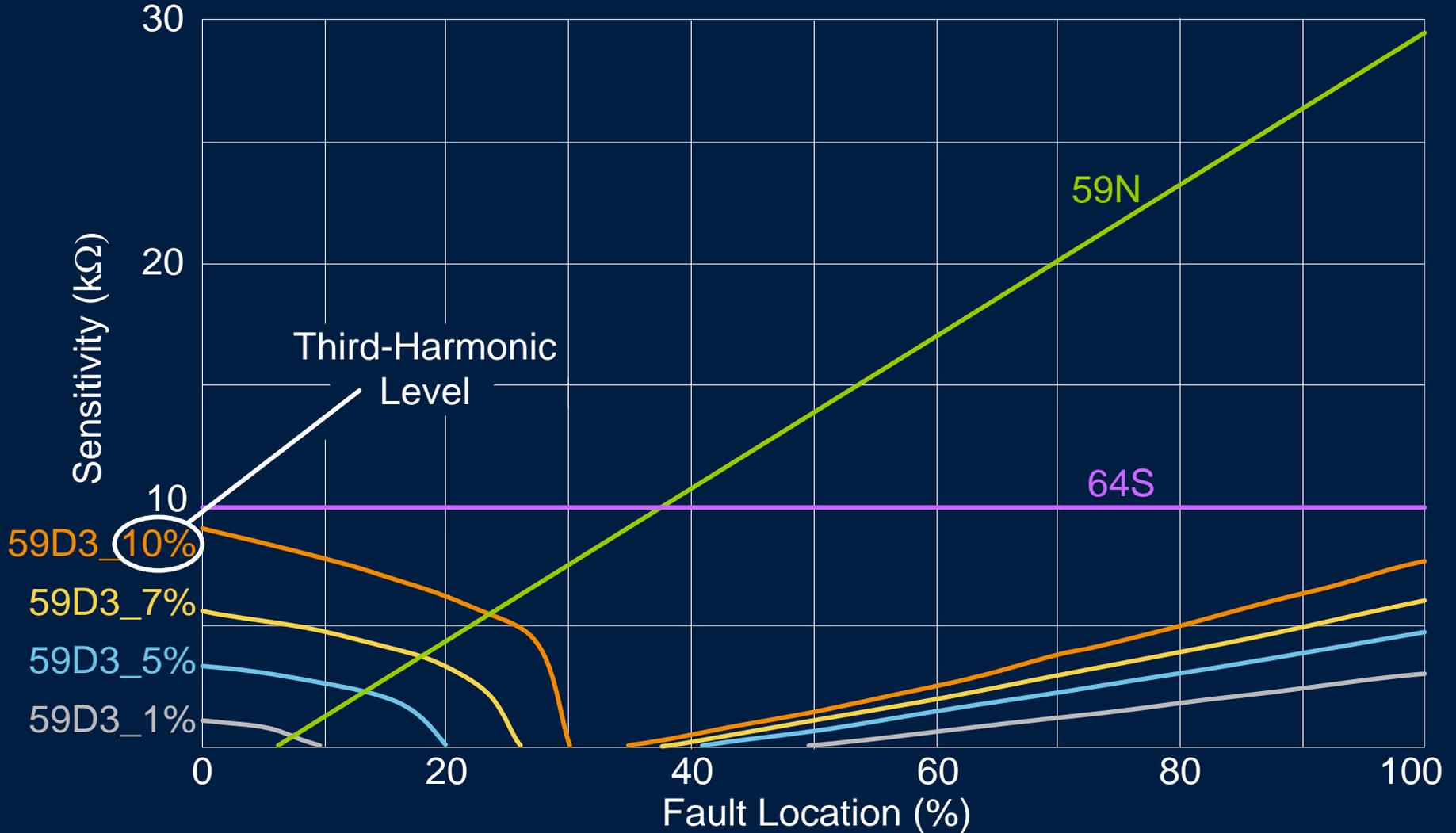


Multisine

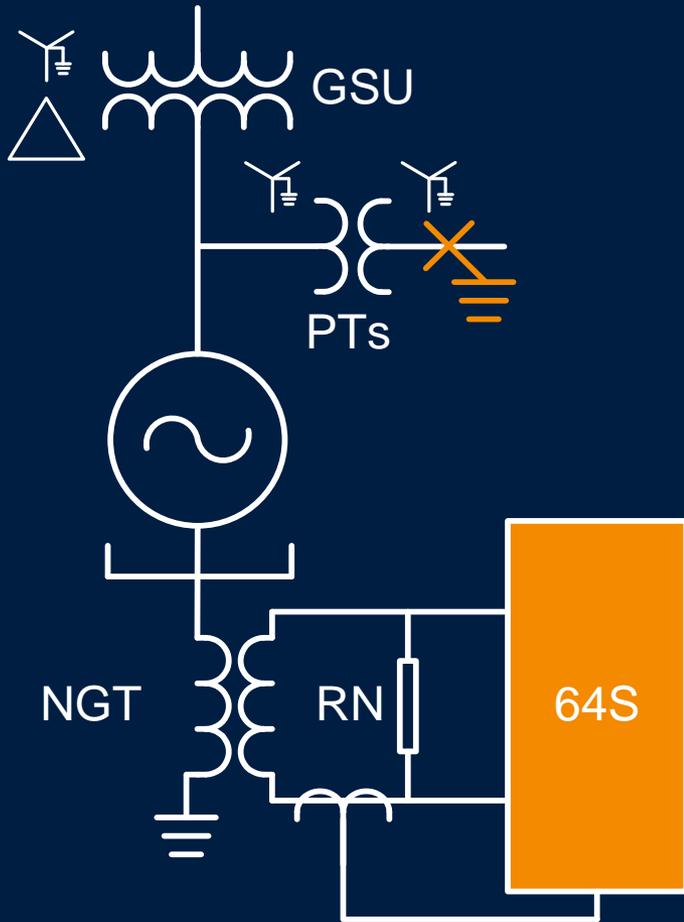


Injection of multiple sources allows application of redundant 64S units

64S Coverage Does Not Depend on Location



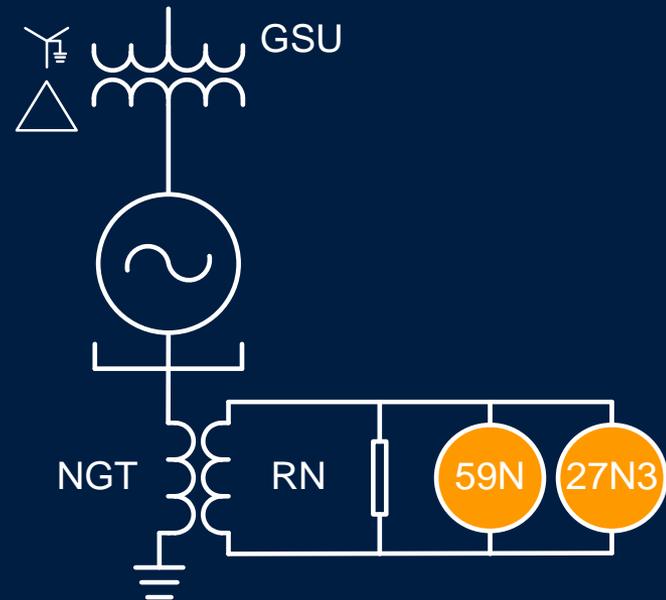
PT Secondary Ground



Test	Insulation (kΩ)
Unit offline	59.2
PT ground, X phase	8.57
PT ground, Y phase	8.11
PT ground, Z phase	8.05

Conclusions

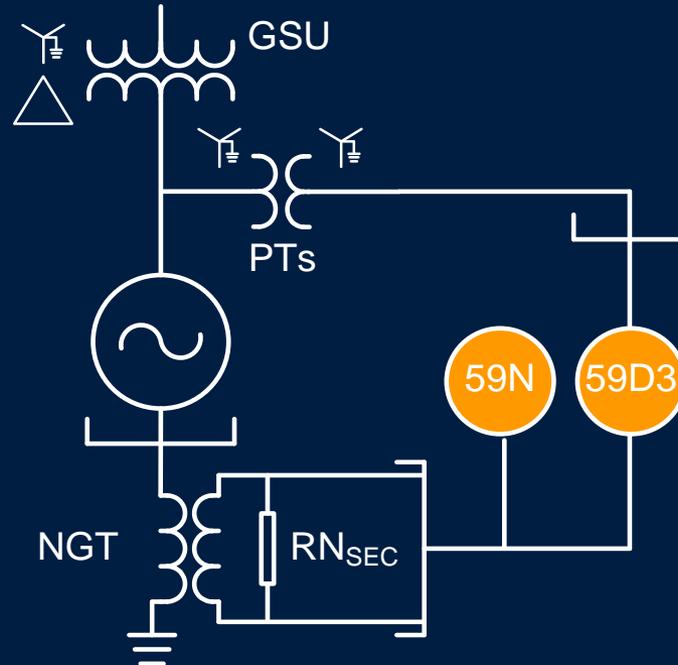
- 59N protects ~95% of winding (need to consider system and PT faults)
- 27N3 can protect remaining 5% (can be challenging to set)



Conclusions

59N3 Can Protect Remaining 5%

- Requires grounded-wye PT
- Is easier to set



Conclusions

64S Can Protect Entire Winding

- Requires extra hardware
- Is straightforward to set
- Works at standstill and starting
- Is applicable to parallel generators

Questions?

