



Zone-1 Ground Distance Element Mis-Operation for External Fault

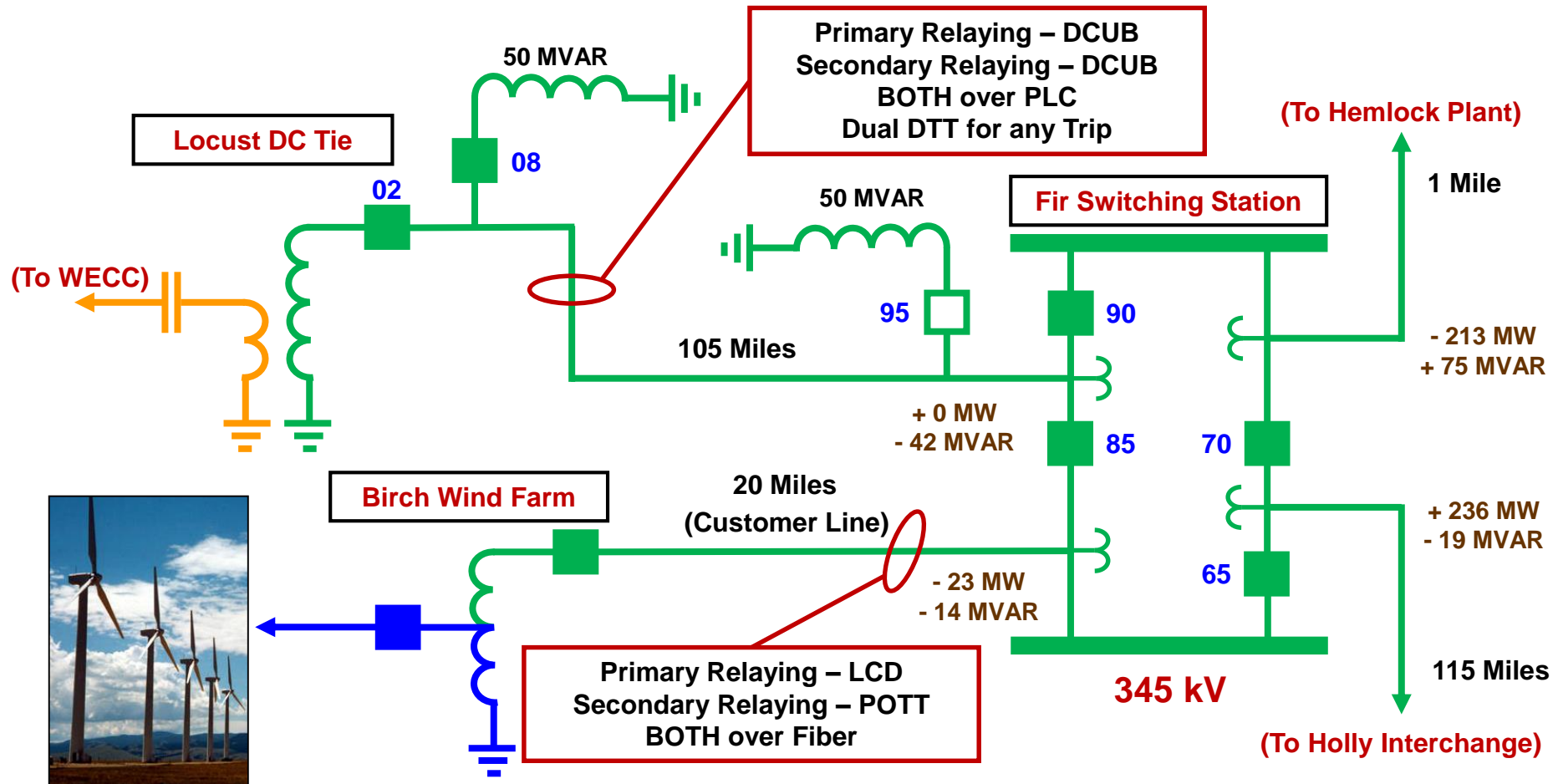
Presented by Kevin W. Jones, P.E.

Consulting Engineer, System Protection Engineering

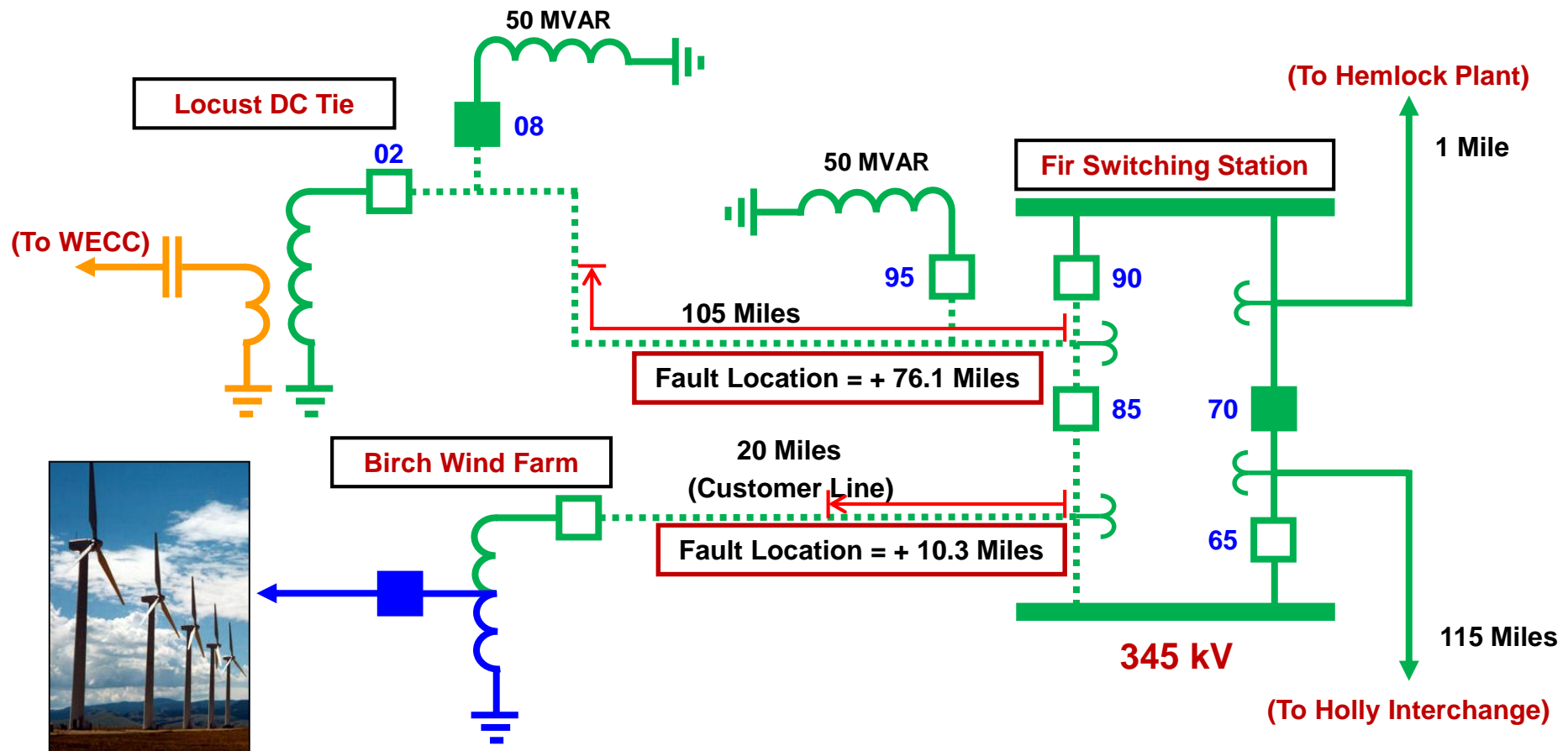
69th Annual Conference for Protective Relay Engineers

April 6, 2016

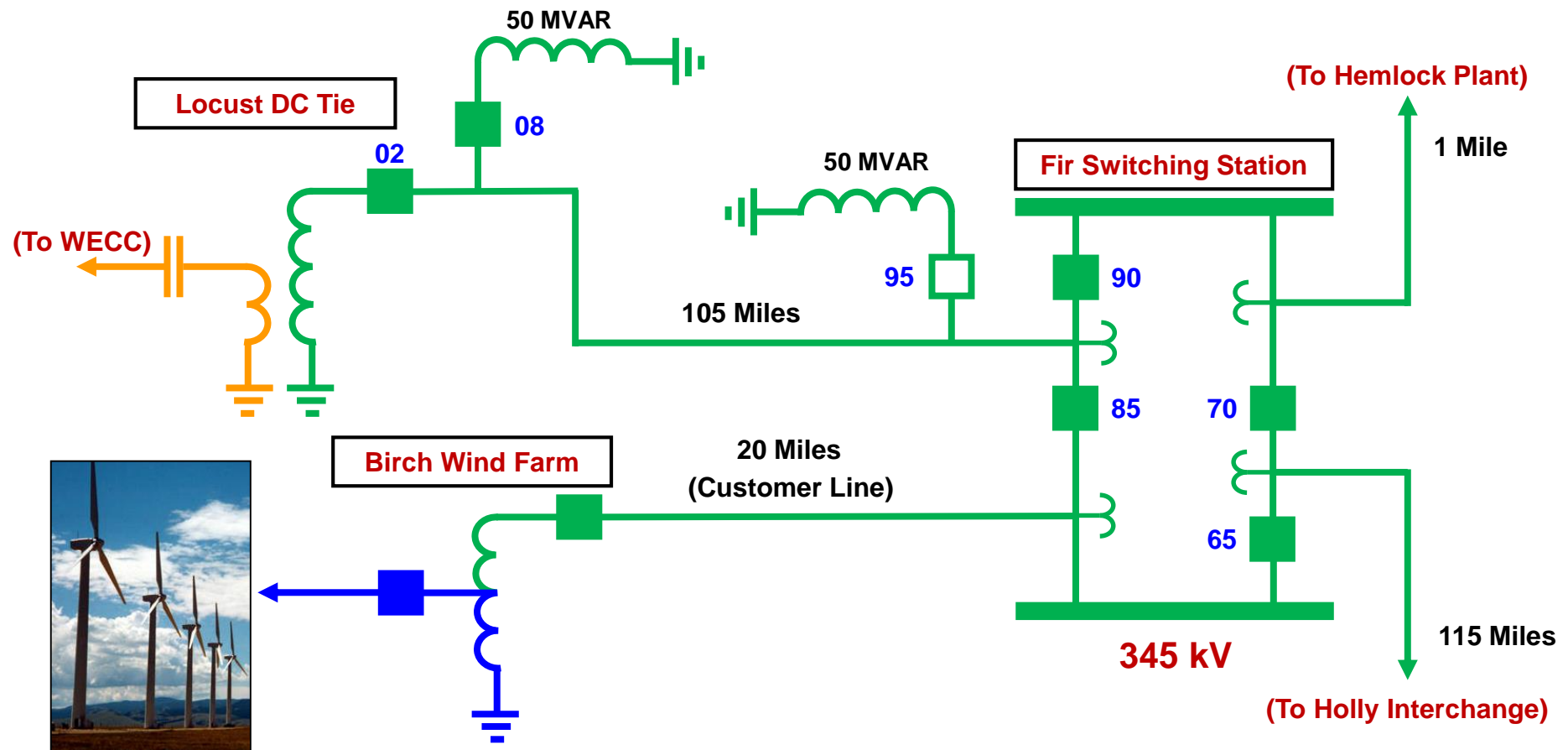
Pre-Disturbance System Configuration



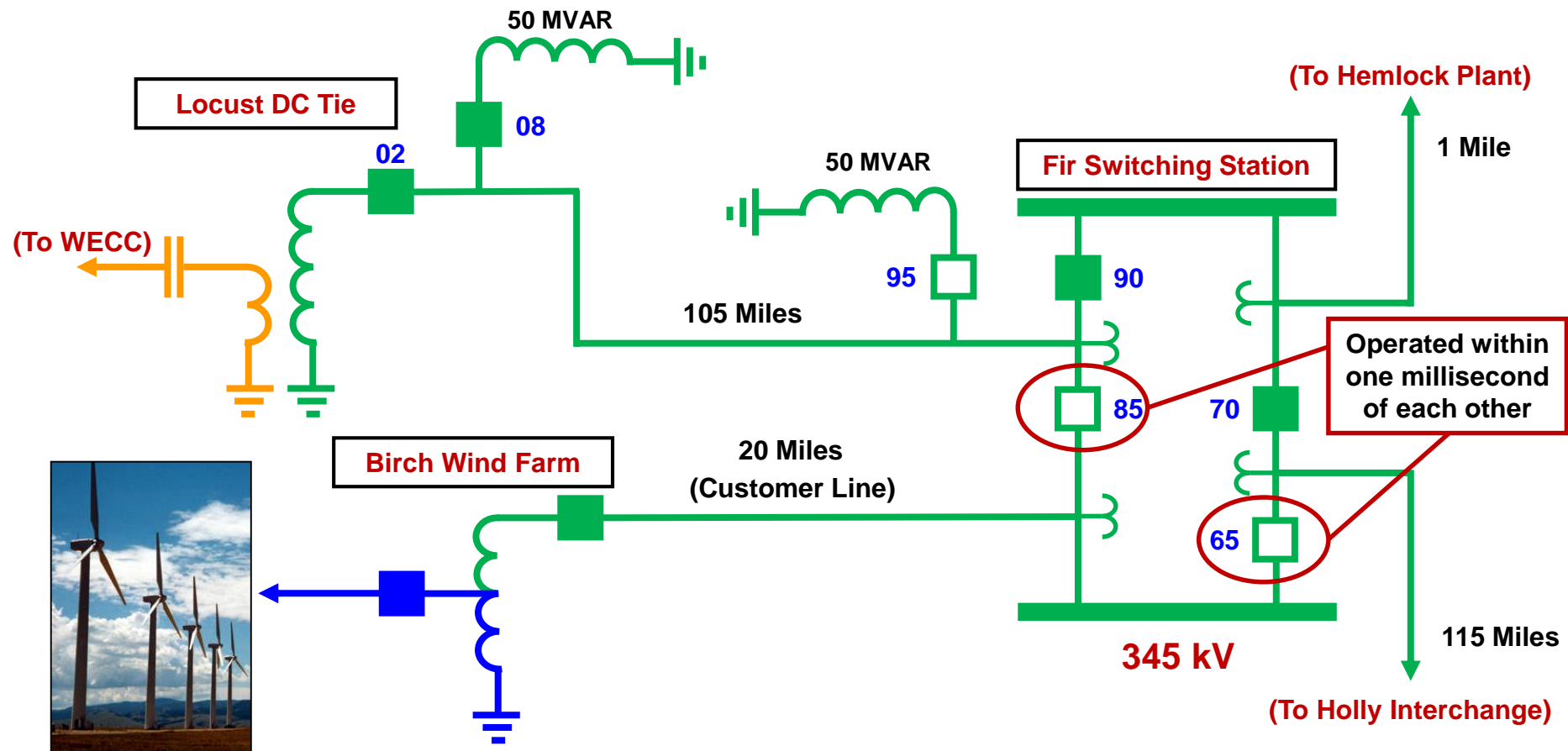
Post-Disturbance System Configuration



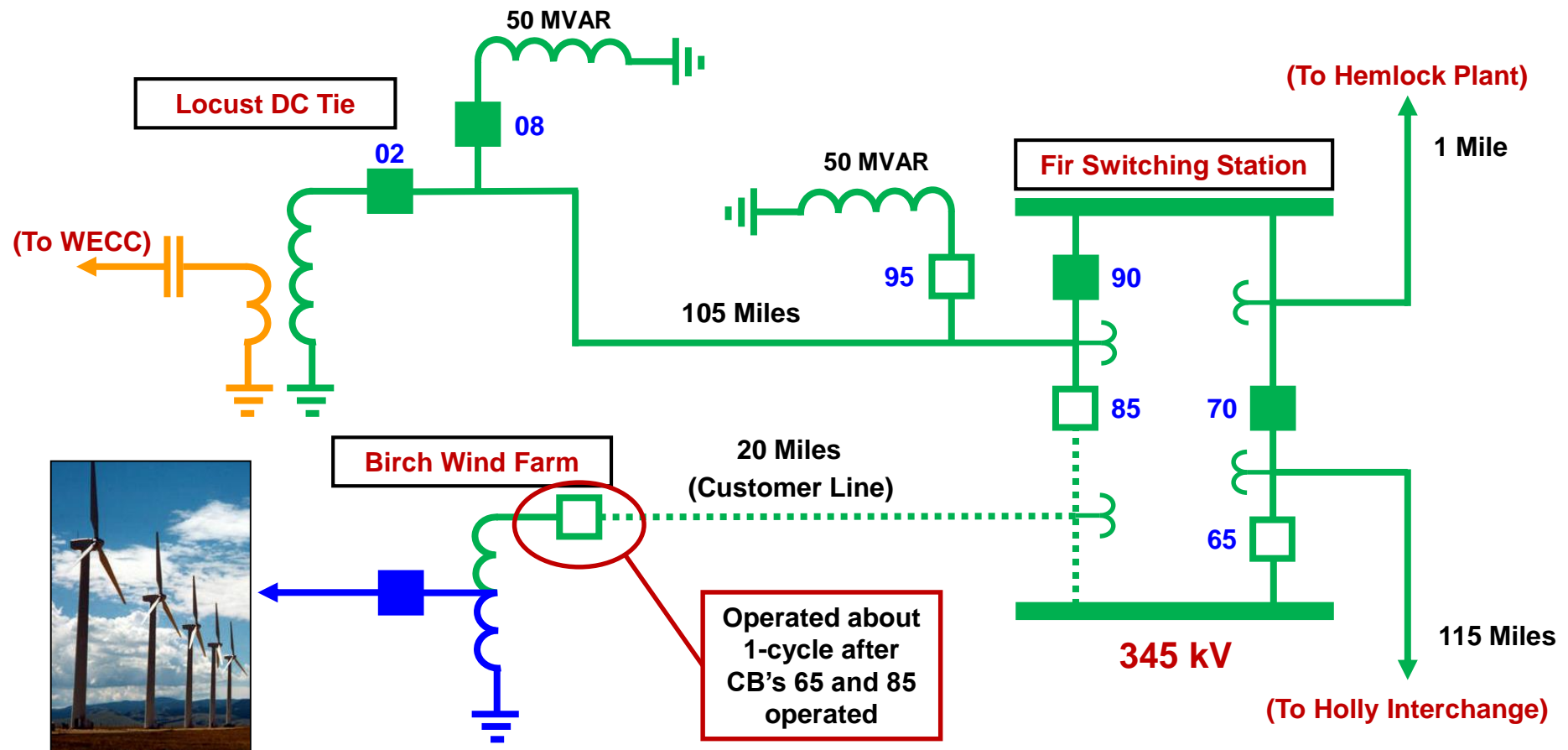
Sequence Of Events (SOE) Analysis



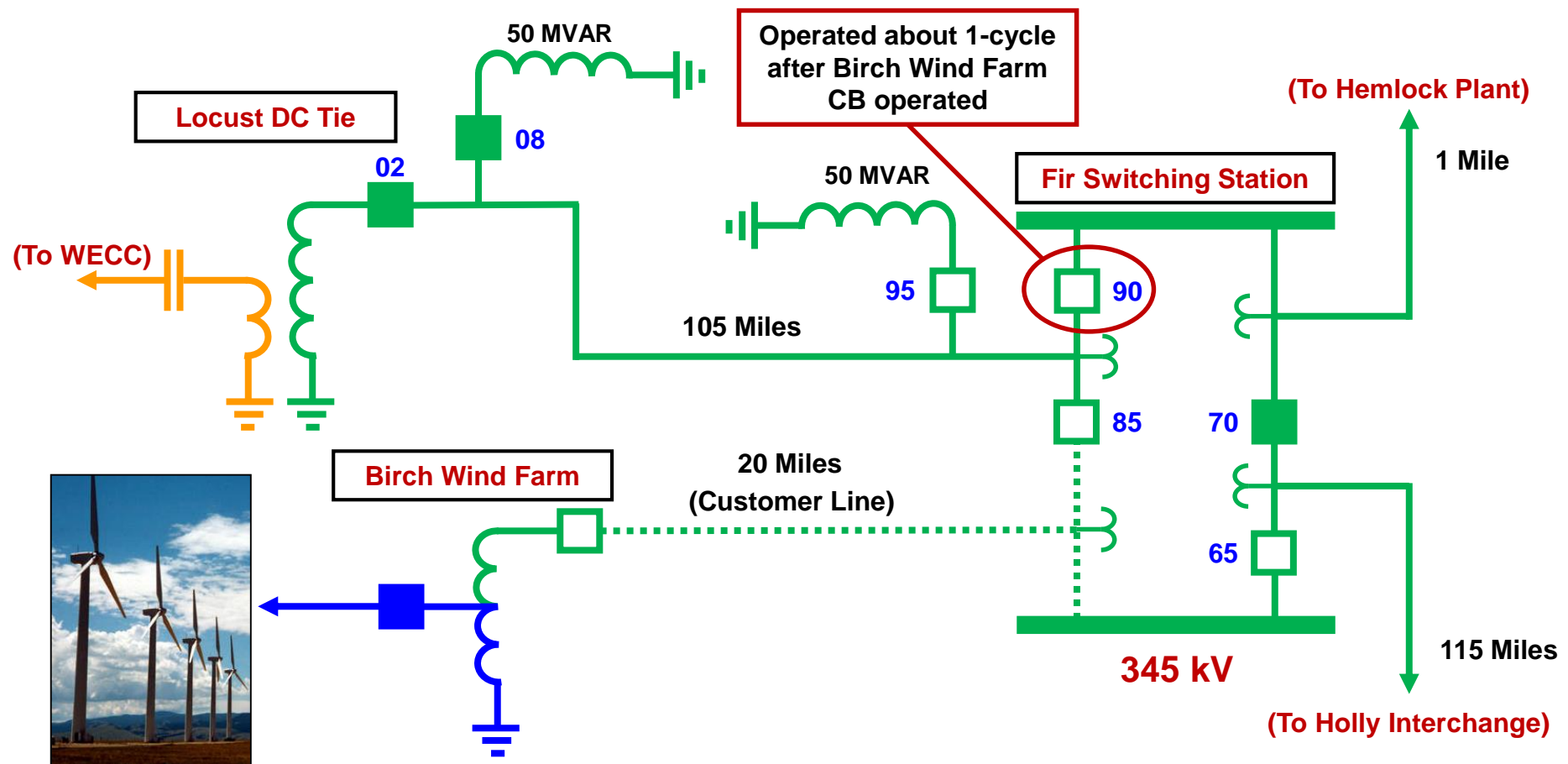
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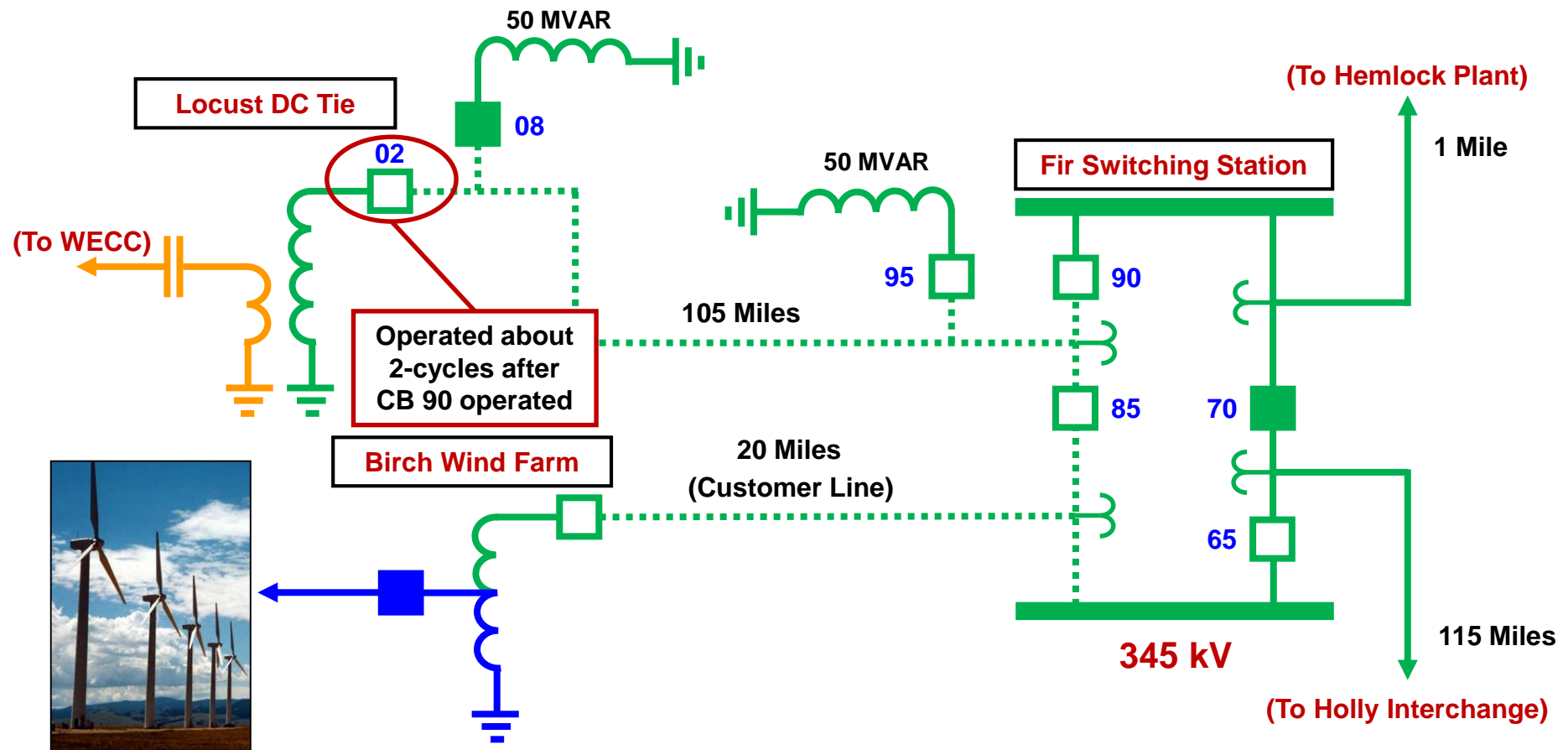
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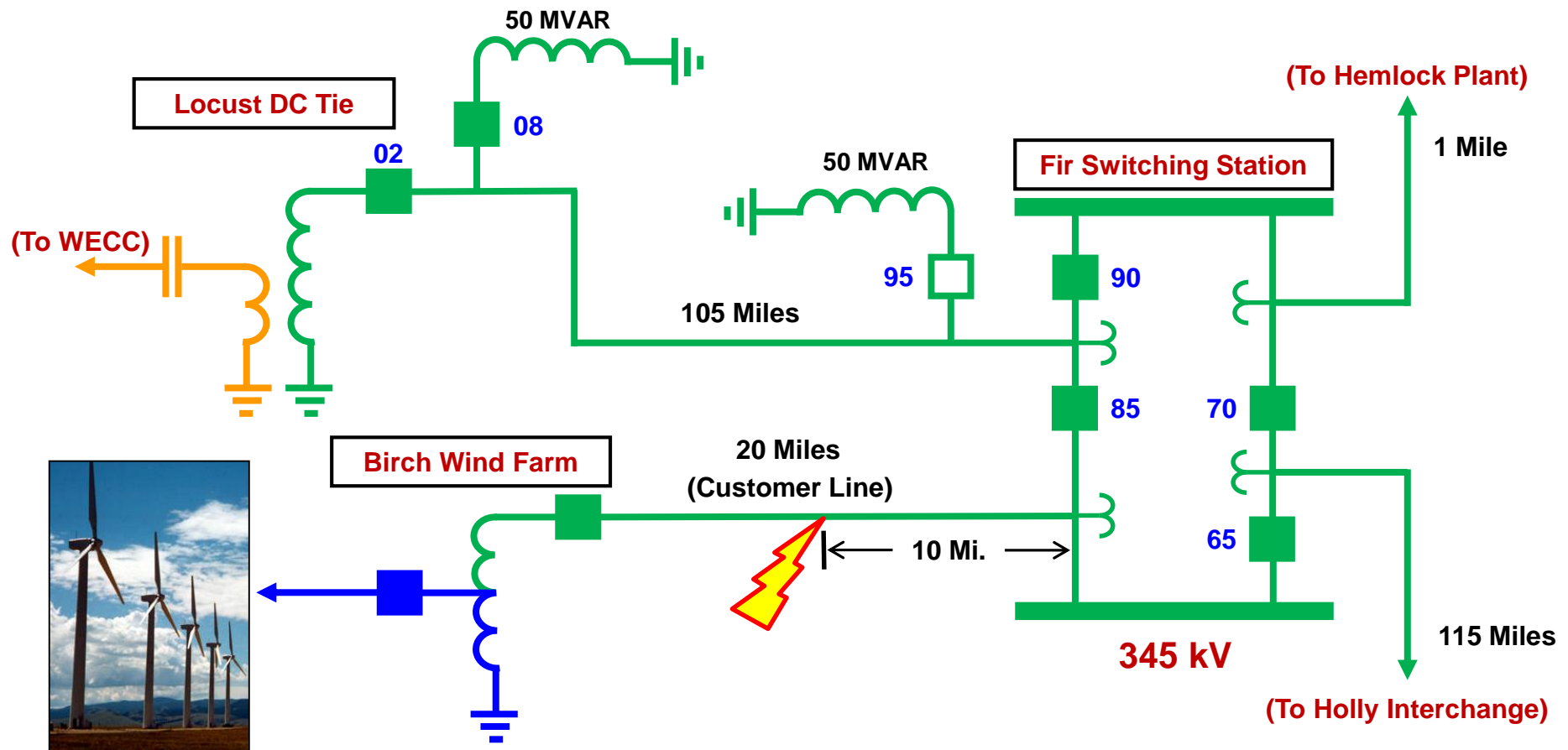
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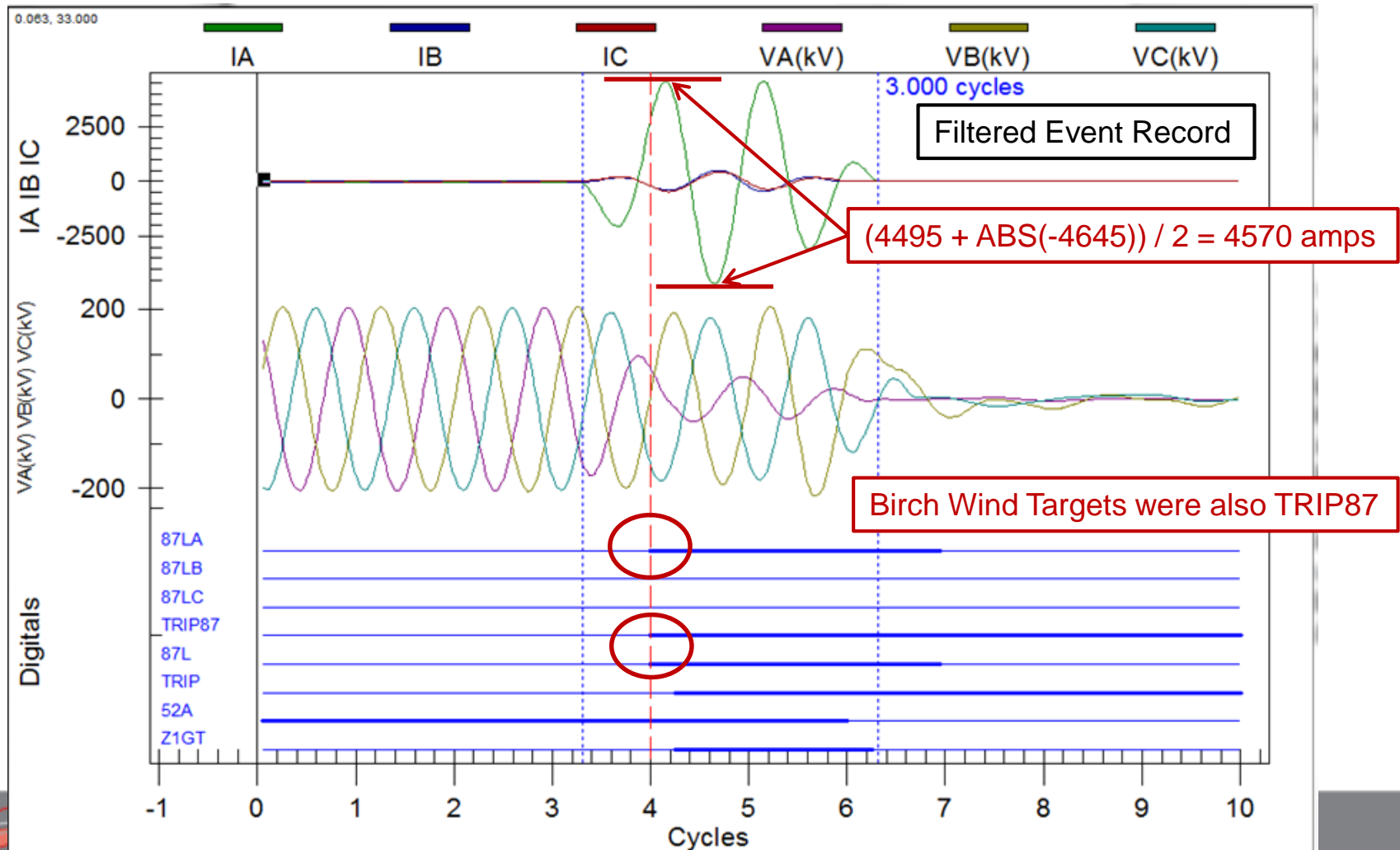
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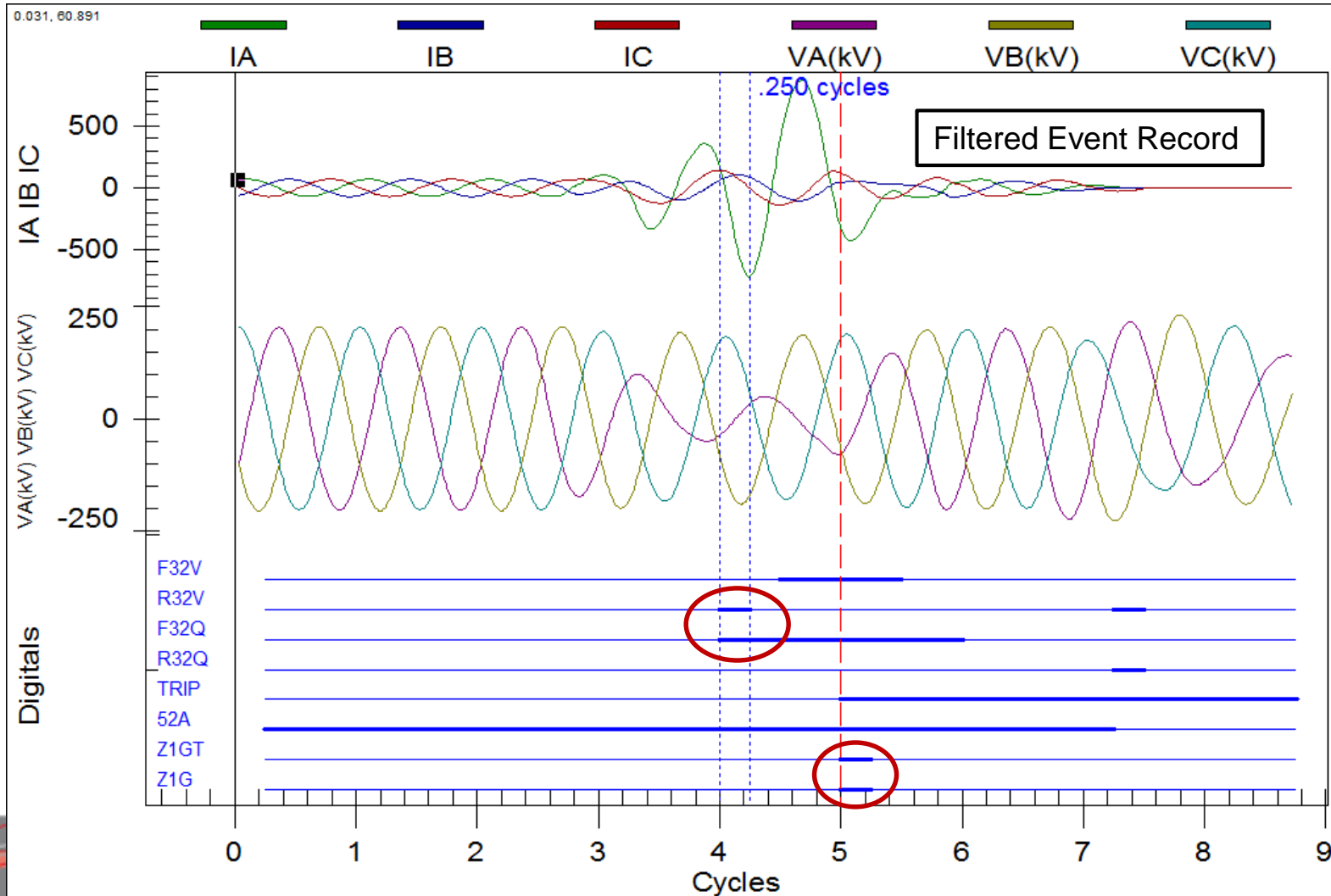
Lightning Analysis



Fir – Birch Event Record Analysis

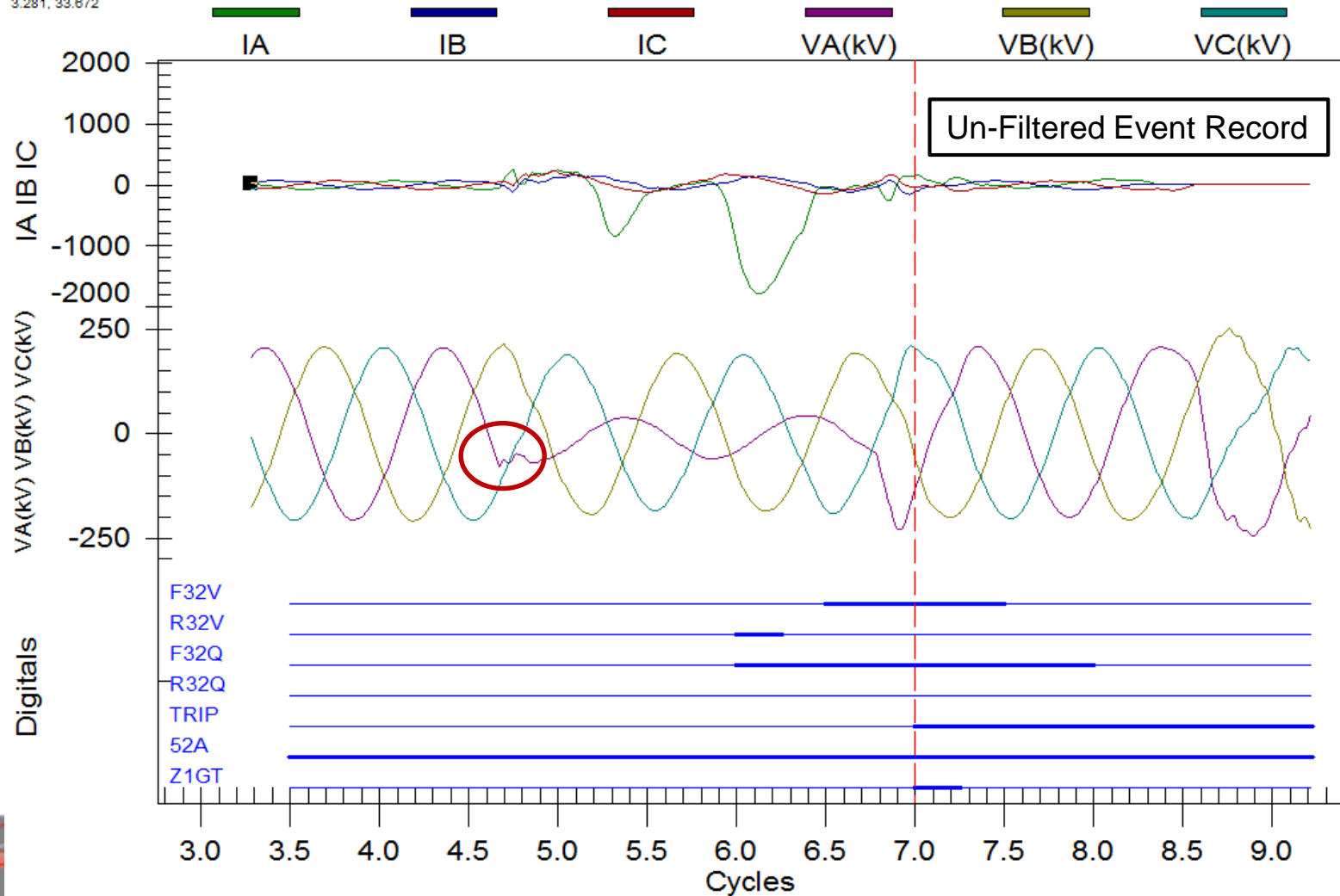


Fir – Locust Event Record Analysis

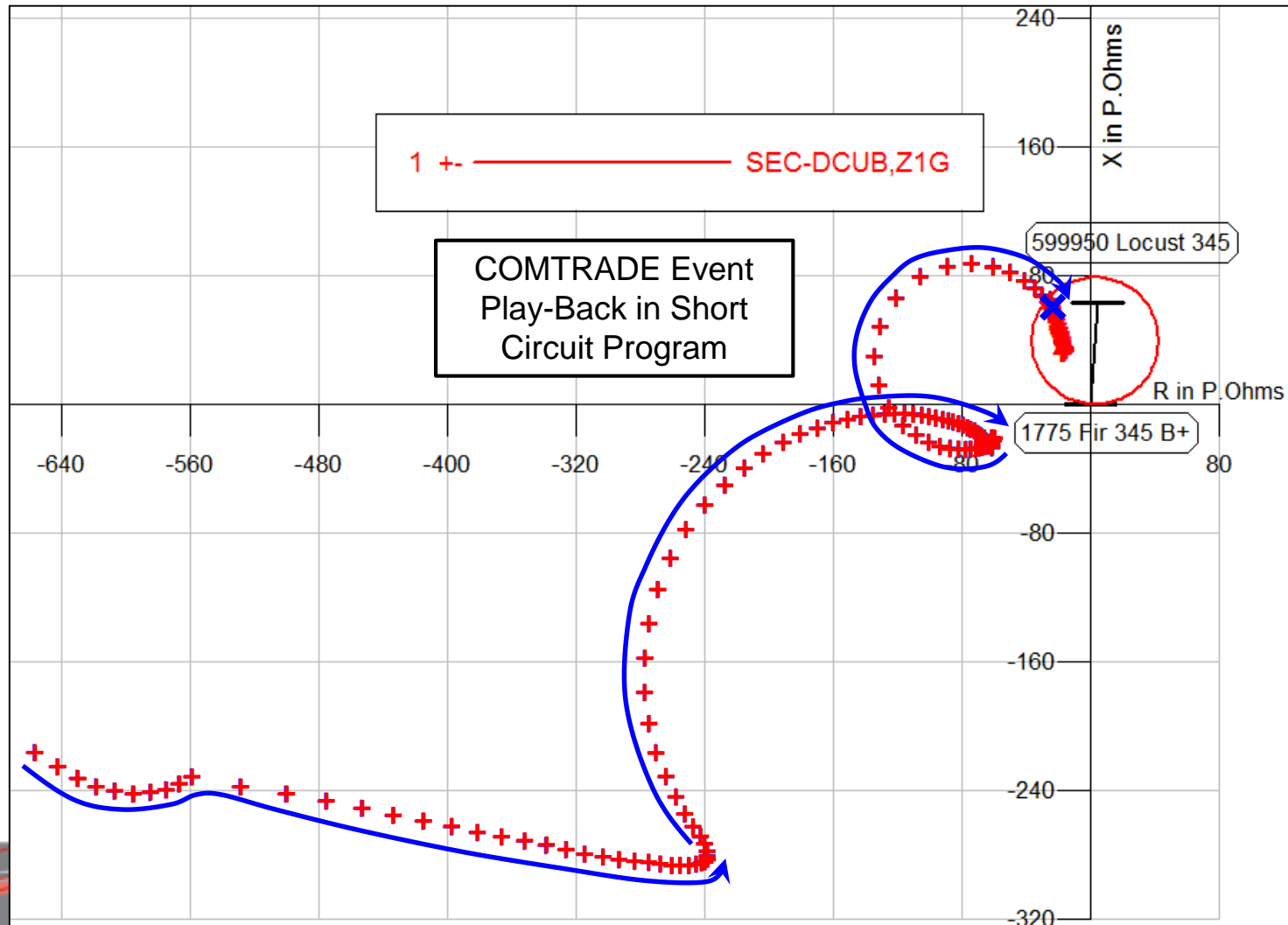


Fir – Locust Event Record Analysis

3.281, 33.672



Fir – Locust Event Record Analysis



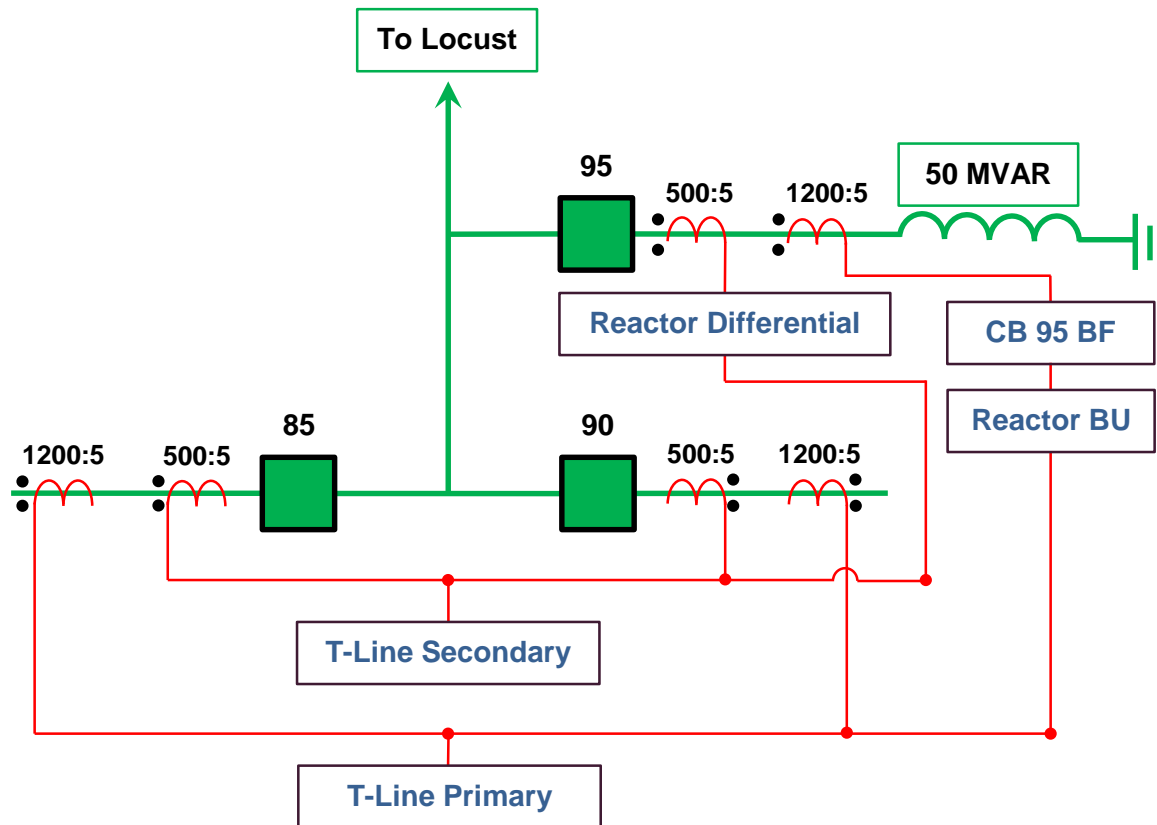
Preliminary Fault Analysis Conclusions

- A lightning induced fault occurred on the Fir to Birch 345 kV line.
- Fir to Birch operated correctly at both ends to clear the fault.
- The Locust end of the Fir to Locust line correctly operated on receive DTT.
- The Fir end of the Fir to Locust line incorrectly tripped due to unknown transient condition.

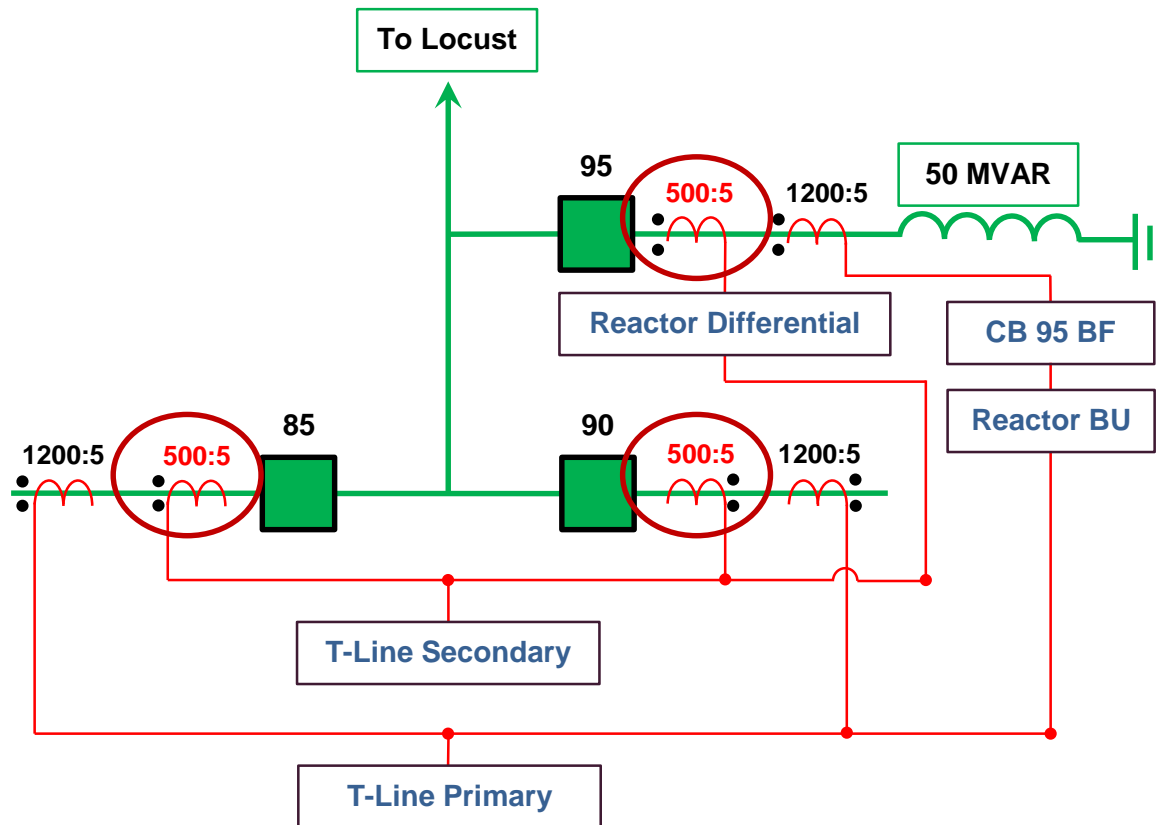
HELP!!!

- **Consulted with a relay manufacturer engineer.**
- **Engineer's analysis concluded that a CT was severely saturated and caused the mis-operation.**

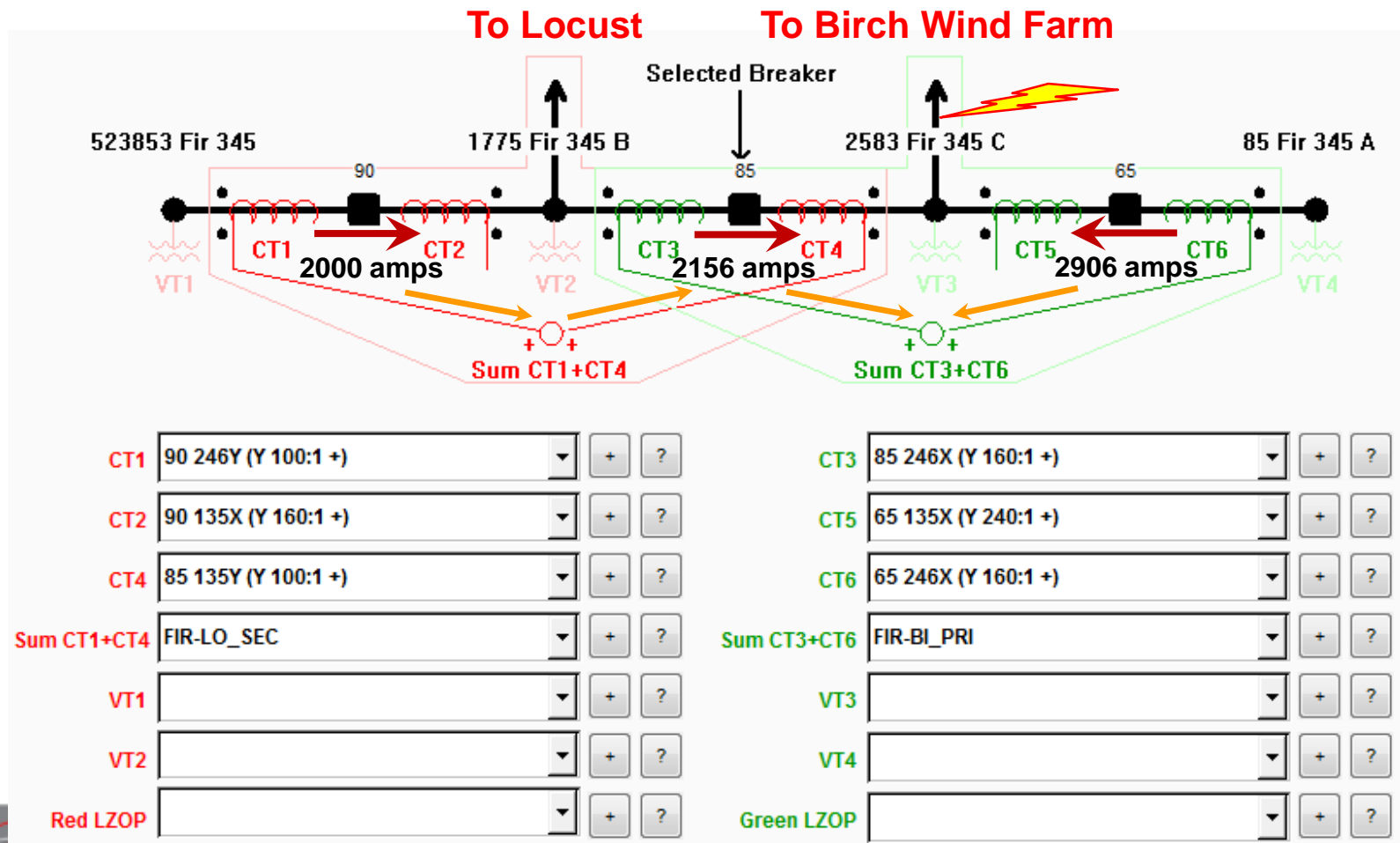
CT Saturation Theory Investigation



CT Saturation Theory Investigation



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CT Saturation Theory Investigation CB 85

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Sheet 1: CALCULATOR (this sheet)

Sheet 2: INSTRUCTIONS

Sheet 4: BACKGROUND

CT Saturation Calculator

Excel Spread Sheet

See IEEE publication C37.110: "IEEE Guide for the Application of Current Transformers Used for Protective Relaying Purposes"

A document of the

IEEE Power Systems Relaying Committee

Contact: gswift@nxtphase.com

Refer also to "CT SAT Theory (PSRC)".

VERSION:
30 Dec 2002

ASSUMPTIONS:

CT core losses and sec'y reactance zero (thru-hole primary).

Frequency: 60 Hz

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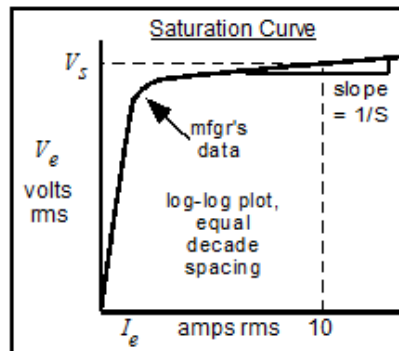
CT is 5 amp nominal

Time step = $1/12,000$ second.

INPUT PARAMETERS:

ENTER:

Inverse of sat. curve slope =	S =	25.5	---
RMS voltage at 10A exc. current =	Vs =	210	volts rms
Turns ratio = $n2/1$ =	N =	100	---
Winding resistance =	Rw =	0.100	ohms
Burden resistance =	Rb =	0.870	ohms
Burden reactance =	Xb =	0.087	ohms
System X/R ratio =	XoverR =	13.5	---
Per unit offset in primary current =	Off =	-0.72	-1 < Off < 1
Per unit remanence (based on Vs) =	λ_{rem}	0.48	---
Symmetrical primary fault current =	Ip =	-2,156	amps rms

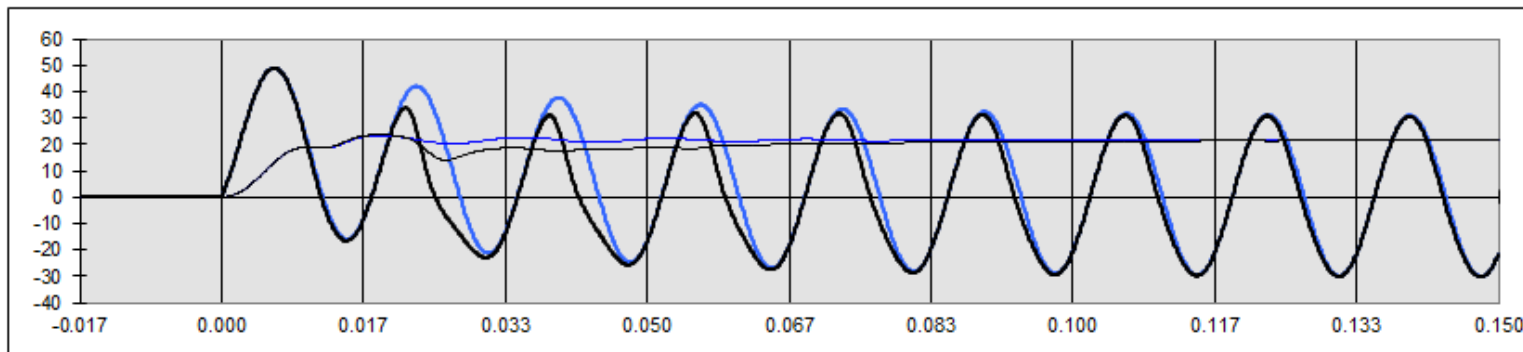


CALCULATED:

Rt = Total burden resistance = $Rw + Rb$ =	0.970	ohms
pf = Total burden power factor =	0.996	---
Zb = Total burden impedance =	0.974	ohms
Tau1 = System time constant =	0.036	seconds
Lamsat = Peak flux-linkages corresponding to Vs	0.788	Wb-turns
ω = Radian freq =	376.99	rad/s
RP = Rms-to-peak ratio =	0.33344	---
A = Coefficient in instantaneous ie versus lambda curve: $ie = A * I^S$:	1.31E+04	---
dt = Time step =	0.000083	seconds
Lb = Burden inductance =	0.00023	henries

Thick lines: Ideal (blue) and actual (black) secondary current in amps vs time in seconds.

Thin lines: Ideal (blue) and actual (black) secondary current extracted fundamental rms value, using a simple DFT with a one-cycle window.



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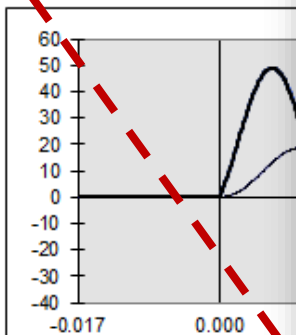
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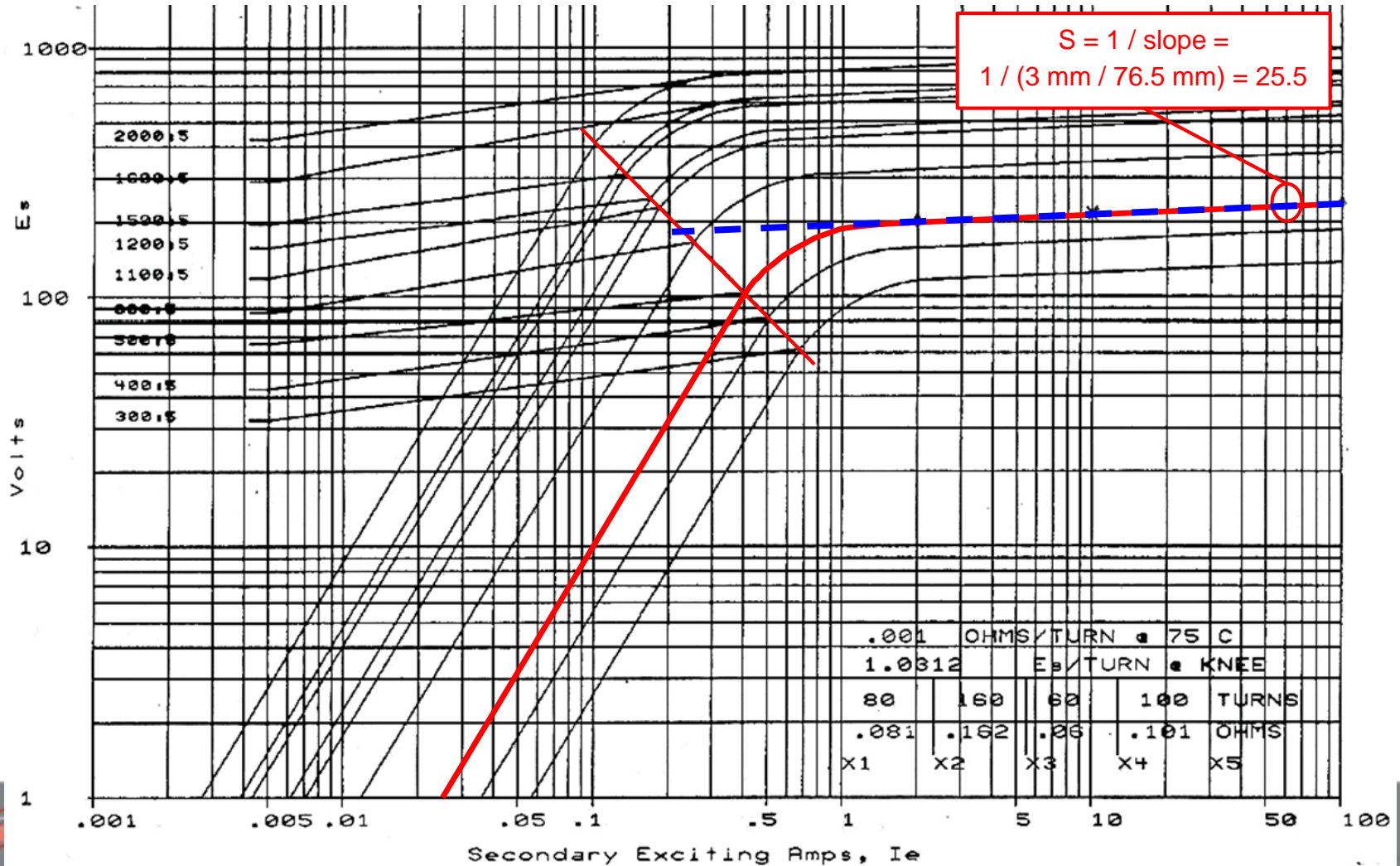
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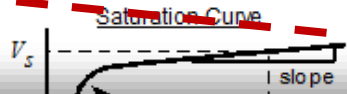
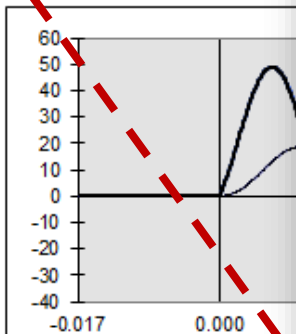
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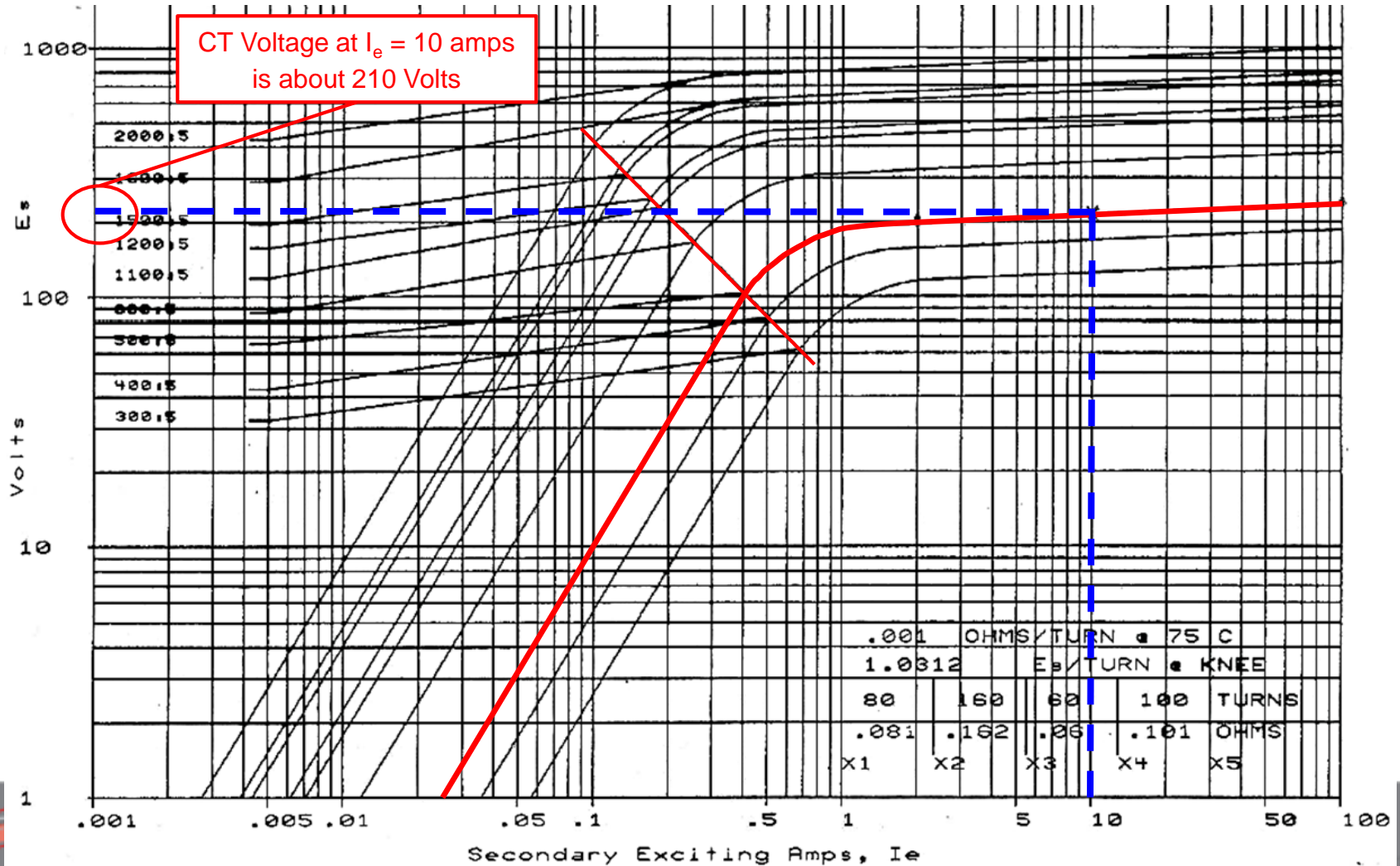
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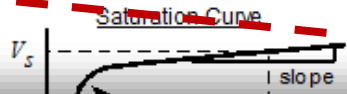
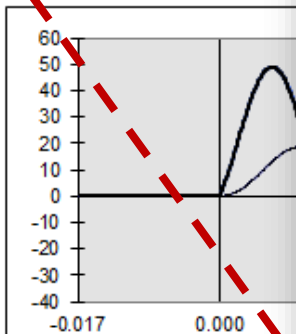
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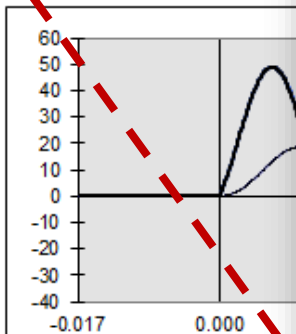
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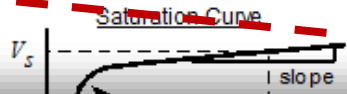
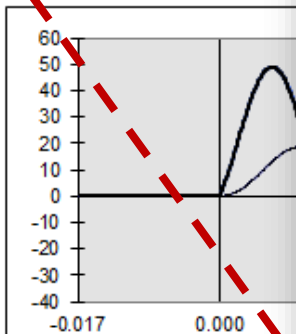
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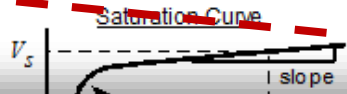
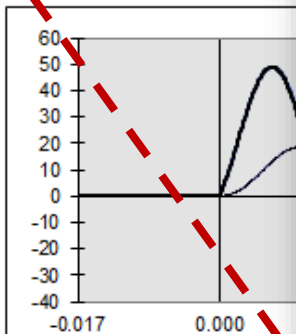
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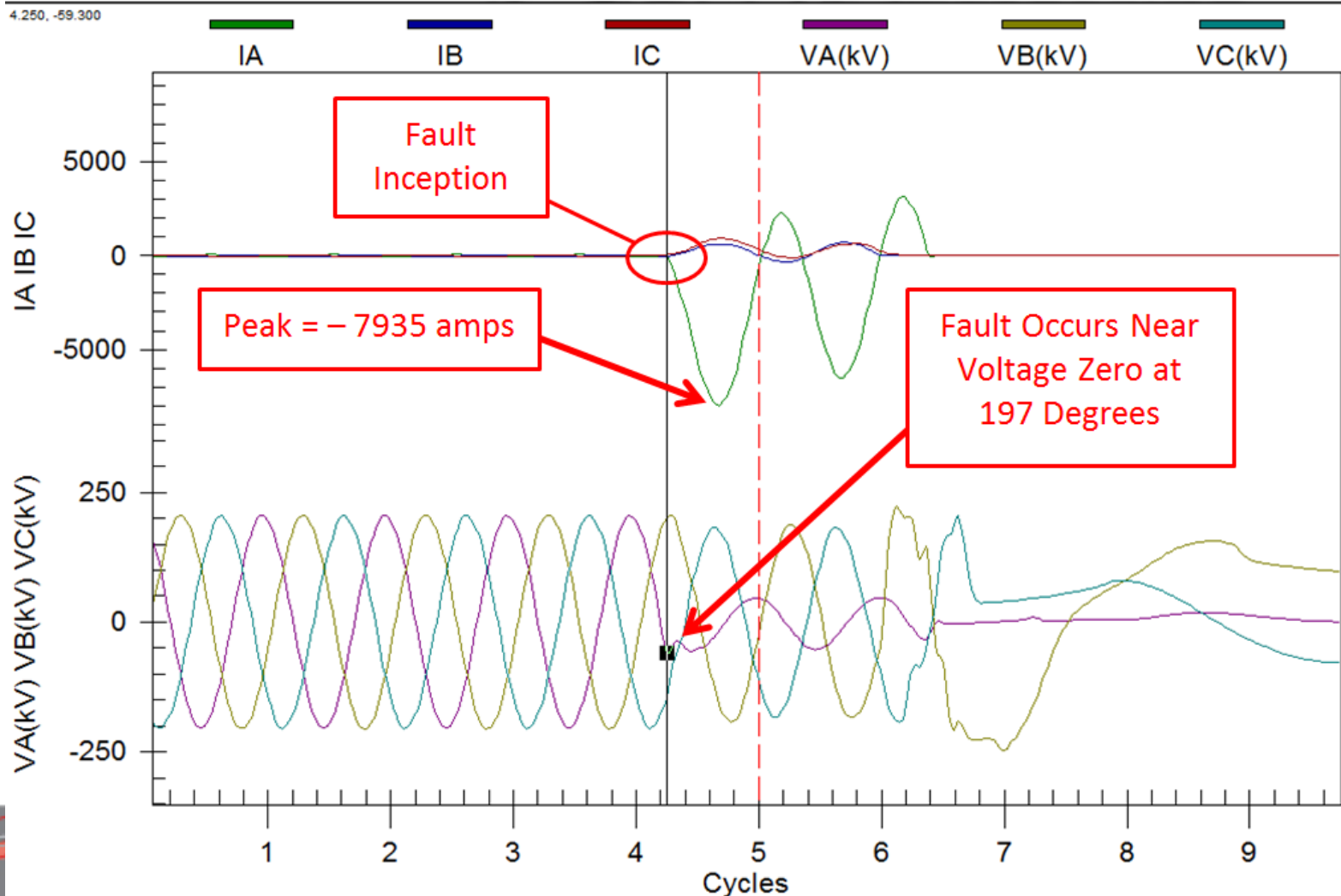
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DC Offset Calculator

$$f := 60 \text{ hertz}$$

$$\omega := 2 \cdot \pi \cdot f$$

$$I_{\max} := 4570 \text{ amps (peak)}$$

$$R := 1.322$$

$$X := 14.498$$

$$L := \frac{X}{\omega}$$

$$\theta := \operatorname{atan}\left(\frac{X}{R}\right)$$

$$\theta = 84.7899 \cdot \text{deg}$$

The percent DC offset at 197 degrees is:
 $(|-7863| - 4570) / 4570 * 100 = 72.06\%$

$$\alpha := 197 \cdot \text{deg}$$

(angle of voltage on faulted phase at fault inception)

$$T_c := \frac{L}{R} \cdot 60$$

$$T_c = 1.7454 \text{ cycles (time constant)}$$

$$I(t) := I_{\max} \cdot \left(\sin(\omega \cdot t + \alpha - \theta) - e^{-R \cdot \frac{t}{L}} \cdot \sin(\alpha - \theta) \right) \text{ amps (peak) theoretical}$$

$$I_{\max} \cdot \left(\sin(\omega \cdot 0.00729167 + \alpha - \theta) - e^{-R \cdot \frac{0.00729167}{L}} \cdot \sin(\alpha - \theta) \right) = -7863 \text{ amps}$$

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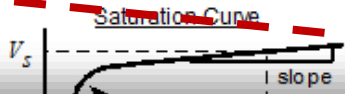
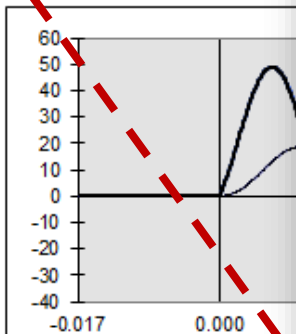
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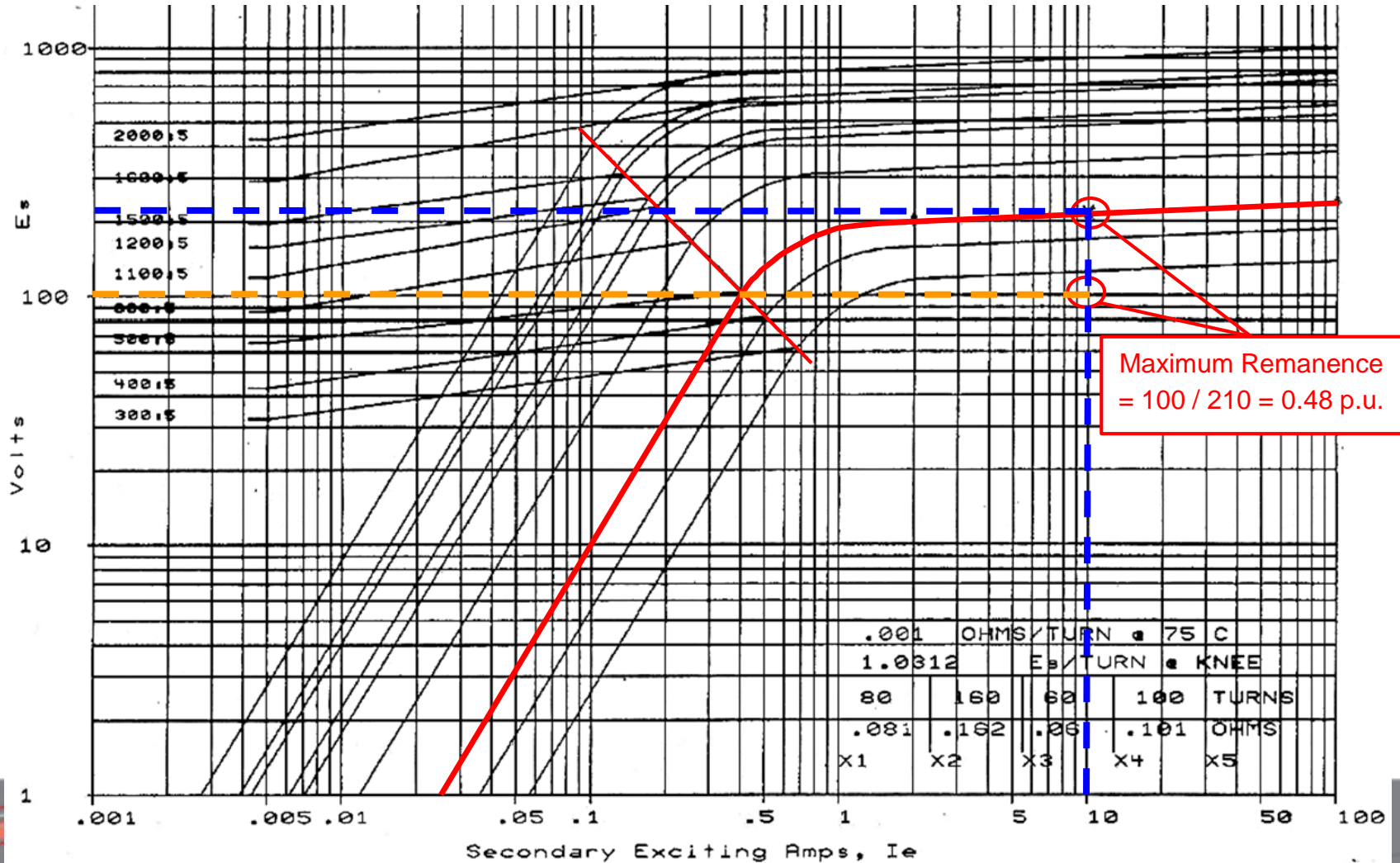
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INPUT PARAMETERS:

Inverse of sat. curve slope = $S =$ 25.5 ---
 RMS voltage at 10A exc. current = $V_s =$ 210 volts rms
 Turns ratio = $n_2/n_1 =$ 100 ---
 Winding resistance = $R_w =$ 0.100 ohms
 Burden resistance = $R_b =$ 0.870 ohms
 Burden reactance = $X_b =$ 0.087 ohms
 System X/R ratio = $X_{over}R =$ 13.5 ---
 Per unit offset in primary current = $Off =$ -0.72 -1 < Off < 1
 Per unit remanence (based on V_s) = $\lambda_{rem} =$ 0.48 ---
 Symmetrical primary fault current = $I_p =$ -2,156 amps rms

CT Saturation Theory Investigation CB 85



CT Saturation Theory Investigation CB 85

CONTENTS

Sheet 1: CALCULATOR (this sheet)

Sheet 2: INSTRUCTIONS

Sheet 4: BACKGROUND

CT Saturation Calculator

Excel Spread Sheet

See IEEE publication C37.110: "IEEE Guide for the Application of Current Transformers Used for Protective Relaying Purposes"

A document of the

IEEE Power Systems Relaying Committee

Contact: gswift@nxtphase.com

Refer also to "CT SAT Theory (PSRC)".

VERSION:
30 Dec 2002

ASSUMPTIONS:

CT core losses and sec'y reactance zero (thru-hole primary).

Frequency: 60 Hz

CT primary current is zero for $t < 0$.

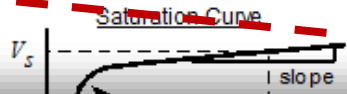
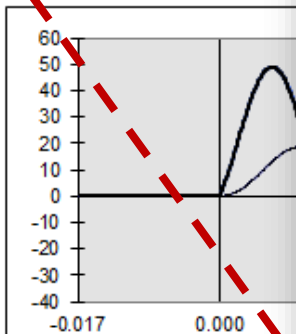
CT is 5 amp nominal

Time step = 1/12,000 second.

INPUT PARAMETERS:

Inverse of sat. curve slope = $S =$ 25.5 ---
 RMS voltage at 10A exc. current = $V_s =$ 210 volts rms
 Turns ratio = $n_2/1 =$ 100
 Winding resistance =
 Burden resistance =
 Burden reactance =
 System X/R ratio =
 Per unit offset in primary current =
 Per unit remanence (based on V_s) =
 Symmetrical primary fault current =

Thick lines
Thin lines



CALCULATED:

R_t = Total burden resistance = $R_w + R_b =$ 0.970 ohms
 pf = Total burden power factor = 0.996 ---

INPUT PARAMETERS:

Inverse of sat. curve slope = $S =$ 25.5 ---
 RMS voltage at 10A exc. current = $V_s =$ 210 volts rms
 Turns ratio = $n_2/1 =$ 100
 Winding resistance = $R_w =$ 0.100 ohms
 Burden resistance = $R_b =$ 0.870 ohms
 Burden reactance = $X_b =$ 0.087 ohms
 System X/R ratio = $X_{overR} =$ 13.5 ---
 Per unit offset in primary current = $Off =$ -0.72 $-1 < Off < 1$
 Per unit remanence (based on V_s) = $\lambda_{rem} =$ 0.48 ---
 Symmetrical primary fault current = $I_p =$ -2,156 amps rms

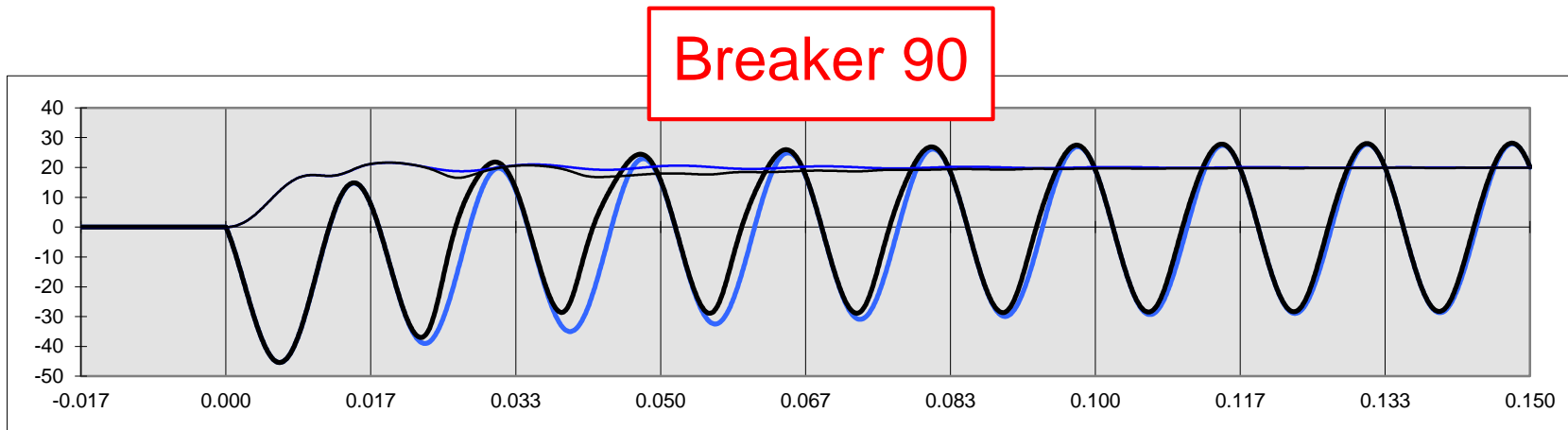
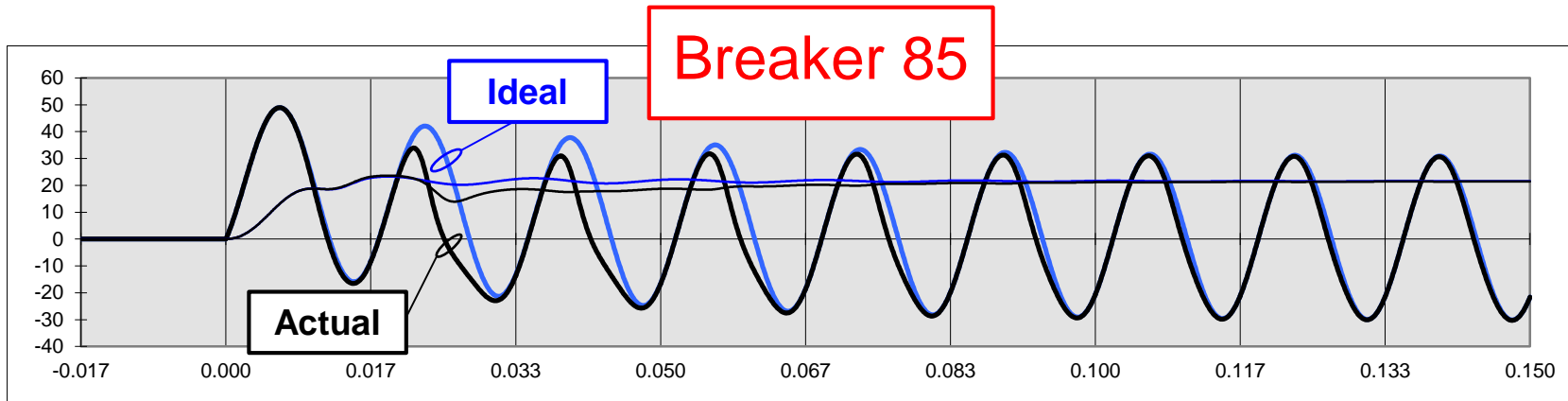
CT Saturation Theory Investigation CB 90

INPUT PARAMETERS:

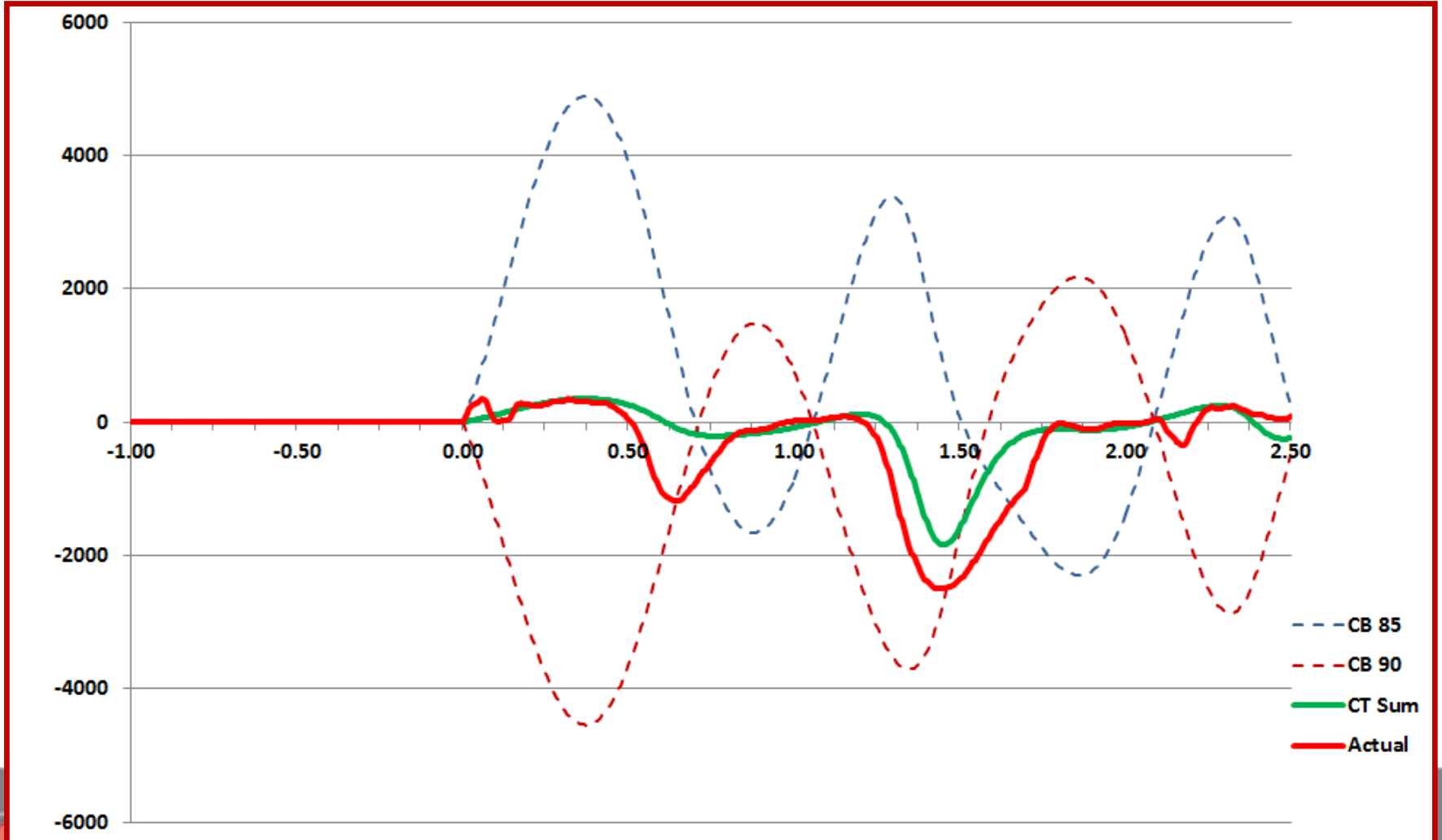
Inverse of sat. curve slope =	S =	25.5	---
RMS voltage at 10A exc. current =	Vs =	210	volts rms
Turns ratio = $n_2/1$ =	N =	100	---
Winding resistance =	Rw =	0.100	ohms
Burden resistance =	Rb =	0.750	ohms
Burden reactance =	Xb =	0.075	ohms
System X/R ratio =	XoverR =	13.5	---
Per unit offset in primary current =	Off =	-0.72	$-1 < \text{Off} < 1$
Per unit remanence (based on Vs) =	λ_{rem}	-0.48	---
Symmetrical primary fault current =	Ip =	2,000	amps rms

ENTER:

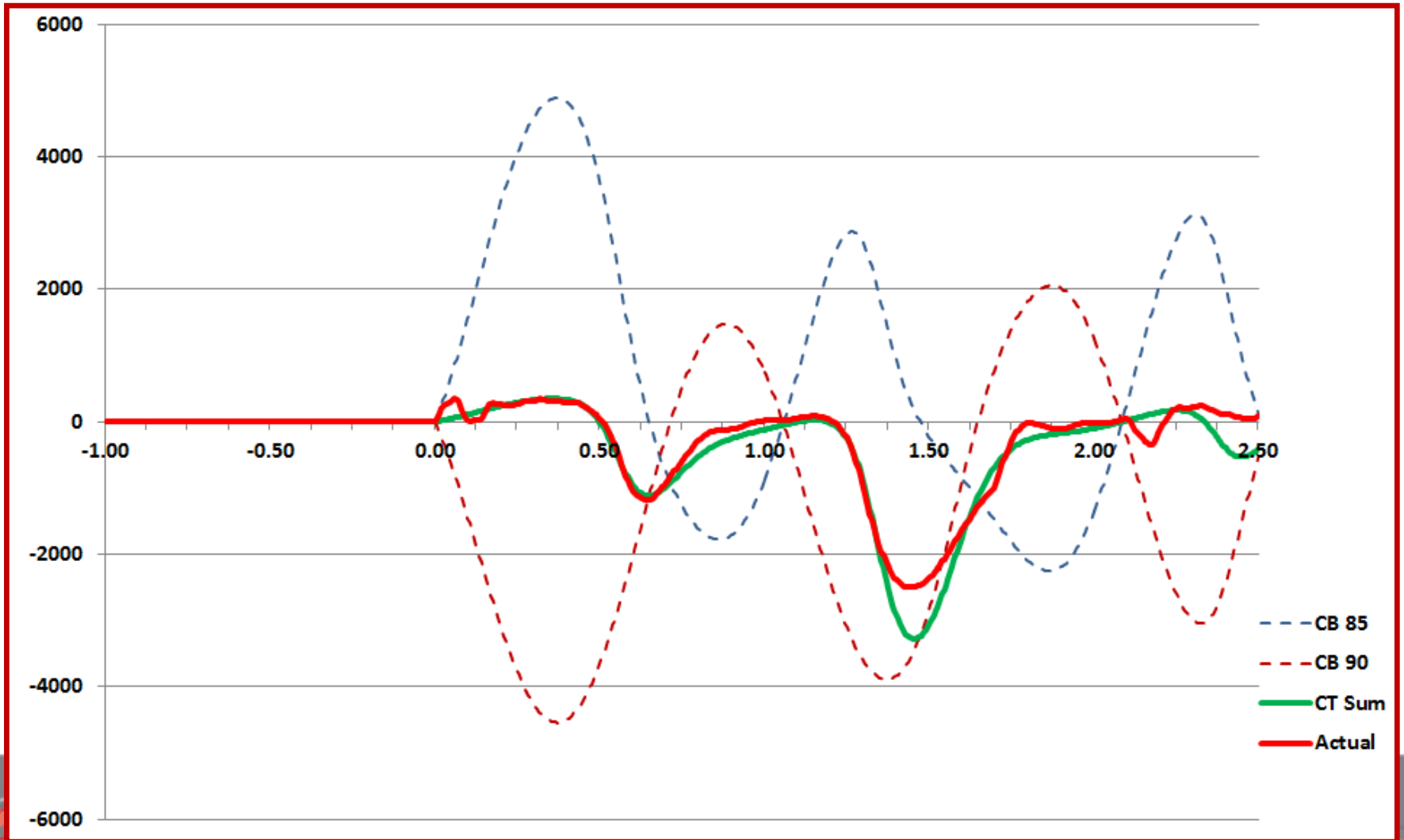
CT Saturation With 500:5 CT Ratio



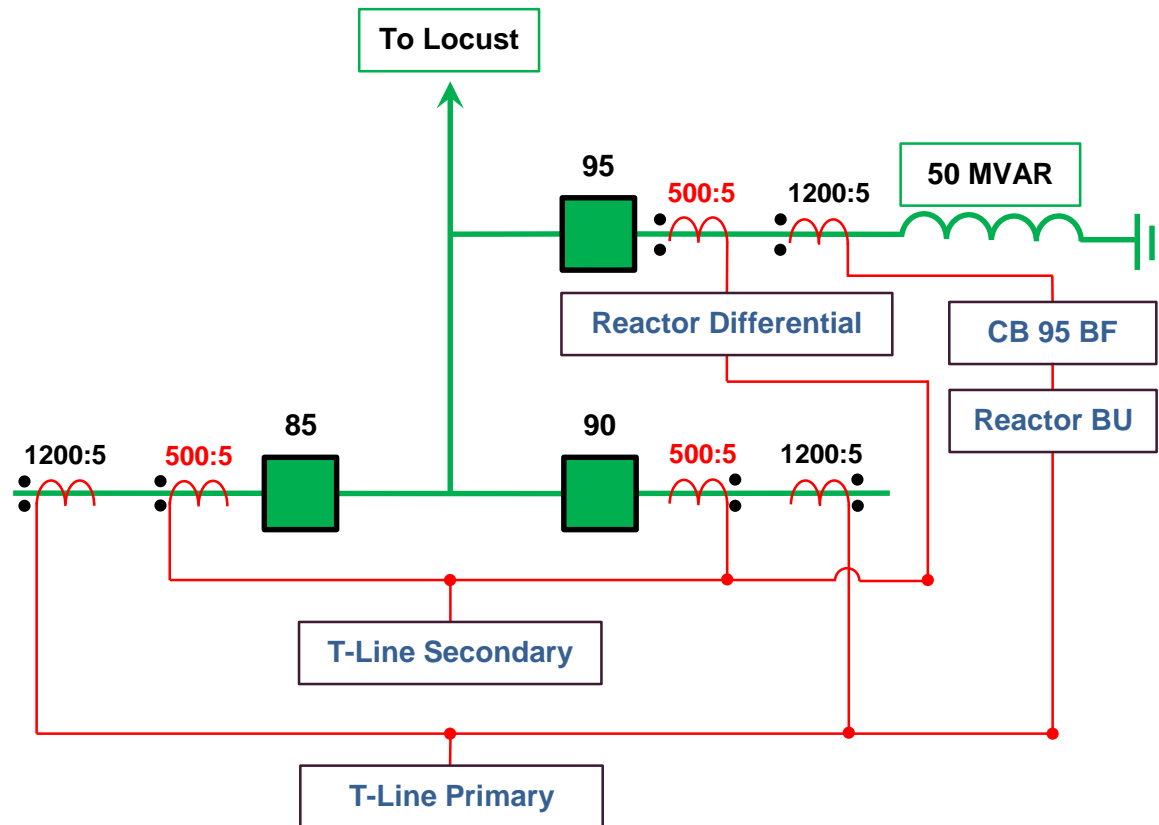
CT Saturation With 500:5 CT Ratio



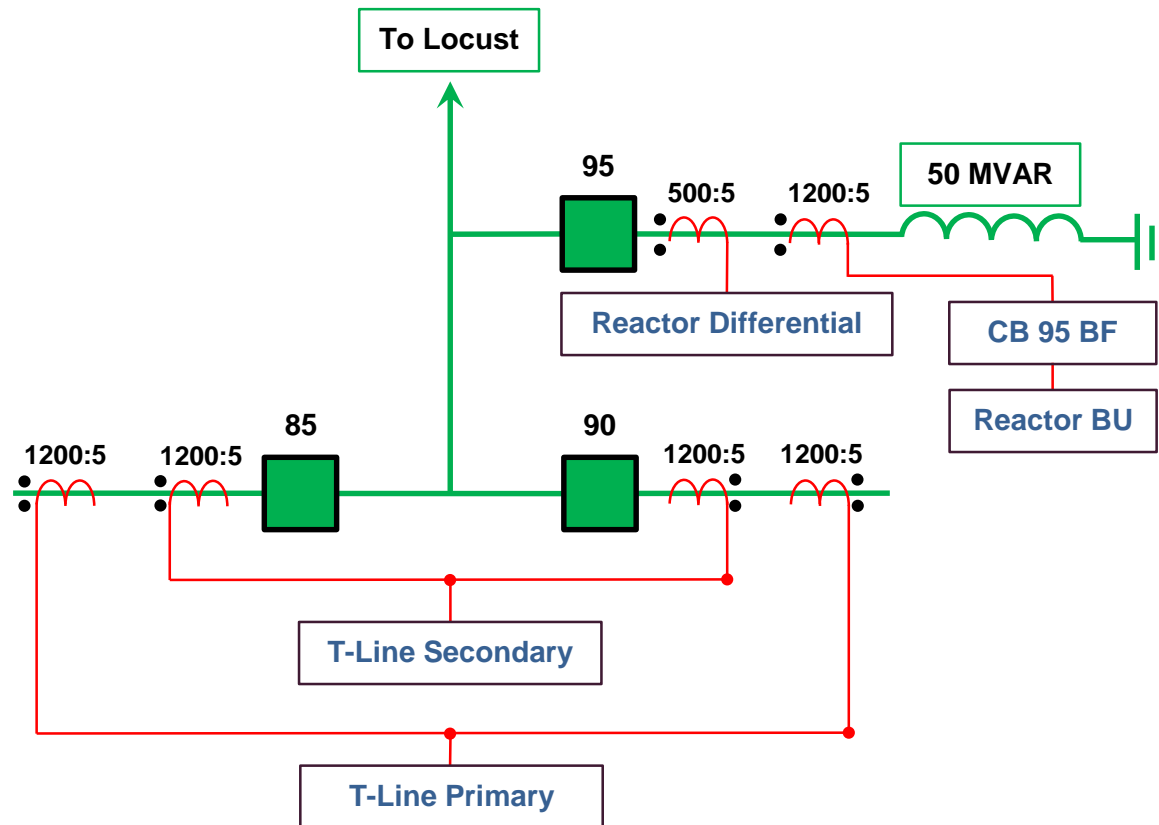
CT Saturation With 500:5 CT Ratio



CT Saturation Solutions

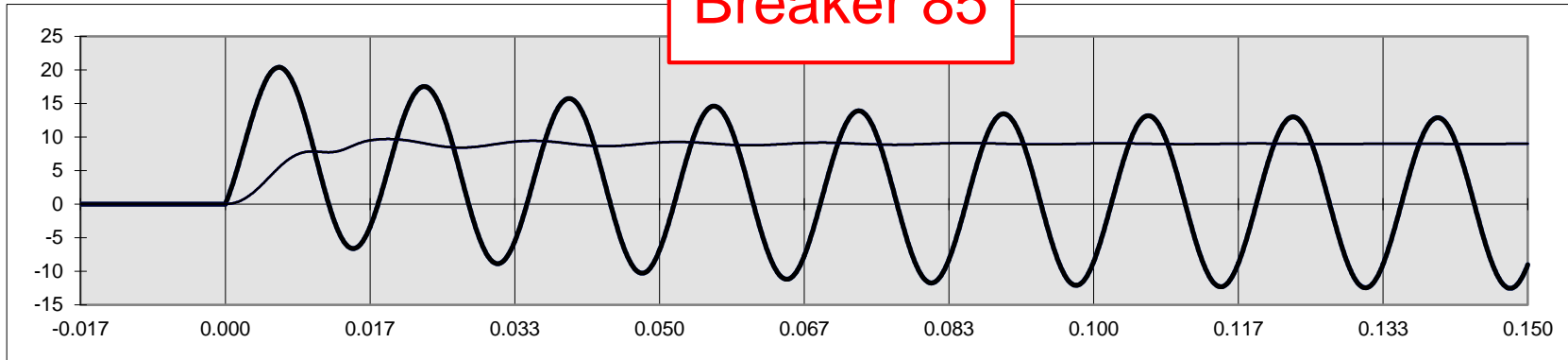


CT Saturation Solutions

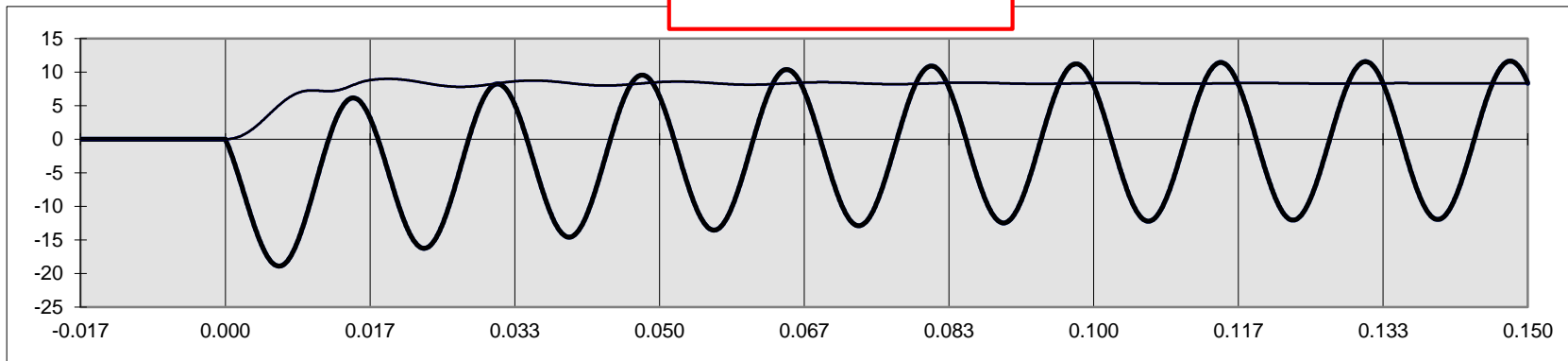


CT Saturation With 1200:5 CT Ratio

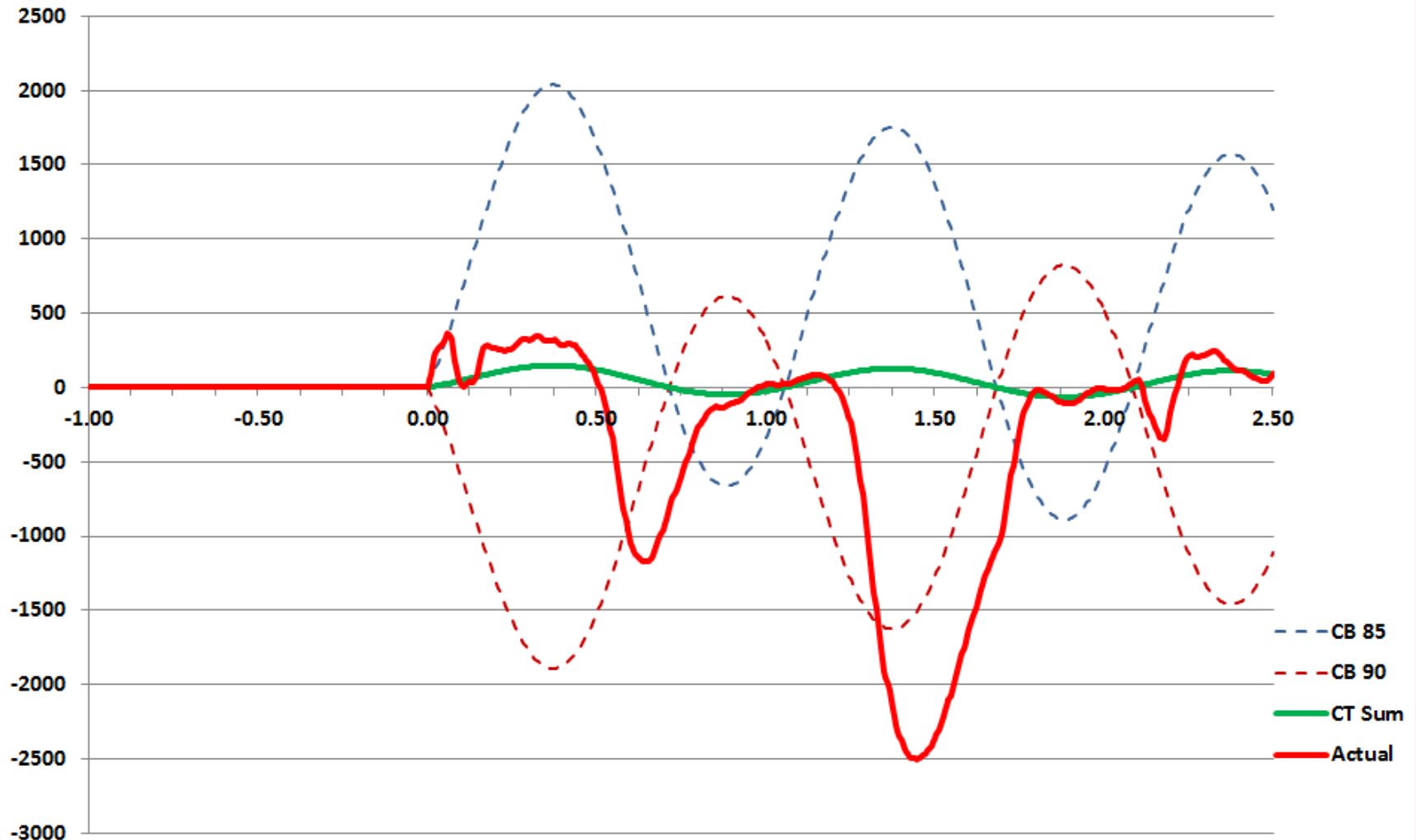
Breaker 85



Breaker 90



CT Saturation With 1200:5 CT Ratio



Lessons Learned

- **CT saturation can cause mis-operation of non-differential elements, such as ground distance elements.**
- **ALWAYS be wary of the effects of CT saturation on relay elements, especially when using less than full CT ratio.**
- **ALWAYS analyze un-filtered relay event records to look for waveform distortions that could indicate CT saturation.**

Questions???

