

Improvements in the Operation of a Distance Relay During Resistive Faults

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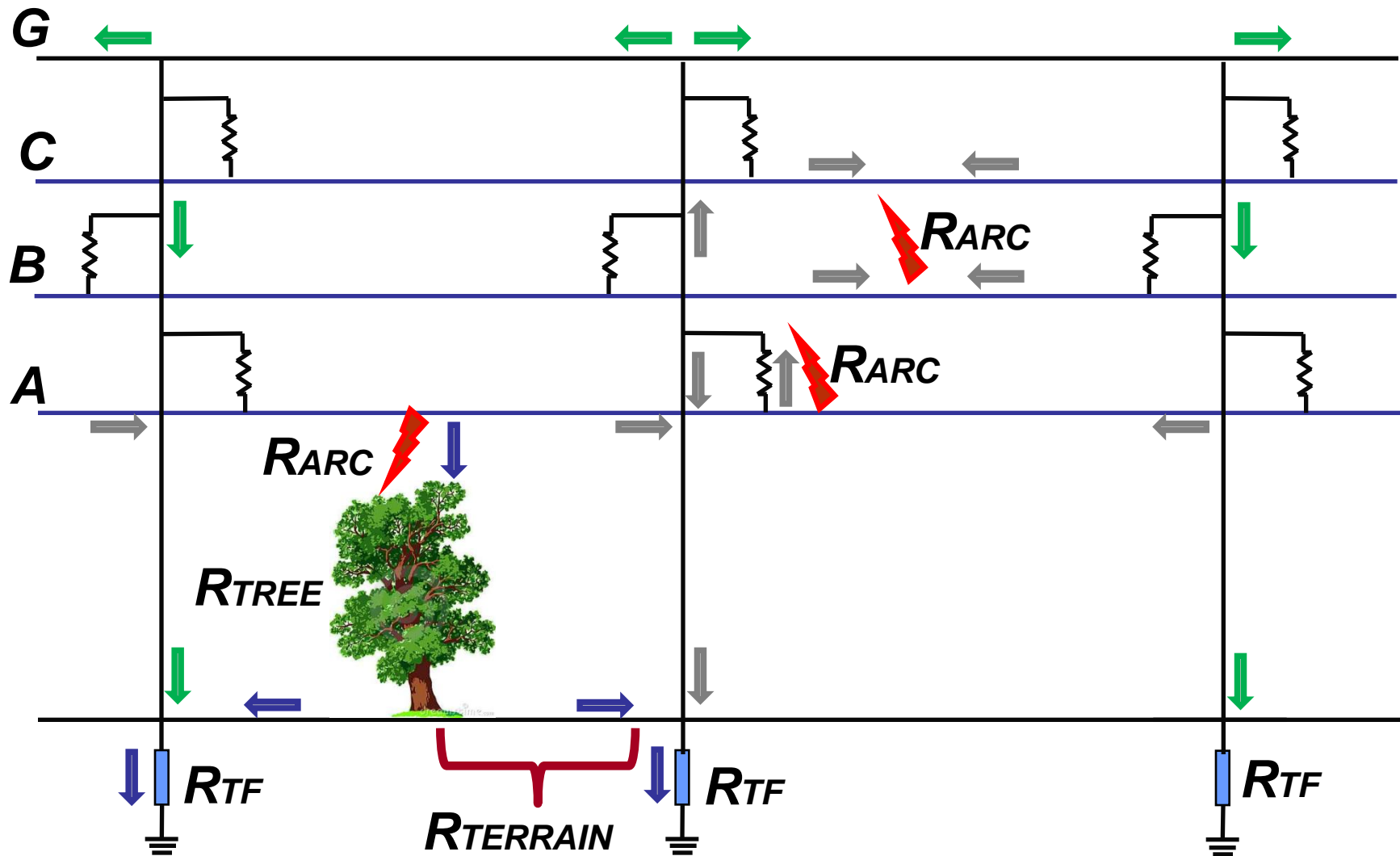
Izaskun García



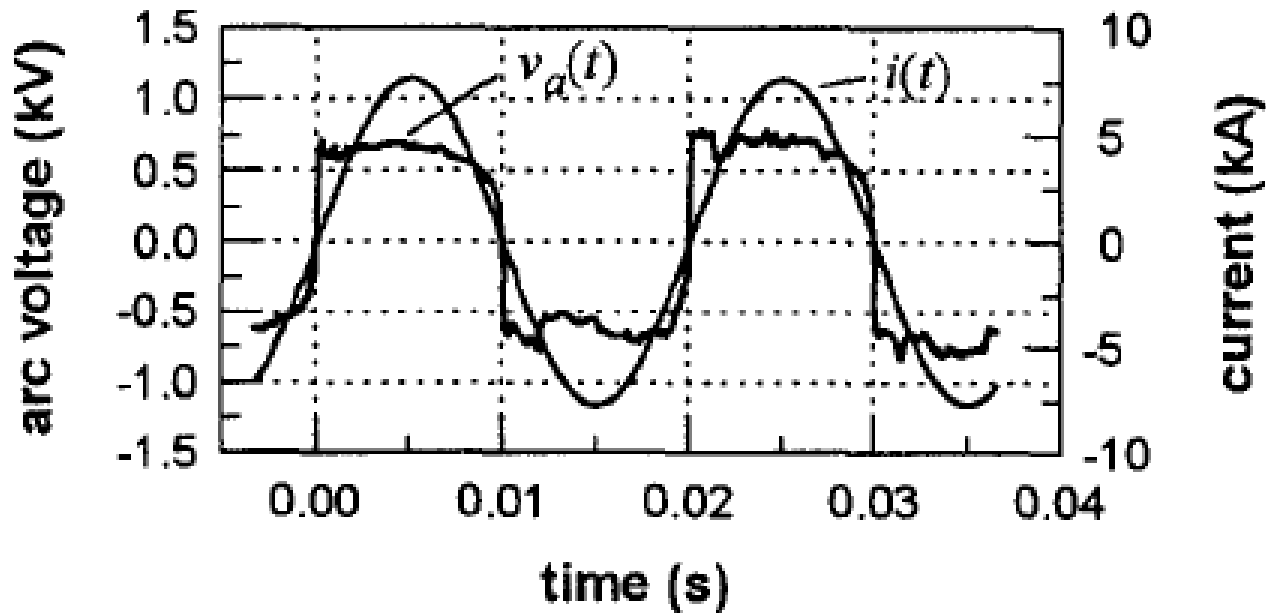
Overview

- Fault resistance
- Influence on Mho and Quadrilateral characteristics
- Special conditions affecting the polarization of the ground reactance line
 - Ground fault during open pole
 - Phase-phase-ground fault
- Resistive reach calculation
- RTDS simulations

Fault Resistances and Current Flow



Arc Resistance

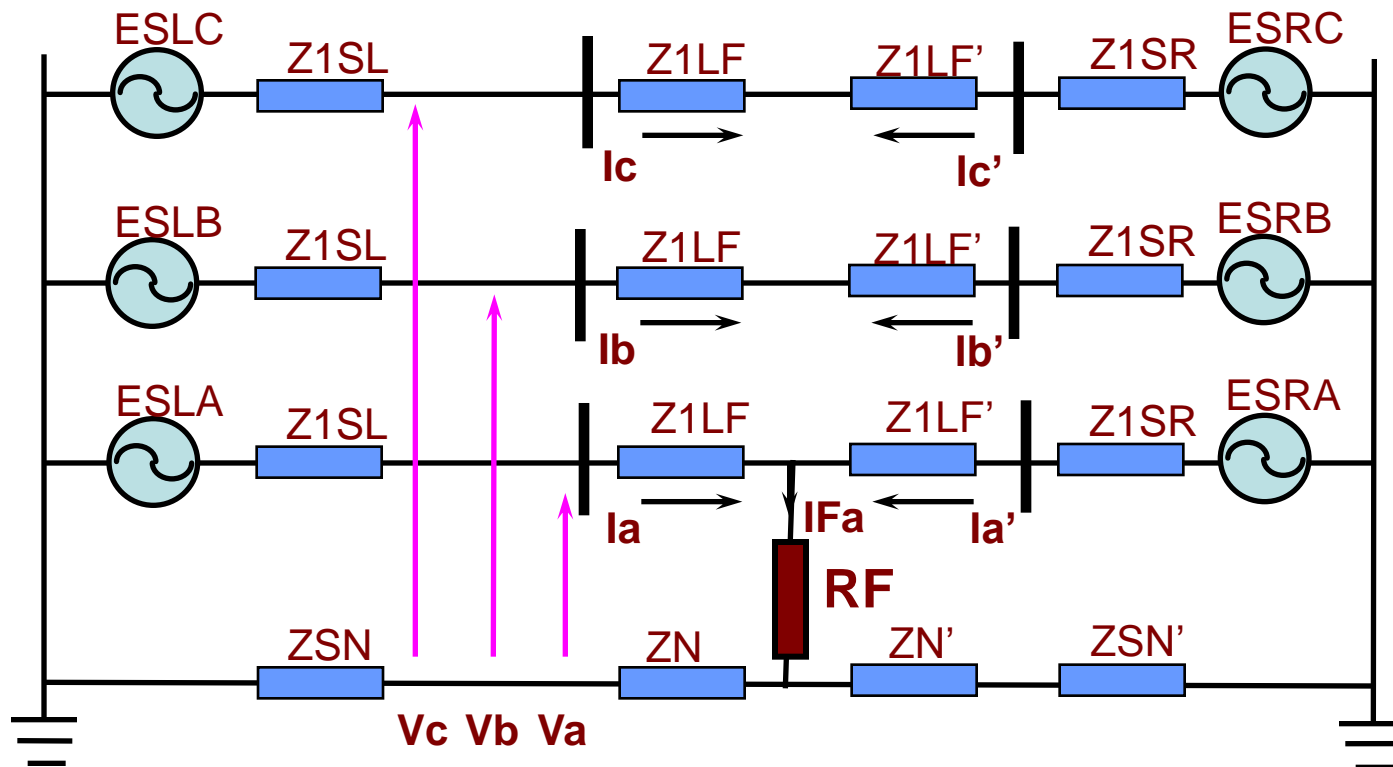


$$R_{arc} = K \cdot \frac{L_{arc}}{I_{arc}^n} \quad n \geq 1$$

AG Fault Loop

$$V_a = I_{aeq} \cdot Z_{1LF} + I_{Fa} \cdot R_F \quad I_{aeq} = I_a + I_0 \cdot K_0$$

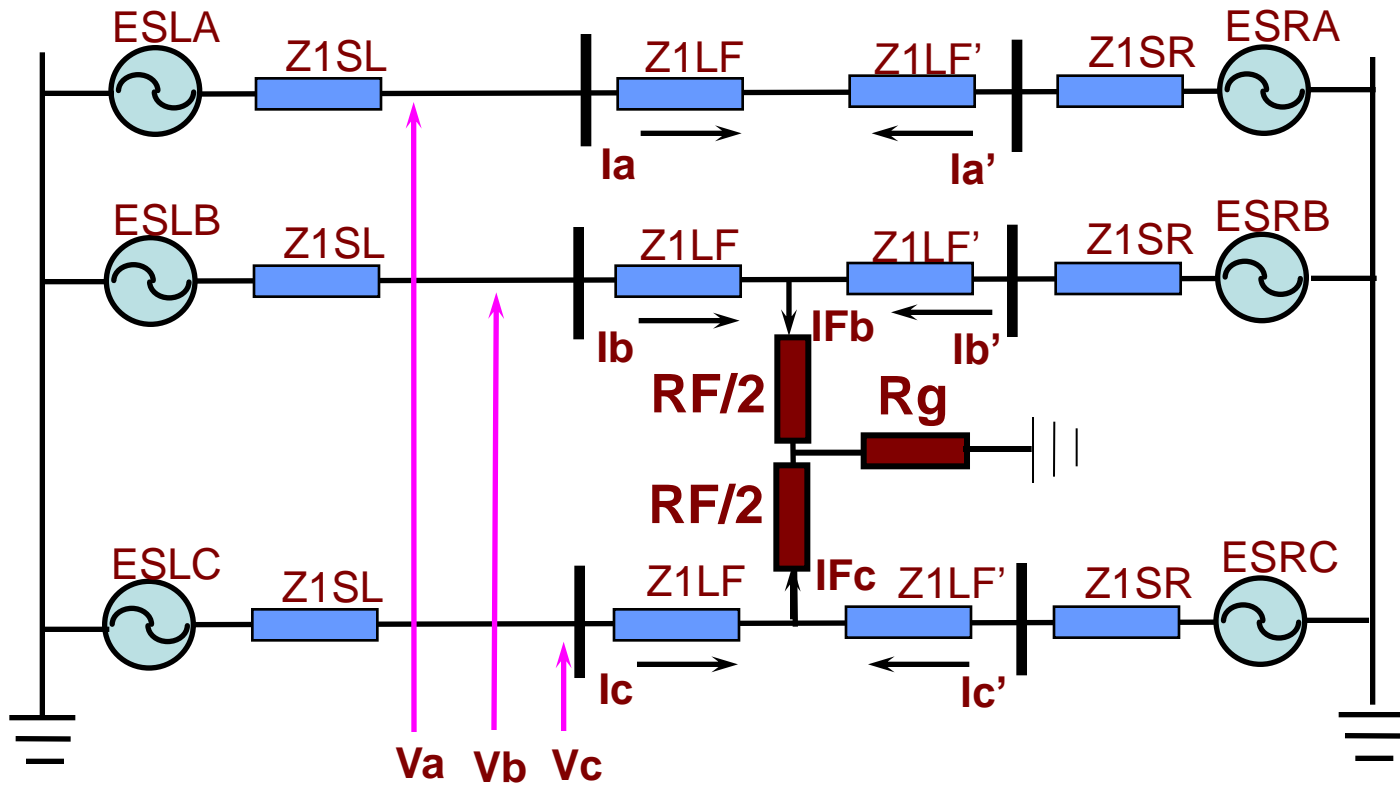
$$K_0 = \frac{Z_{L0} - Z_{L1}}{Z_{L1}}$$



BC Fault Loop

$$V_{bc} = I_{bc} \cdot Z1LF + IF_{bc} \cdot RF / 2$$

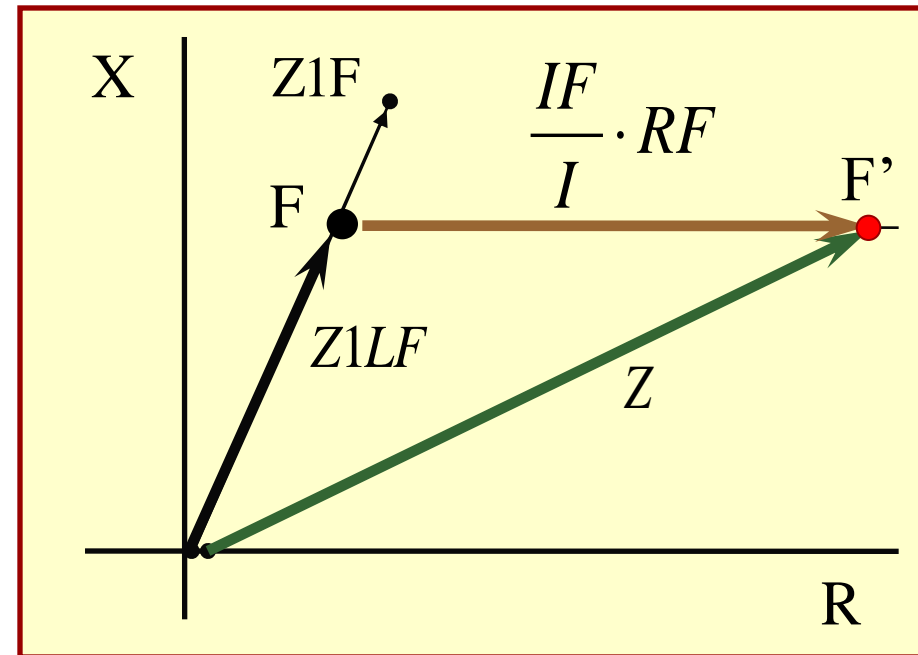
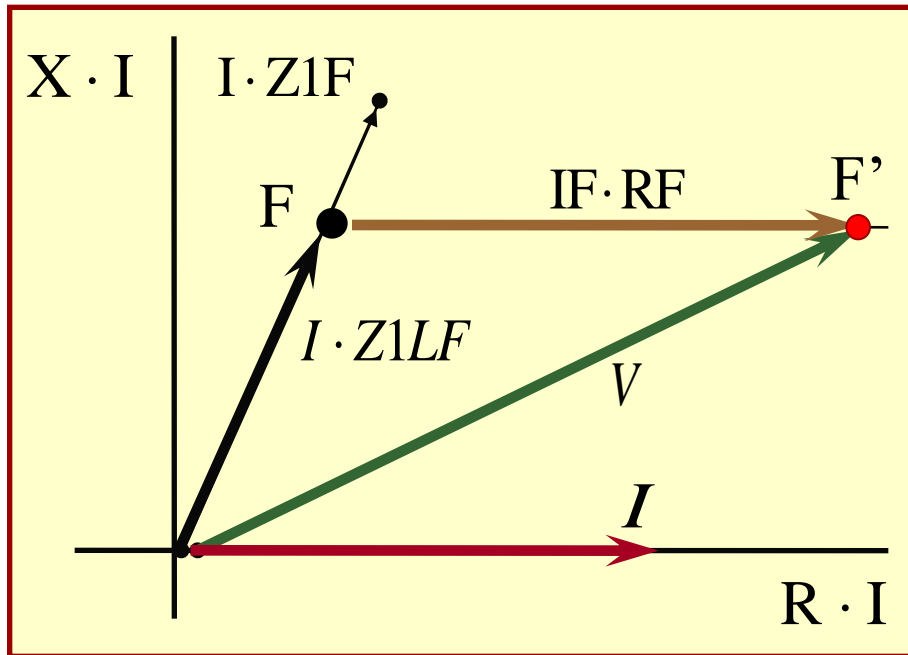
$$IFbc = IFb - IFc$$



Apparent Fault Resistance

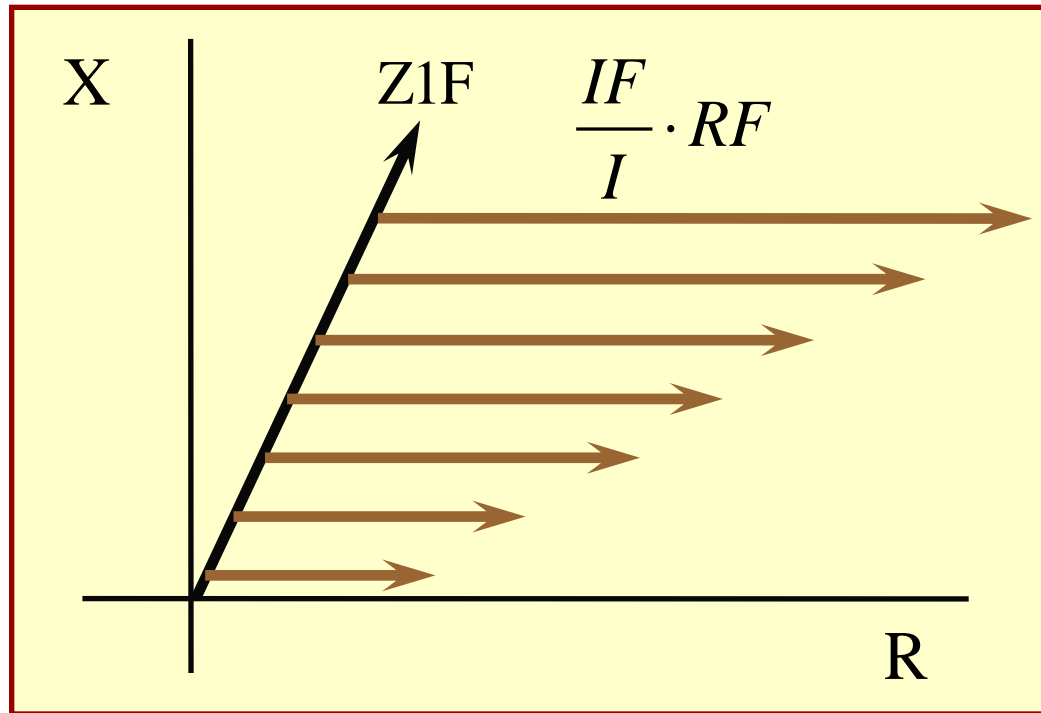
$$V = I \cdot Z_{1LF} + I F \cdot R_F$$

$$Z = Z_{1LF} + \frac{I F \cdot R_F}{I}$$

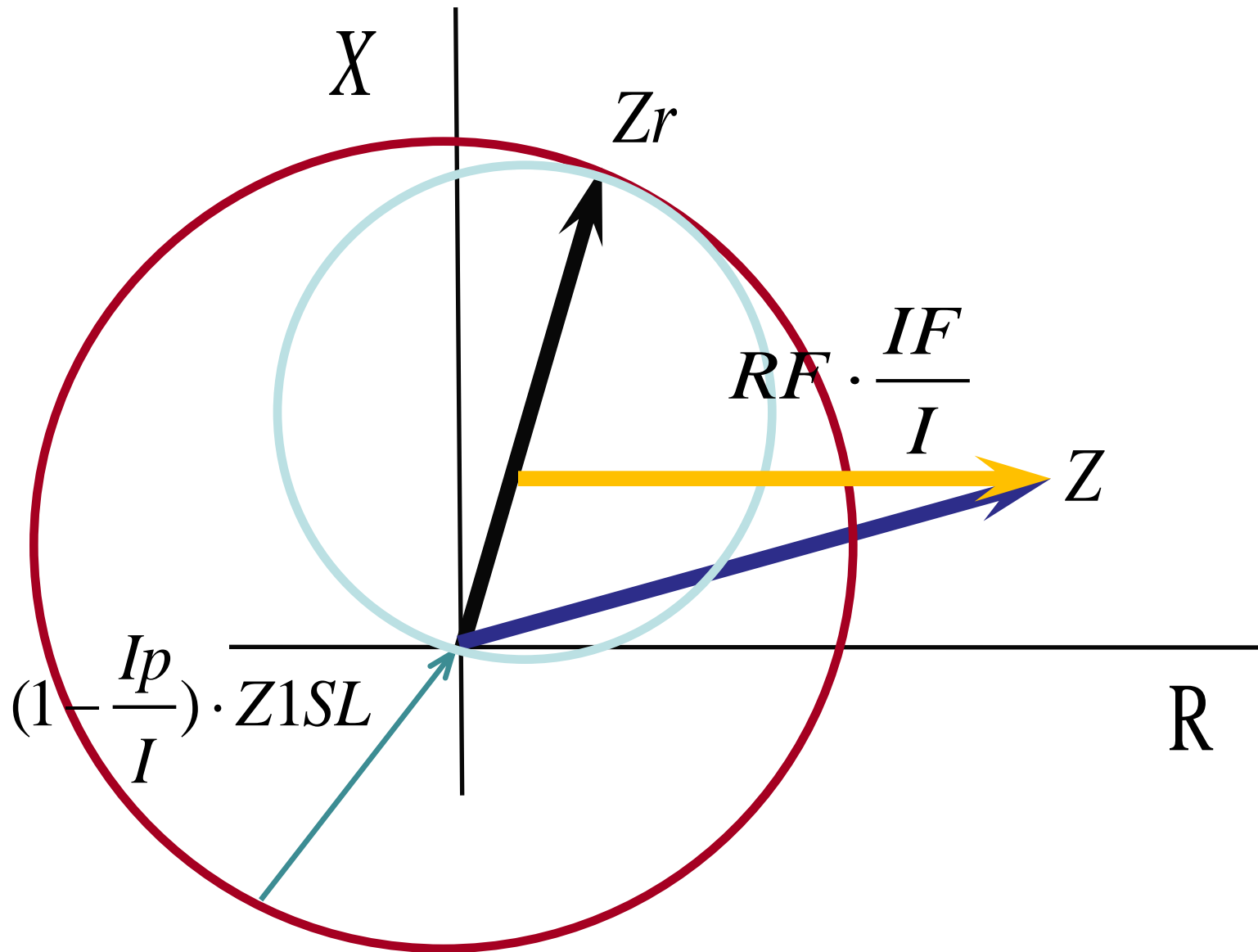


Infeed on Apparent Fault Resistance

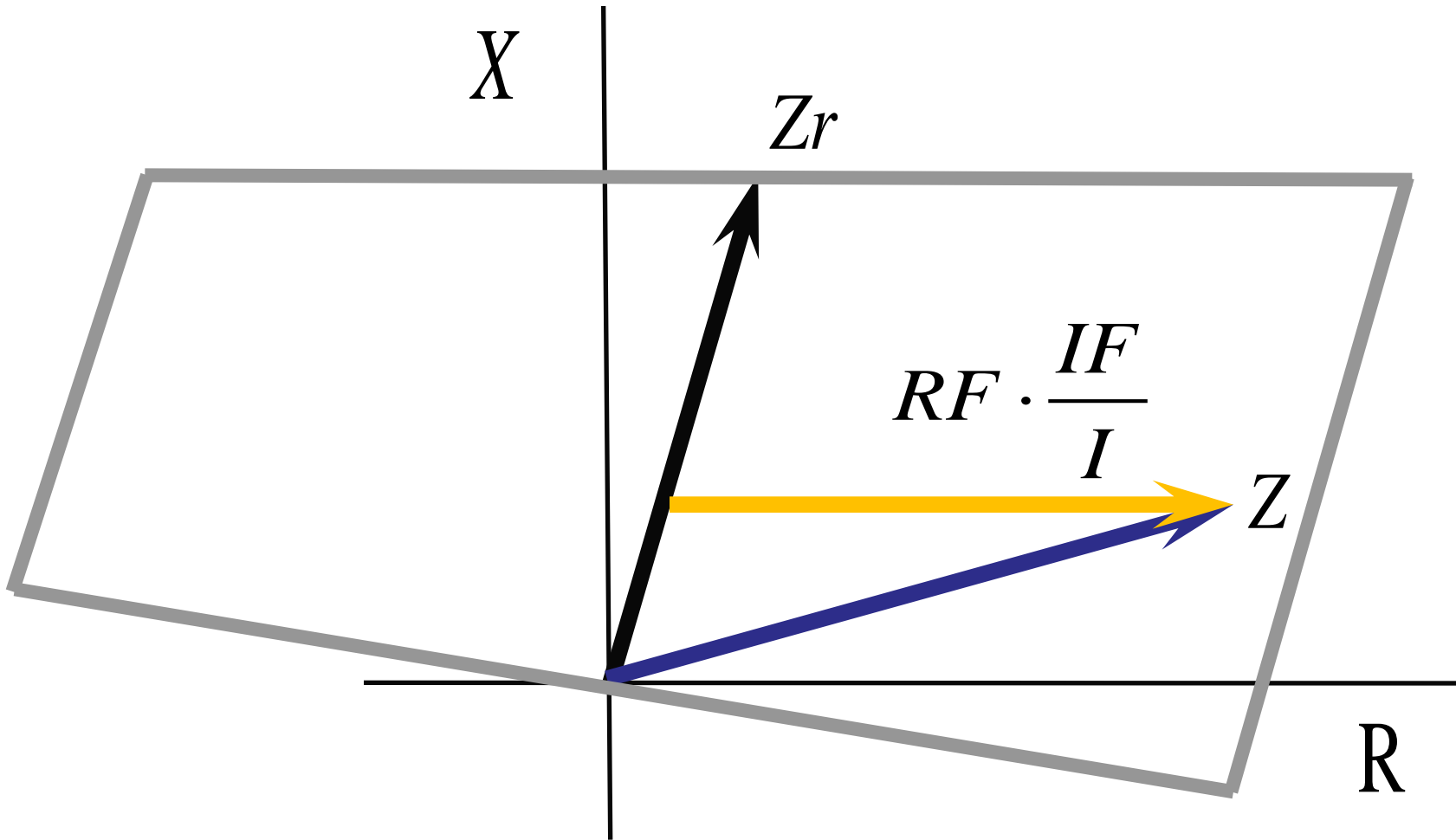
- Amplification of the apparent fault resistance
- Not applicable for arc resistances



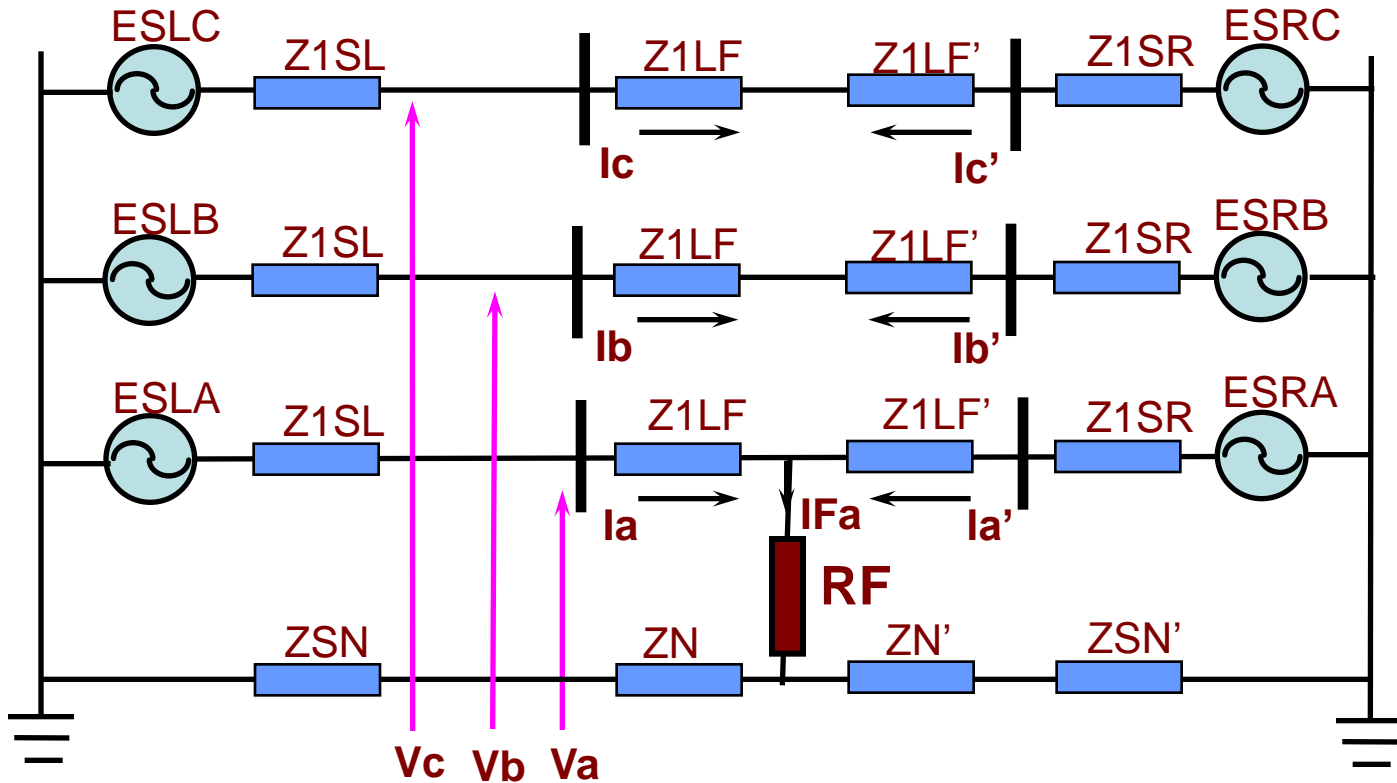
Influence on Mho Characteristic



Influence on Quadrilateral Characteristic

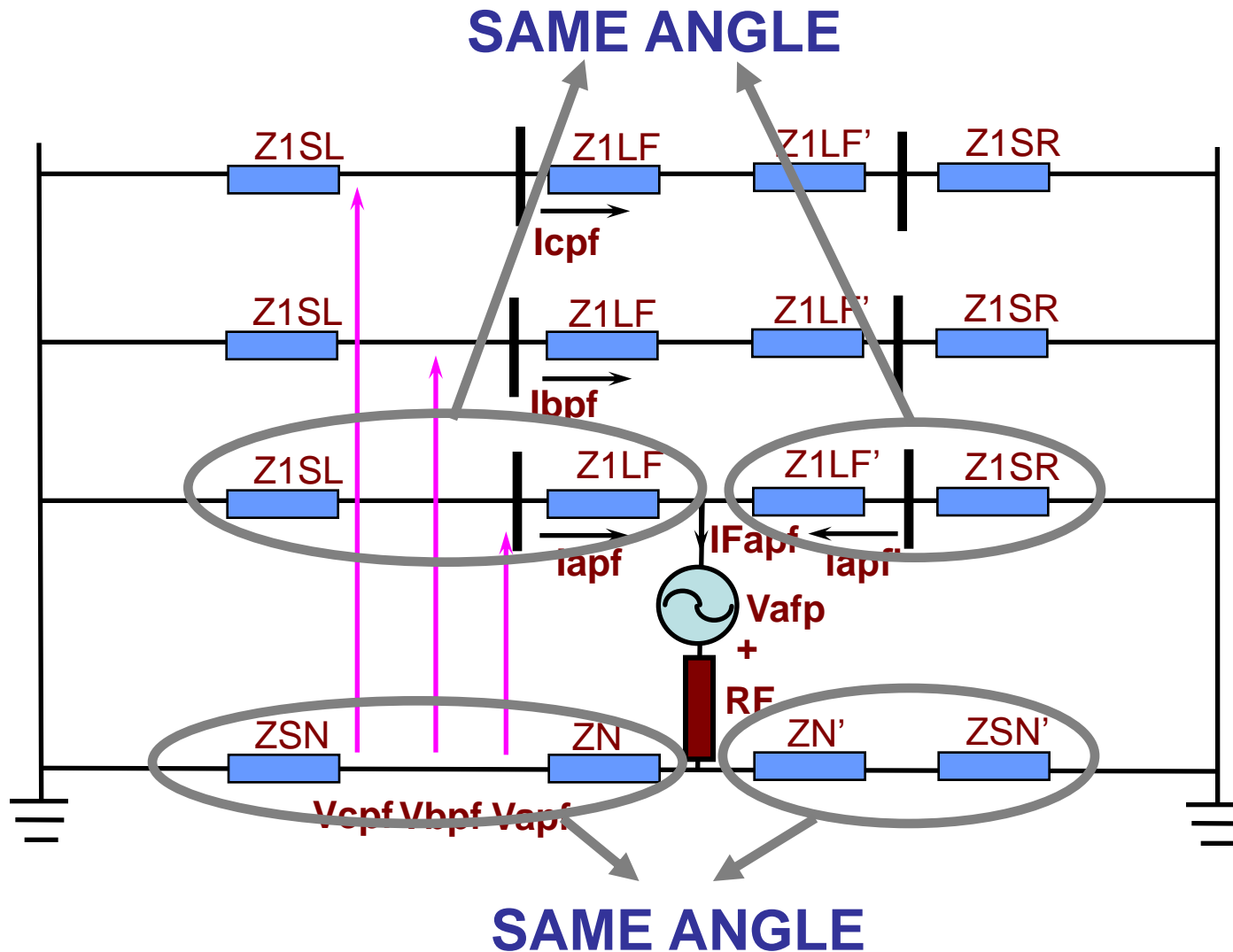


Load Flow Effect: Fault



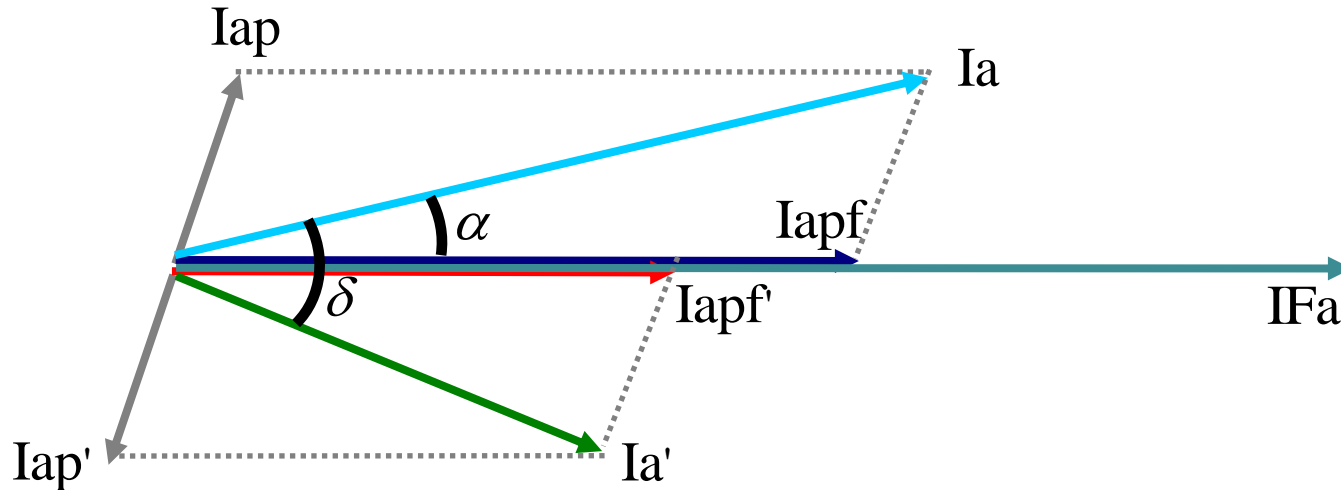
[illegible]

Load Flow Effect: Pure Fault

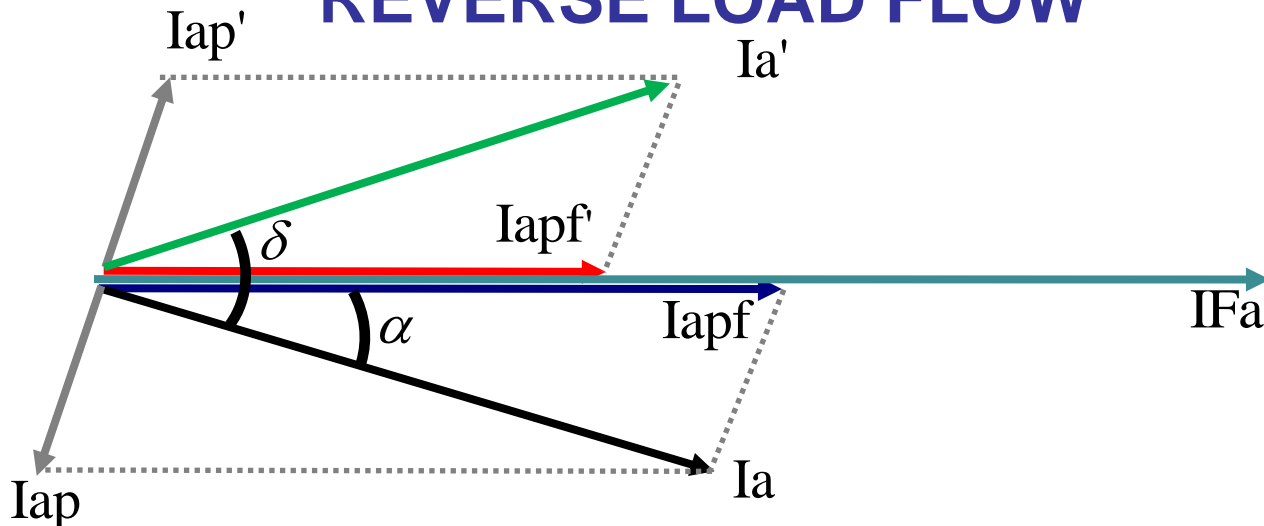


Load Flow Effect

FORWARD LOAD FLOW

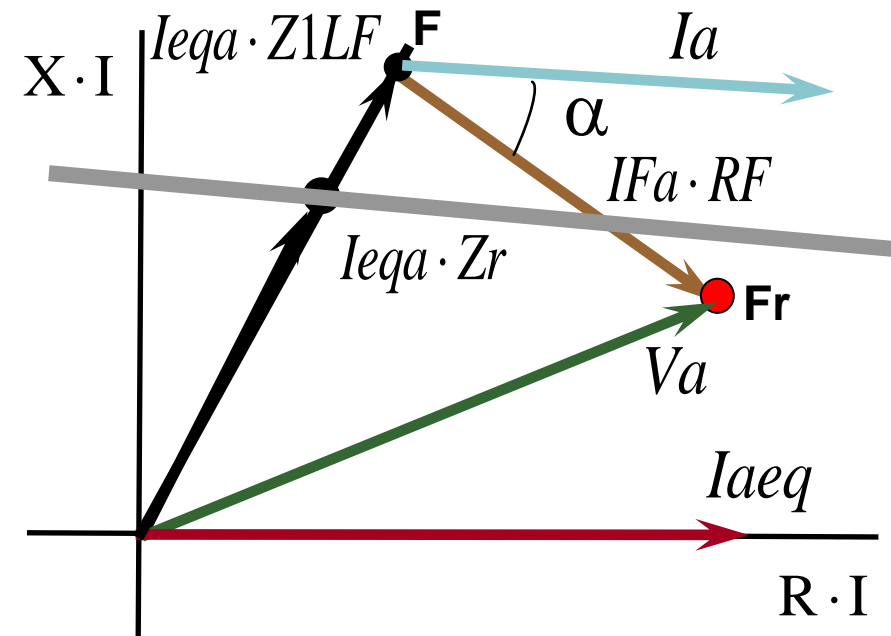


REVERSE LOAD FLOW

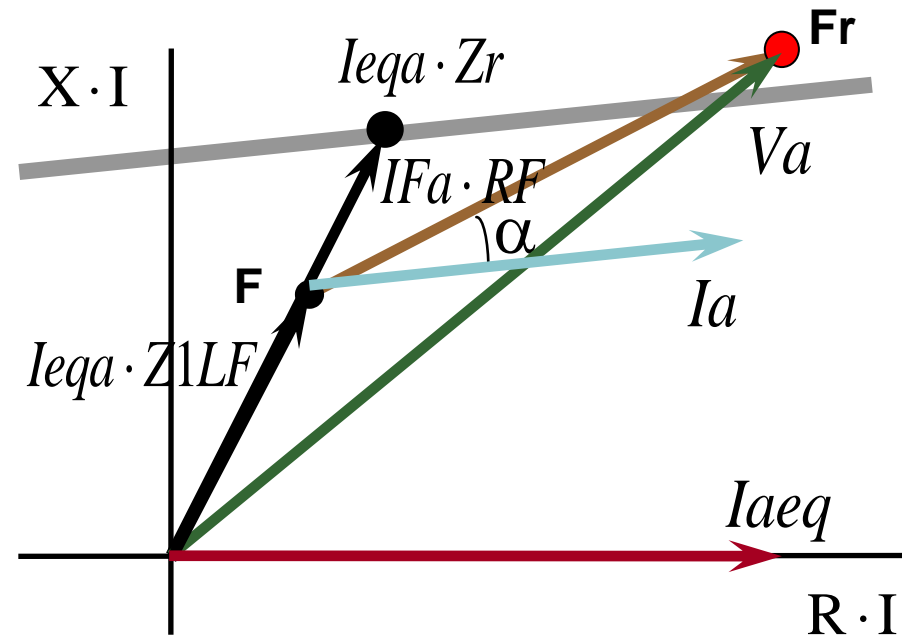


Quadrilateral Characteristic: Phase Polarization

FORWARD LOAD FLOW OVERREACHING

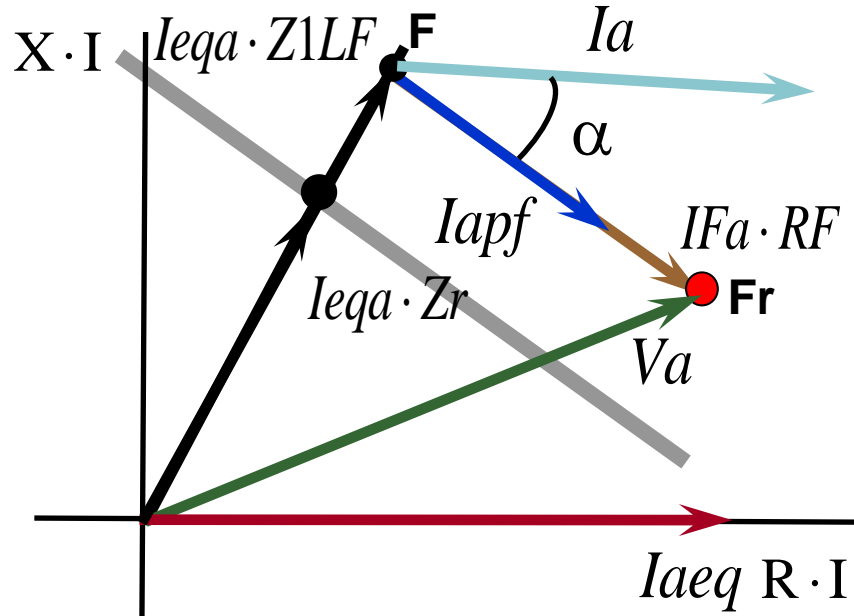


REVERSE LOAD FLOW UNDERREACHING

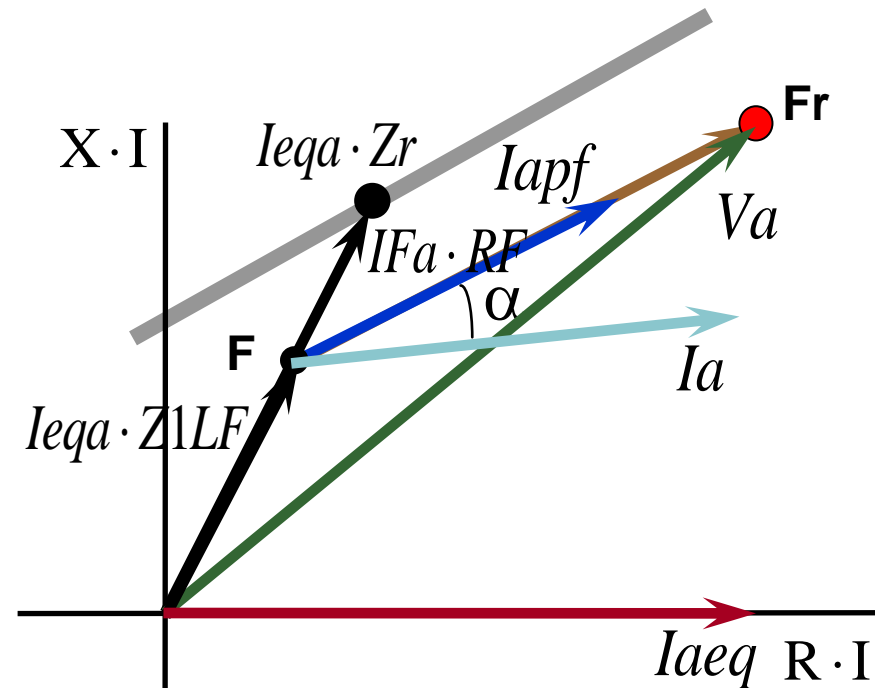


Quadrilateral Characteristic: Pure Fault Phase Polarization

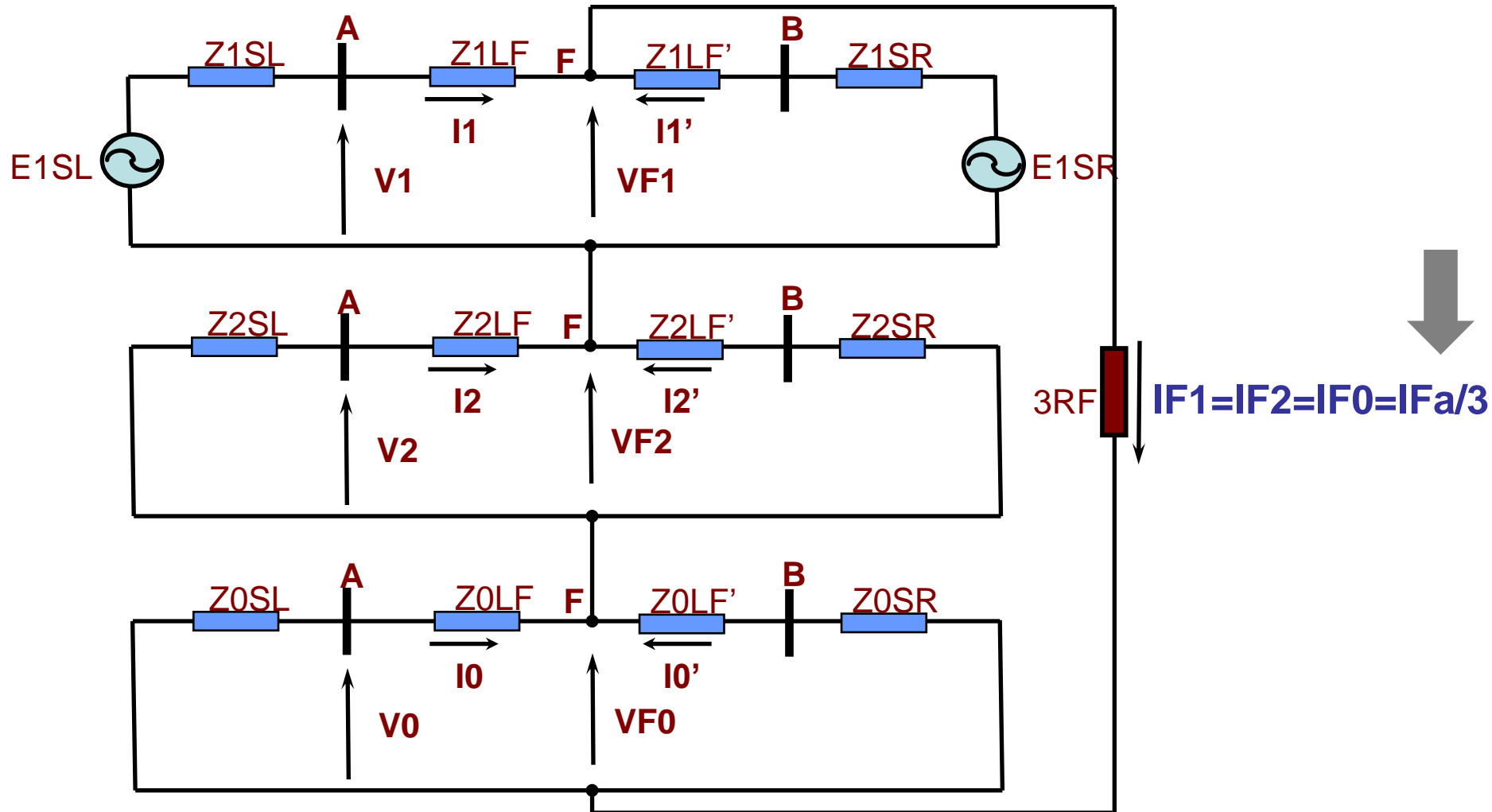
FORWARD LOAD FLOW



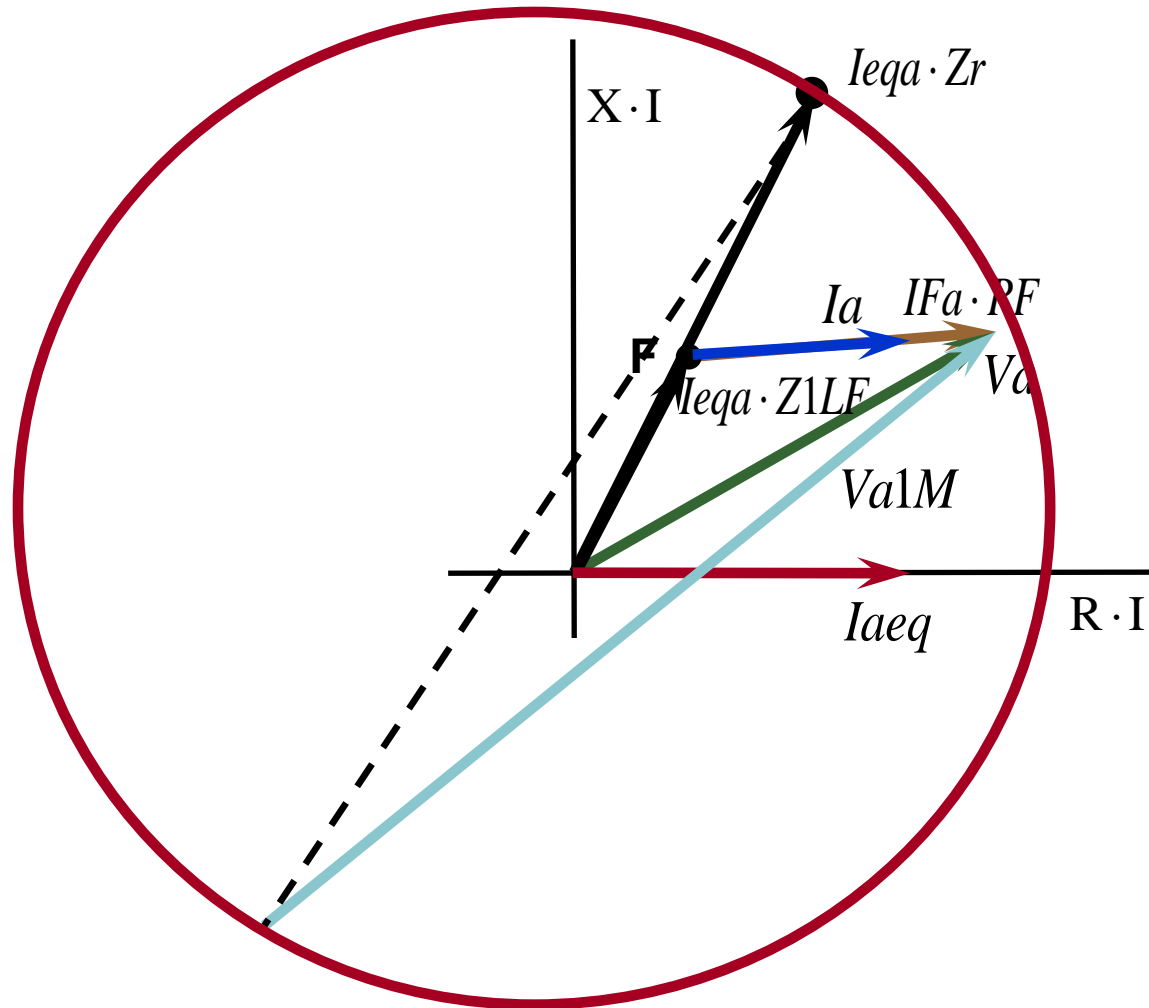
REVERSE LOAD FLOW



Quadrilateral Characteristic: I2 and I0 Polarization

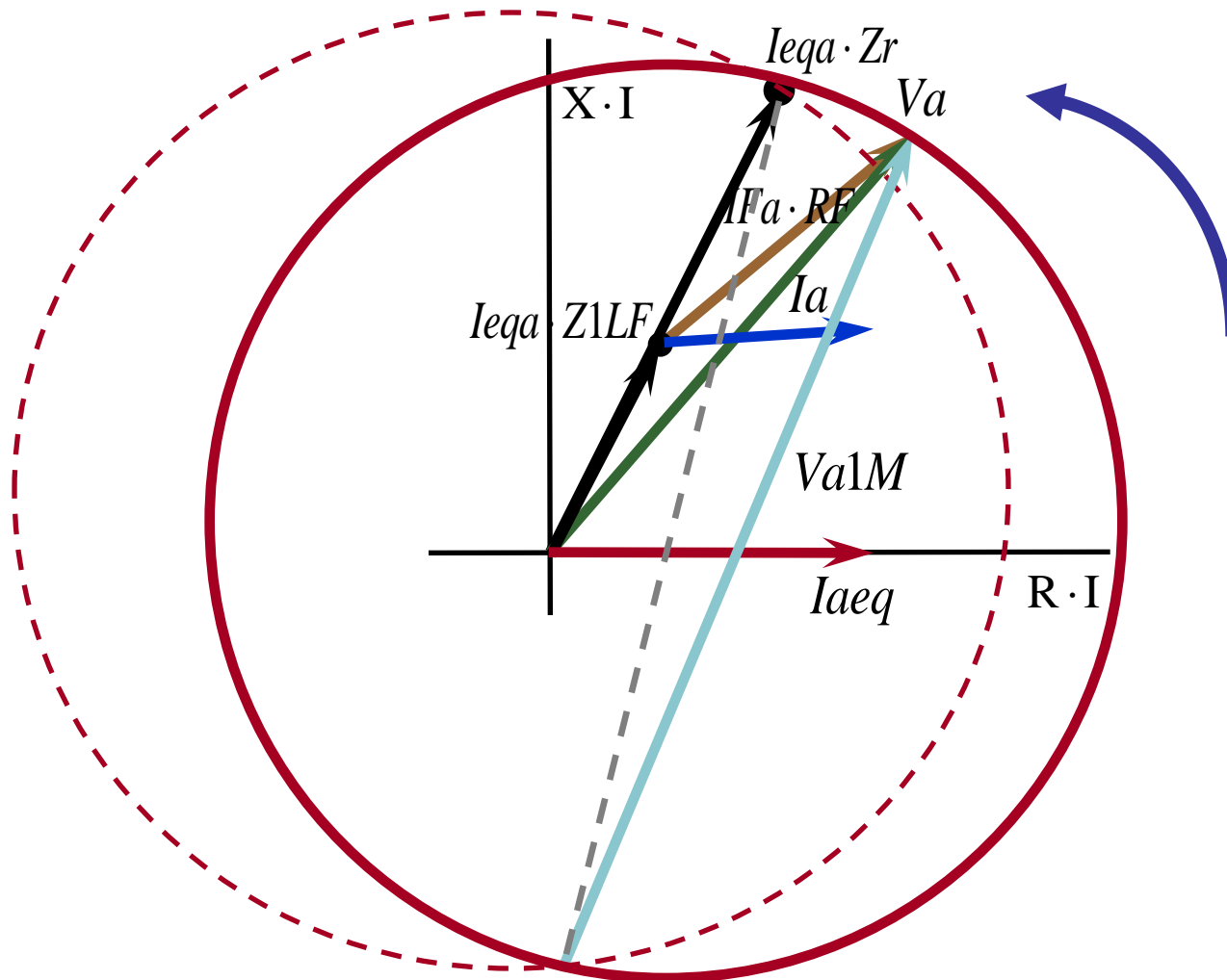


NO LOAD FLOW



Mho Characteristic

REVERSE LOAD FLOW



System Non-Homogeneity

$$K1 = \frac{1}{3 \cdot (1 + \frac{Z0X}{Z0Y})}$$

$$\arg(\frac{I_{a_{pf}}}{I_{Fa}}) = \arg(\frac{Z1X + (-Z1X \cdot K1 + Z0X \cdot K1 - Z0Y \cdot K2 + Z1Y \cdot K2)}{Z1X + Z1Y})$$

$$\arg(\frac{I_{a2}}{I_{Fa}}) = \arg(\frac{Z1X}{Z1X + Z1Y})$$

$$K2 = K1 \cdot \frac{Z0X}{Z0Y}$$

ZX: Z AT THE LEFT OF THE FAULT

$$\arg(\frac{I_0}{I_{Fa}}) = \arg(\frac{Z0X}{Z0X + Z0Y})$$

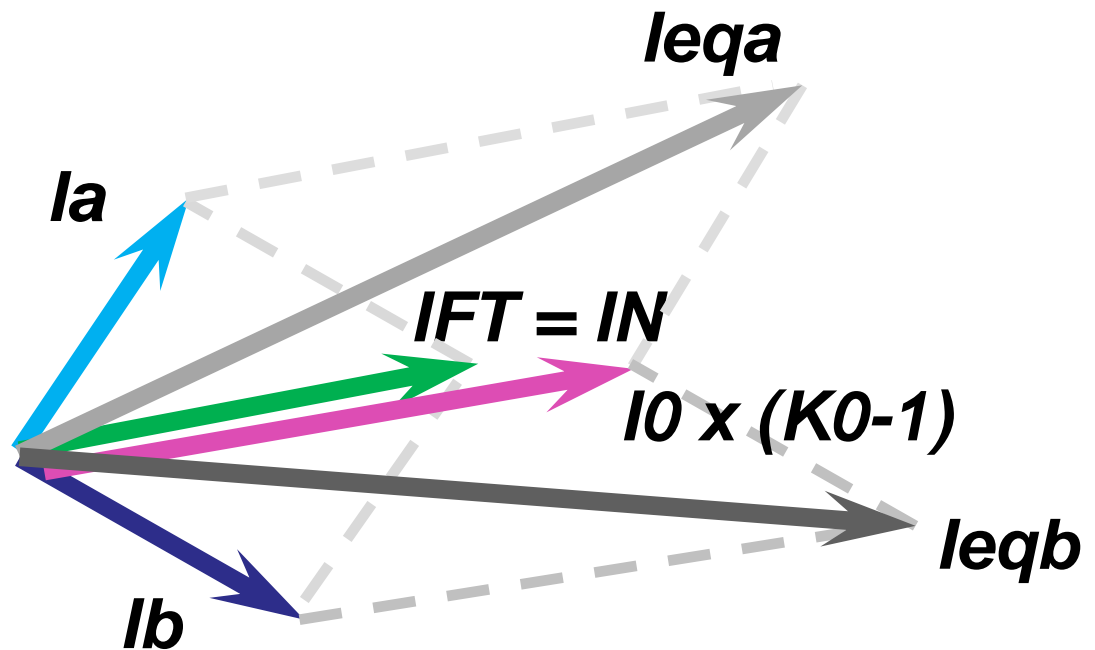
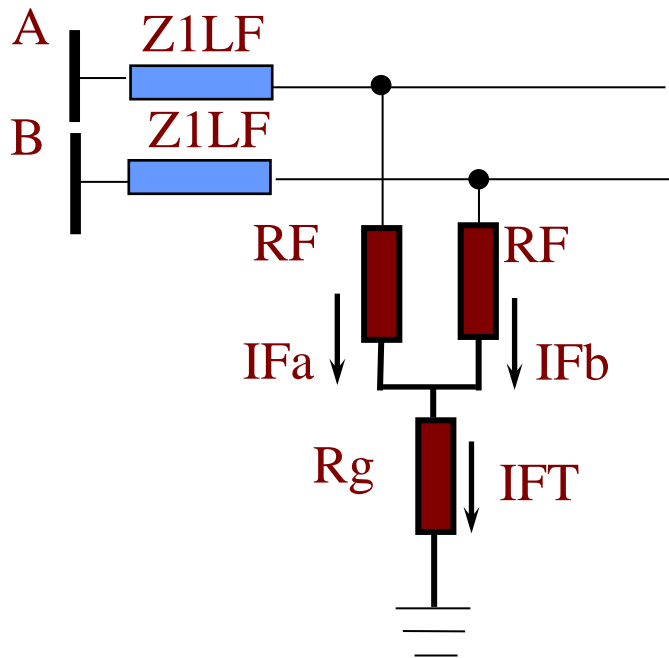
ZY: Z AT THE RIGHT OF THE FAULT

- I₂ is preferable than I_{apf} and I₀
- Tilt angle can be used

Single-Phase Fault with Open Pole

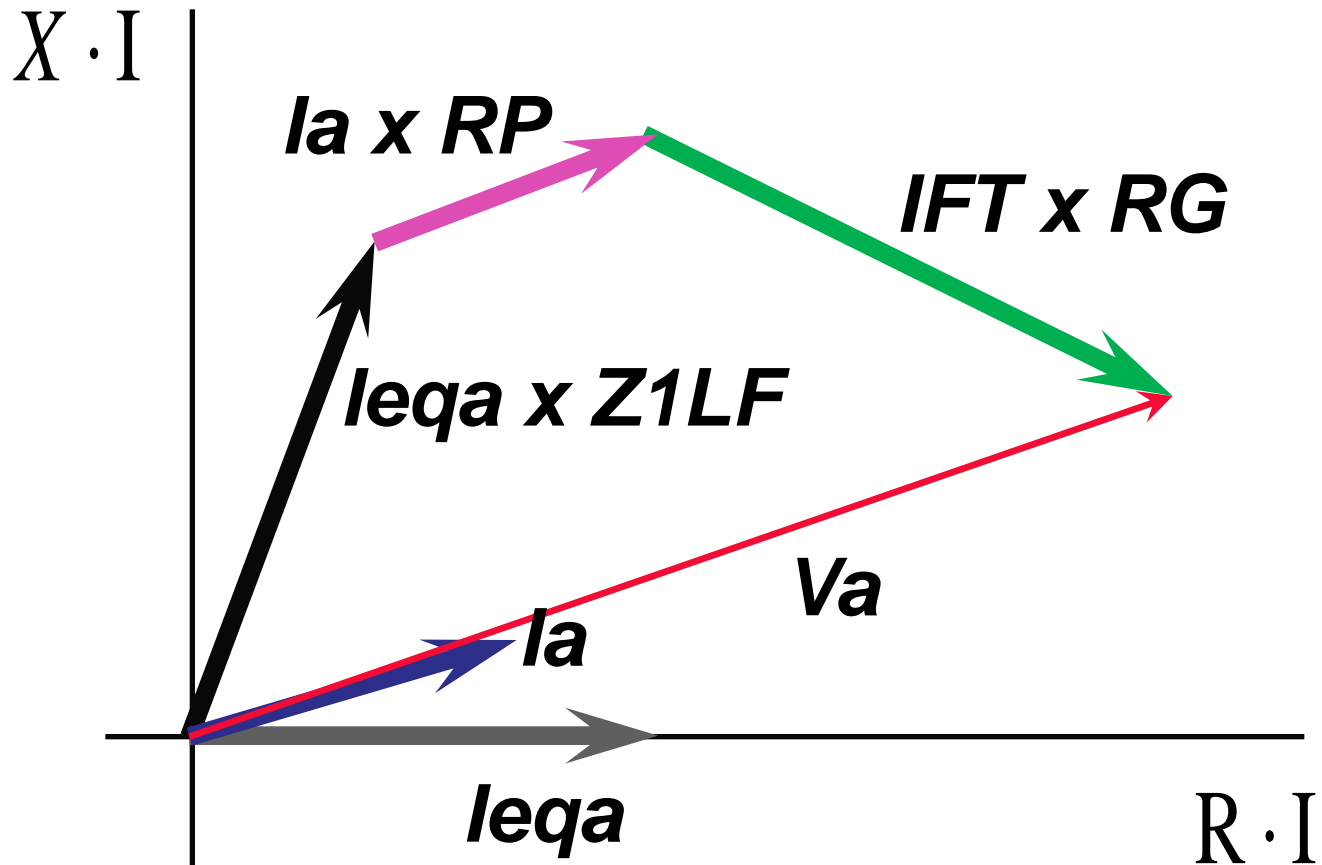
- I_2 is not reliable
- Pure fault phase current is chosen

Phase-Phase-Ground Fault



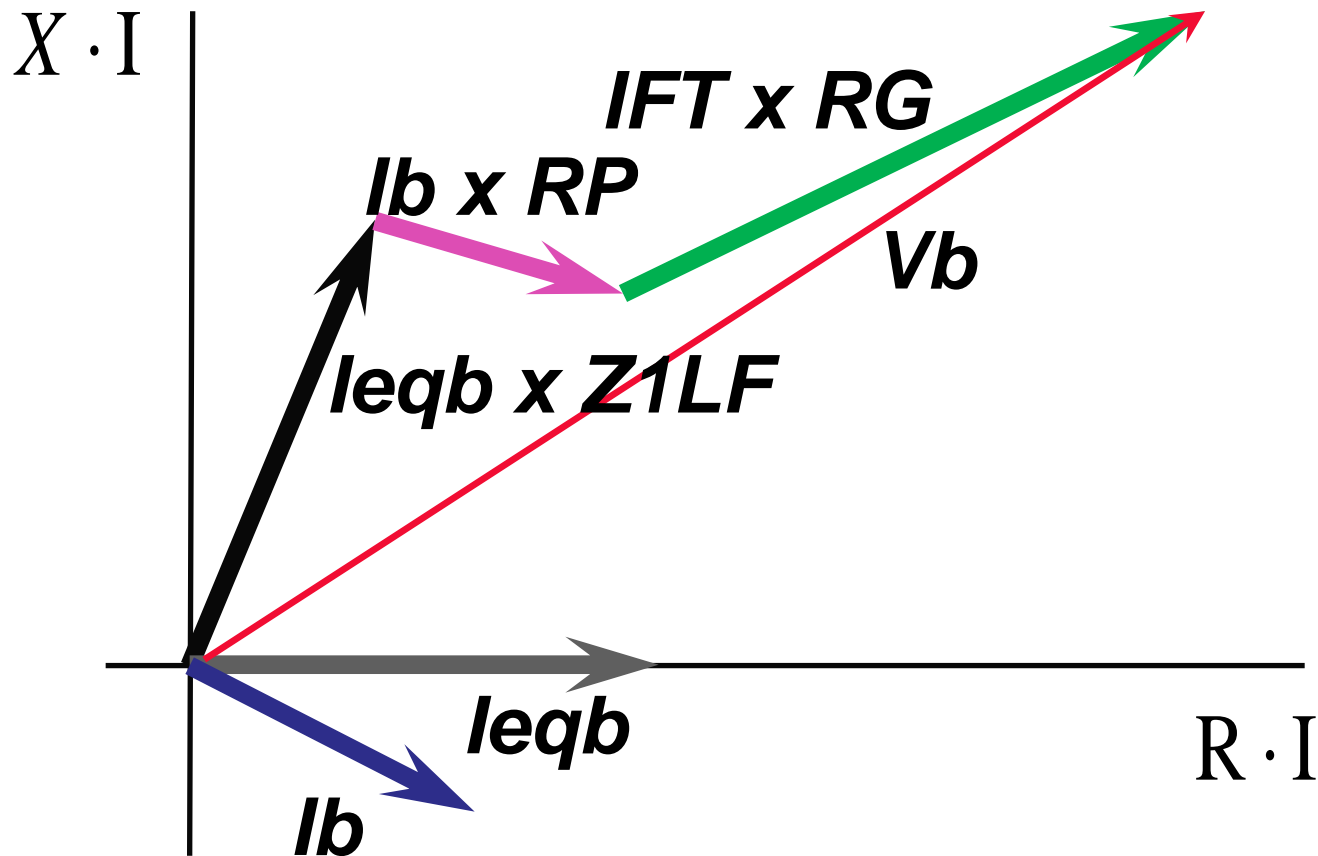
Phase-Phase-Ground Fault

LEADING PHASE (A): OVERREACHES

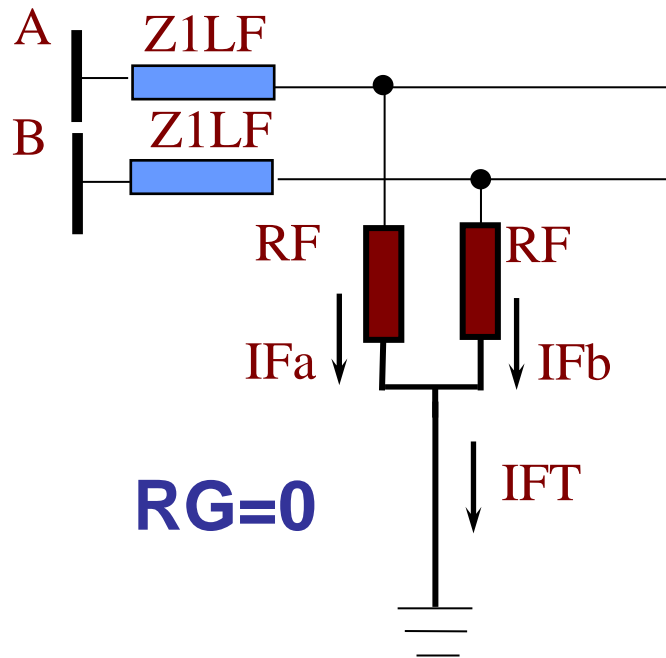


Phase-Phase-Ground Fault

LAGGING PHASE (B): UNDERREACHES



Simultaneous Phase-Ground Faults



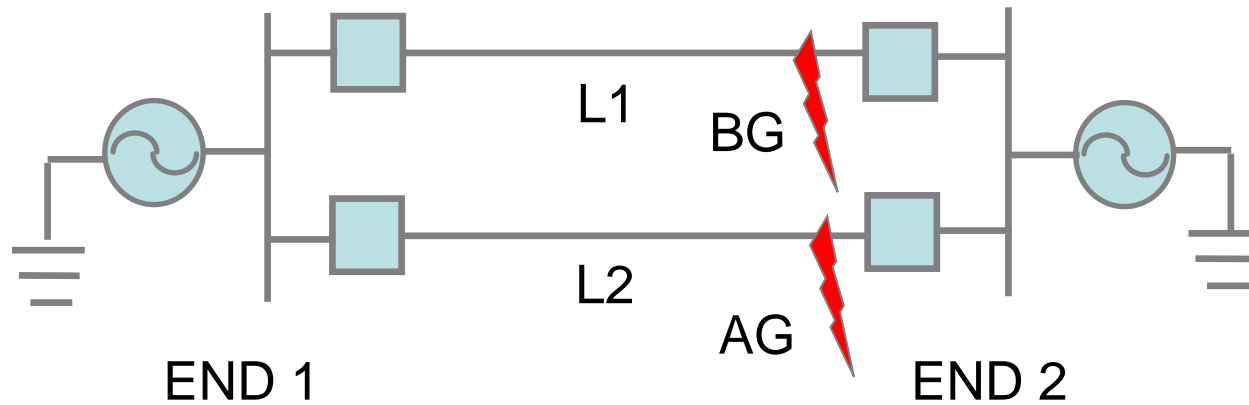
AG DOES NOT OVERREACH

BG DOES NOT UNDERREACH

- I2 polarization is not reliable
- Pure fault phase current polarization must be used

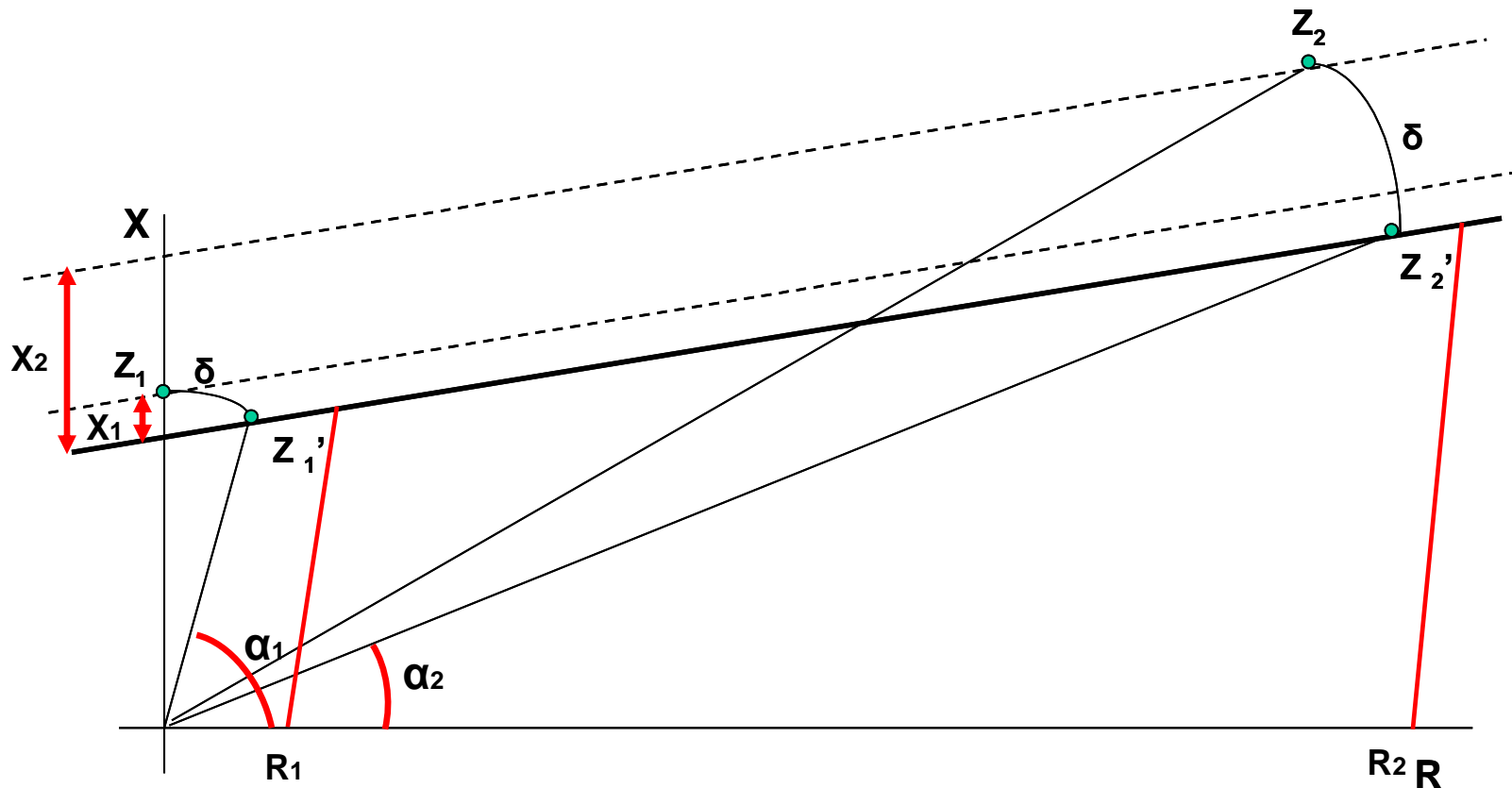
Phase Selector Indicating Single-Phase-Ground Fault During Two-Phase-Ground Fault

- Evolving Fault from Single-Phase-Ground: detection based on a phase selector using the angle between I_2 and I_{1pf}
- Cross-Country Fault

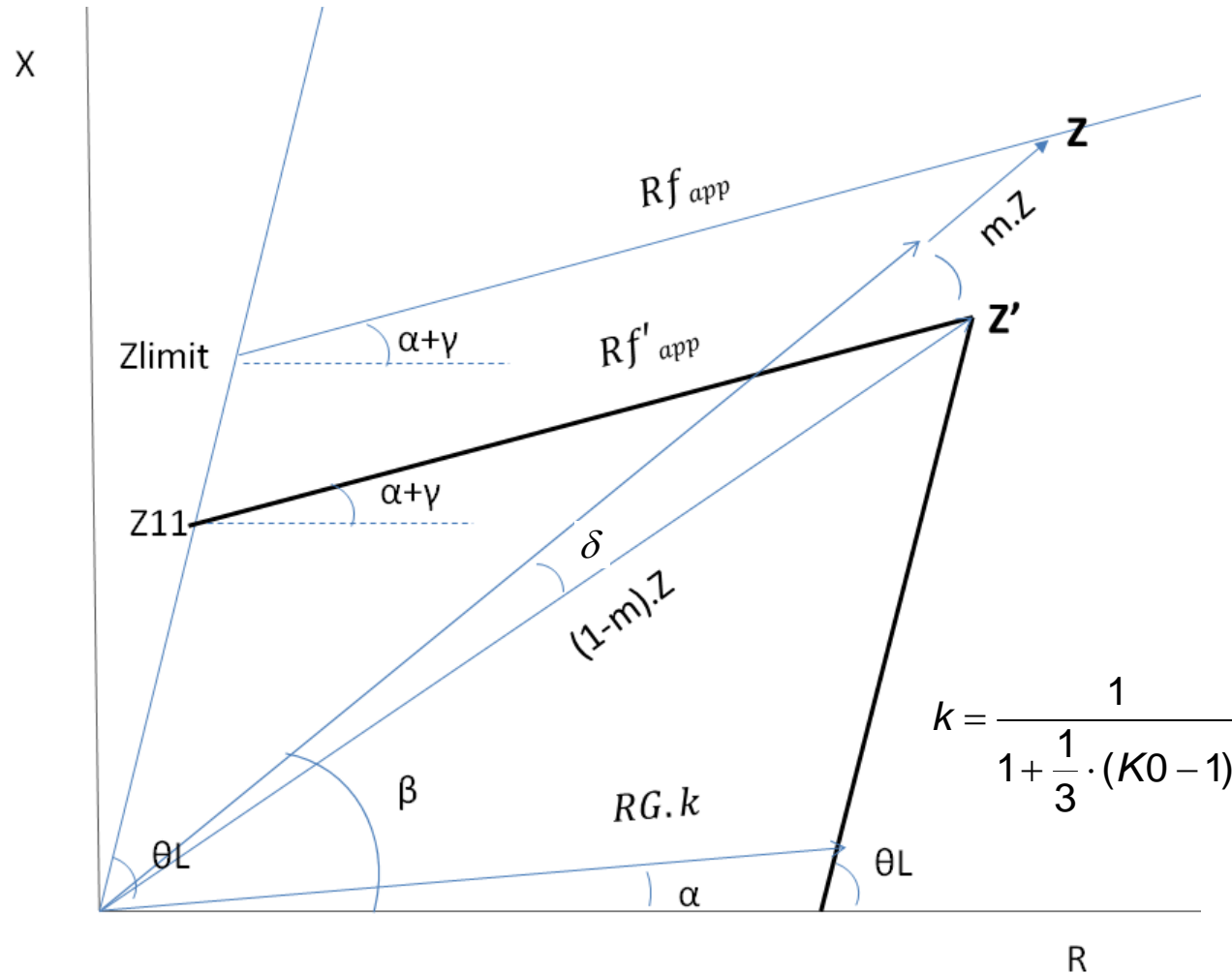


Resistive Reach Calculation

- The higher the resistive reach the lower the impedance angle \rightarrow the higher the overreach with the same angle error (δ)



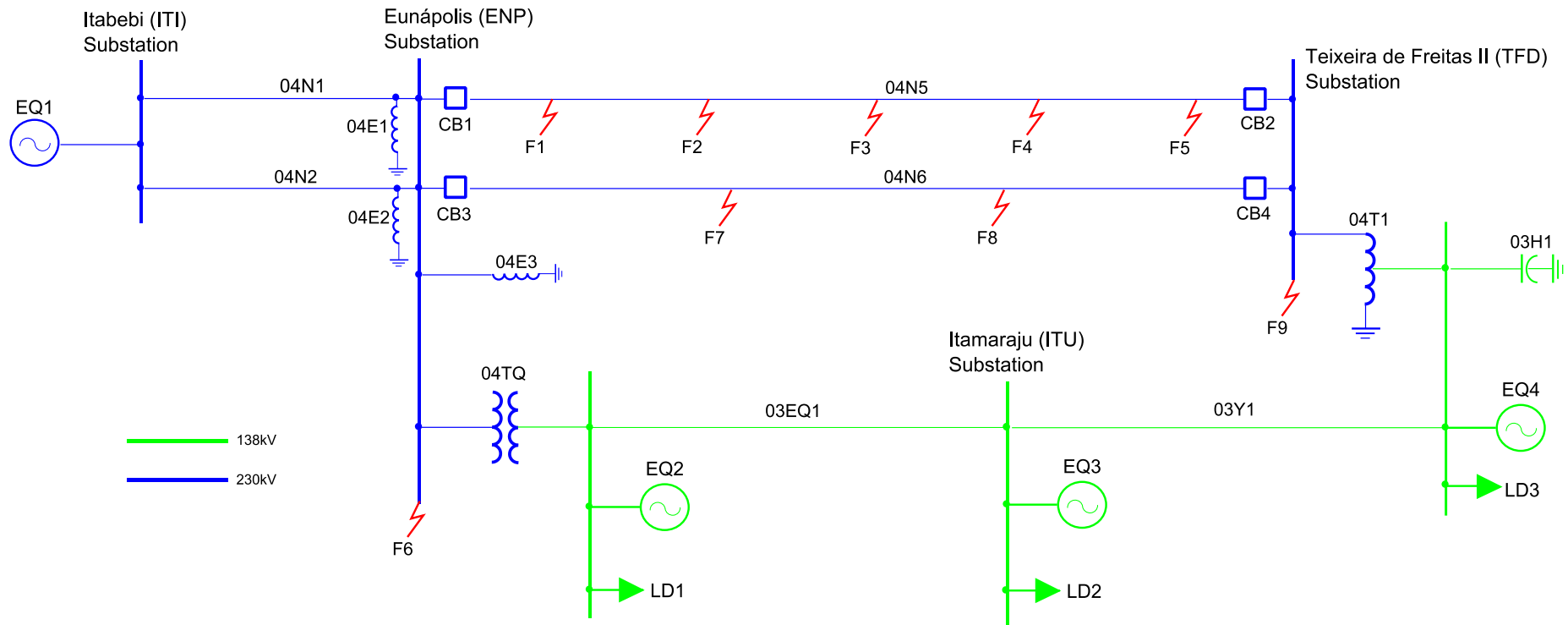
Ground Resistive Reach Calculation



$$RG = \frac{|Z_{L1}| \cdot [(1 - m) \cdot (Z1_reach + overreach) \cdot \sin(\theta_L - \alpha - \gamma) - Z1_reach \cdot \sin(\theta_L - \alpha - \gamma + \delta)]}{\frac{\sin(\theta_L - \alpha)}{\sin(\theta_L - \alpha - \gamma)} \cdot |k| \cdot \sin(\delta)}$$

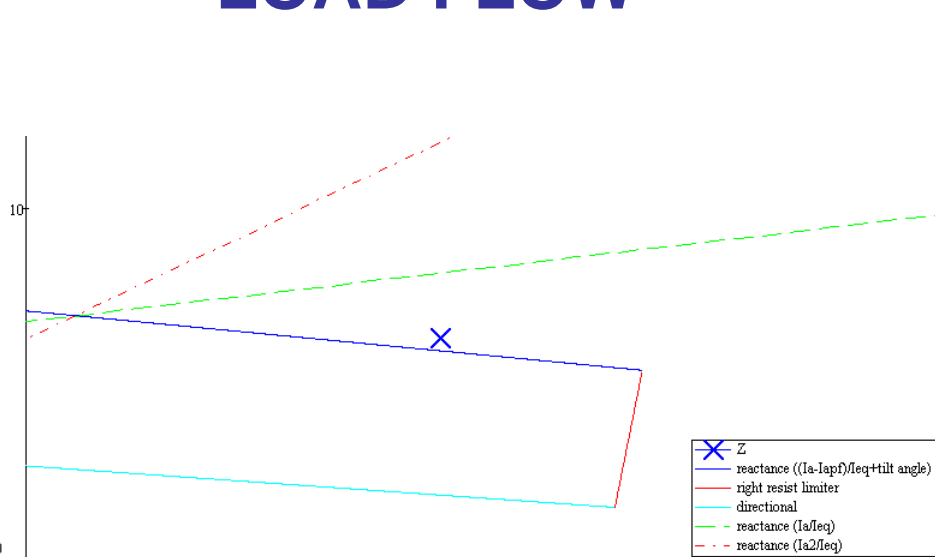
RTDS Simulation

230 kV DOUBLE CIRCUIT LINE

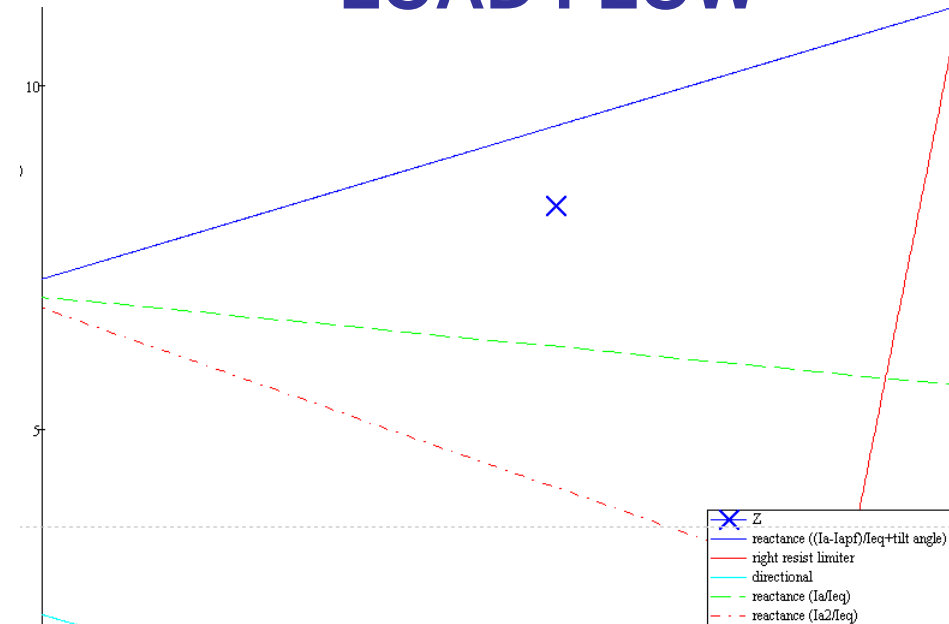


AG Fault with Pole C Open

AT 90% FORWARD
LOAD FLOW



AT 70% REVERSE
LOAD FLOW



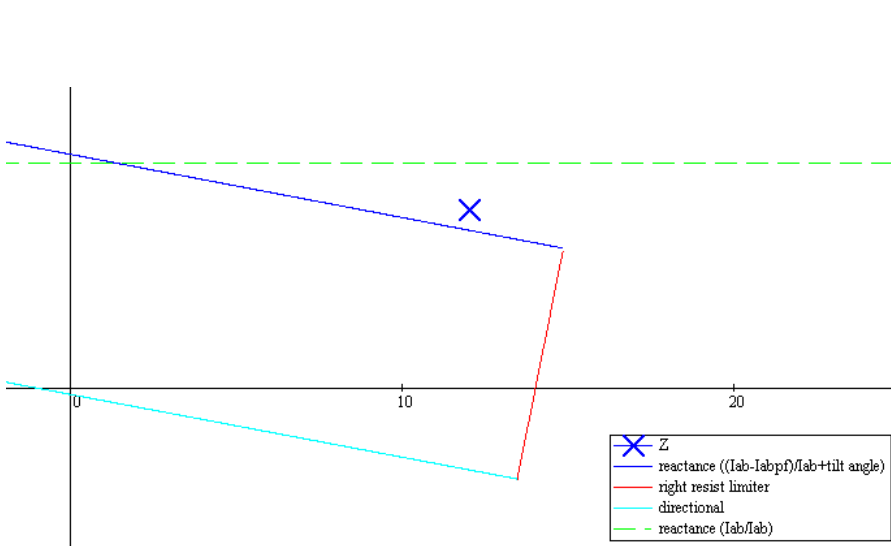
— $(I_a - I_{ap})/I_{eq}$

- - - I_a/I_{eq}

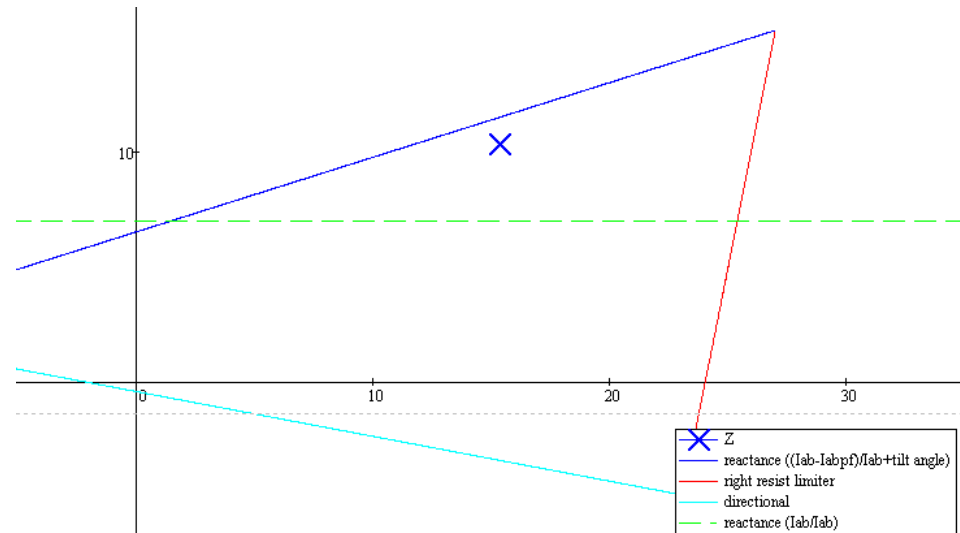
- . - I_{a2}/I_{eq}

Simultaneous Ground Faults (AG BG): AB Unit

AT 90% FORWARD
LOAD FLOW



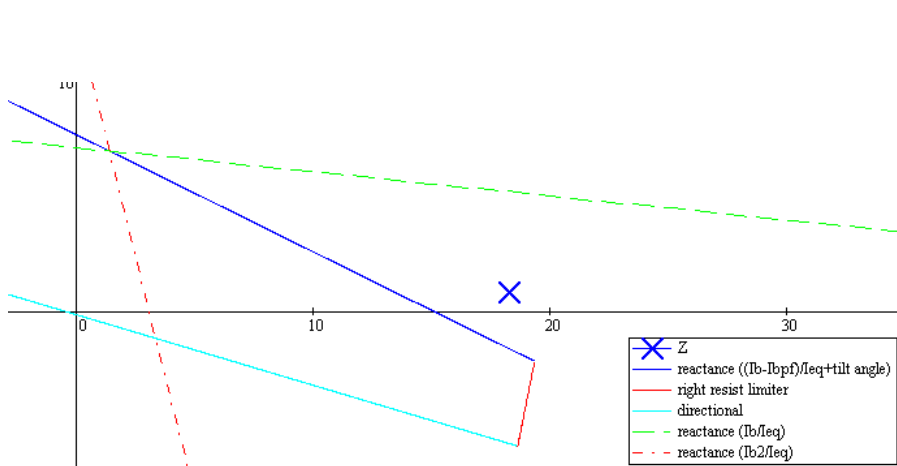
AT 70% REVERSE
LOAD FLOW



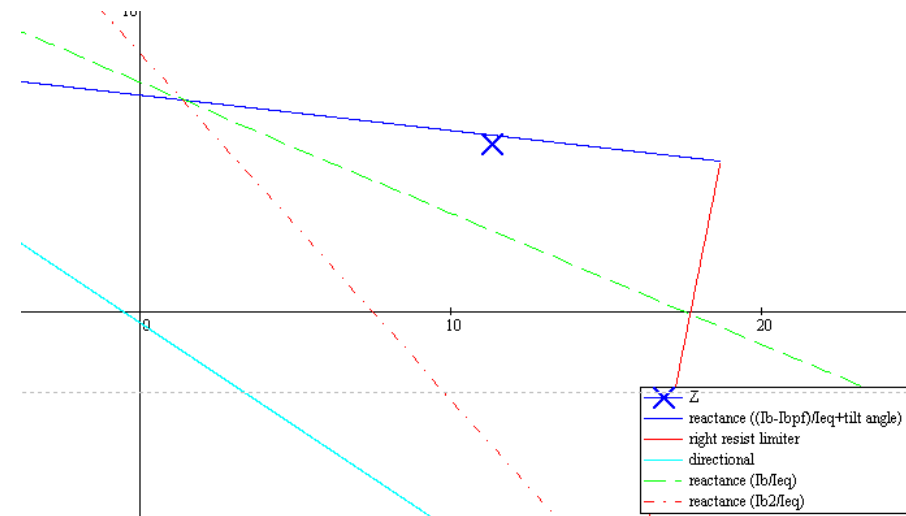
— $(I_{ab} - I_{abp})/I_{ab}$
- - I_{ab}/I_{ab}

Simultaneous Ground Faults (AG BG): BG Unit

AT 90% FORWARD
LOAD FLOW



AT 70% REVERSE
LOAD FLOW



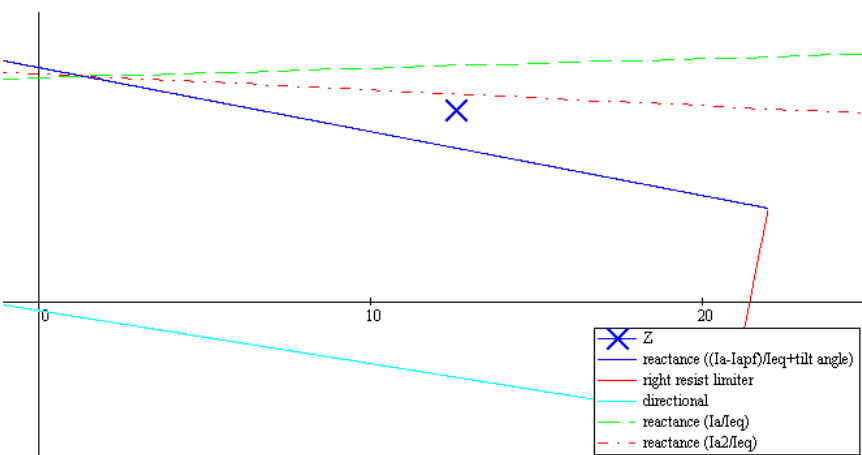
— $(I_a - I_{ap})/I_{aeq}$

- - I_a/I_{aeq}

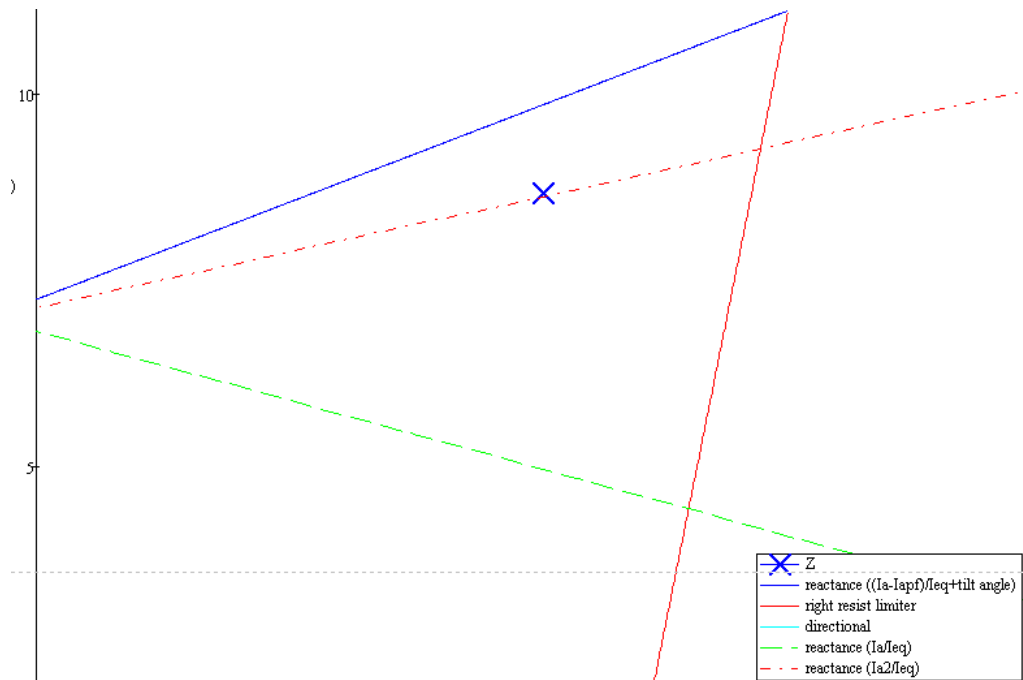
- . - I_a^2/I_{aeq}

Evolving Fault (AG to ABG)

AT 90% FORWARD LOAD FLOW



AT 70% REVERSE LOAD FLOW

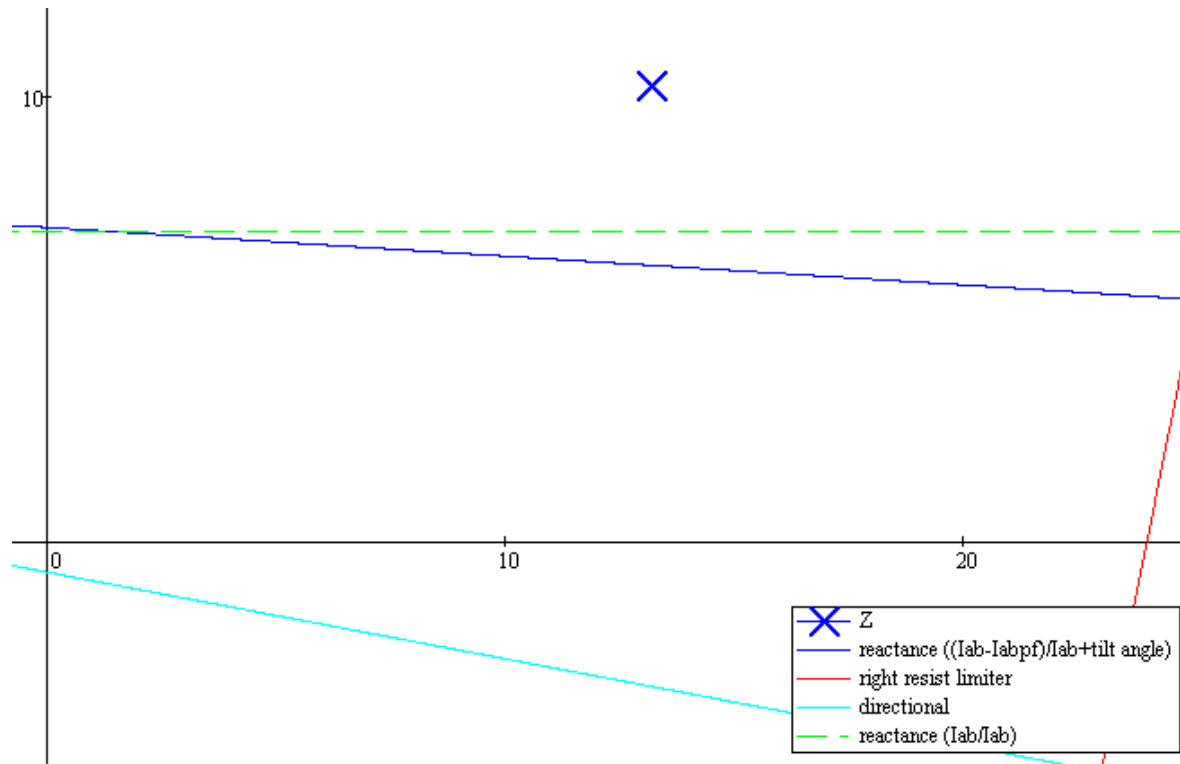


— $(I_a - I_{ap})/I_{eq}$

- - I_a/I_{eq}

- . - I_{a2}/I_{eq}

Cross-Country Fault (Double Circuit): ABG Fault at 70%

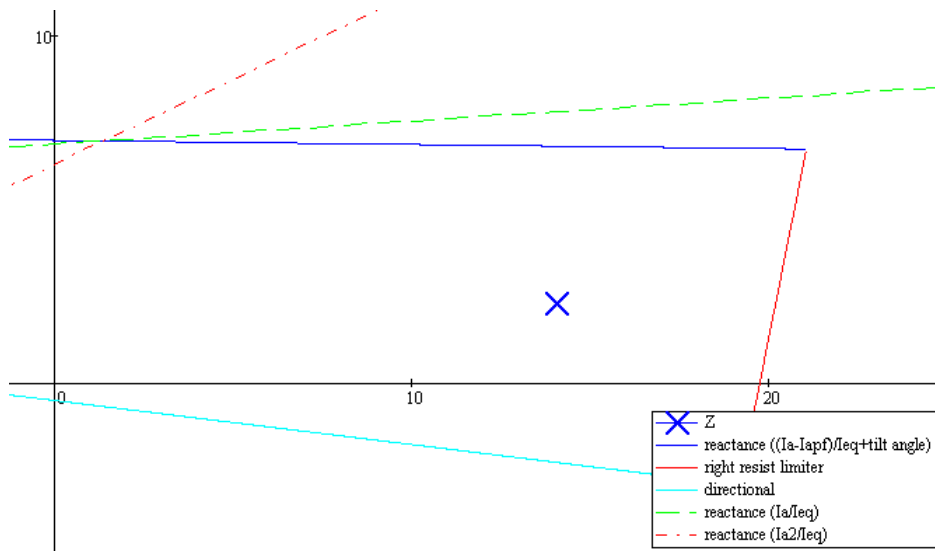


— $(I_{ab}-I_{abp})/I_{ab}$

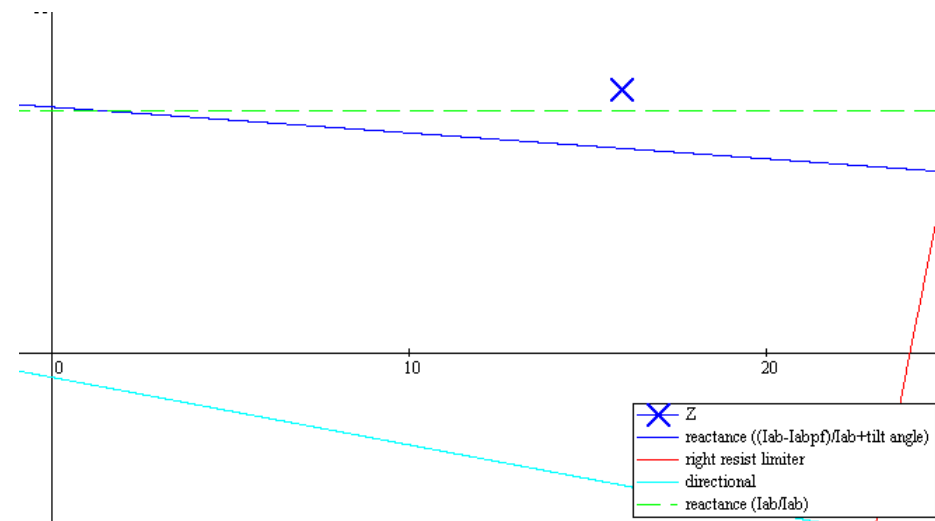
- - - I_{ab}/I_{ab}

Cross-Country Fault (Double Circuit): ABG Fault at 70%

AG FAULT ON PROTECTED LINE



BG FAULT ON PROTECTED LINE



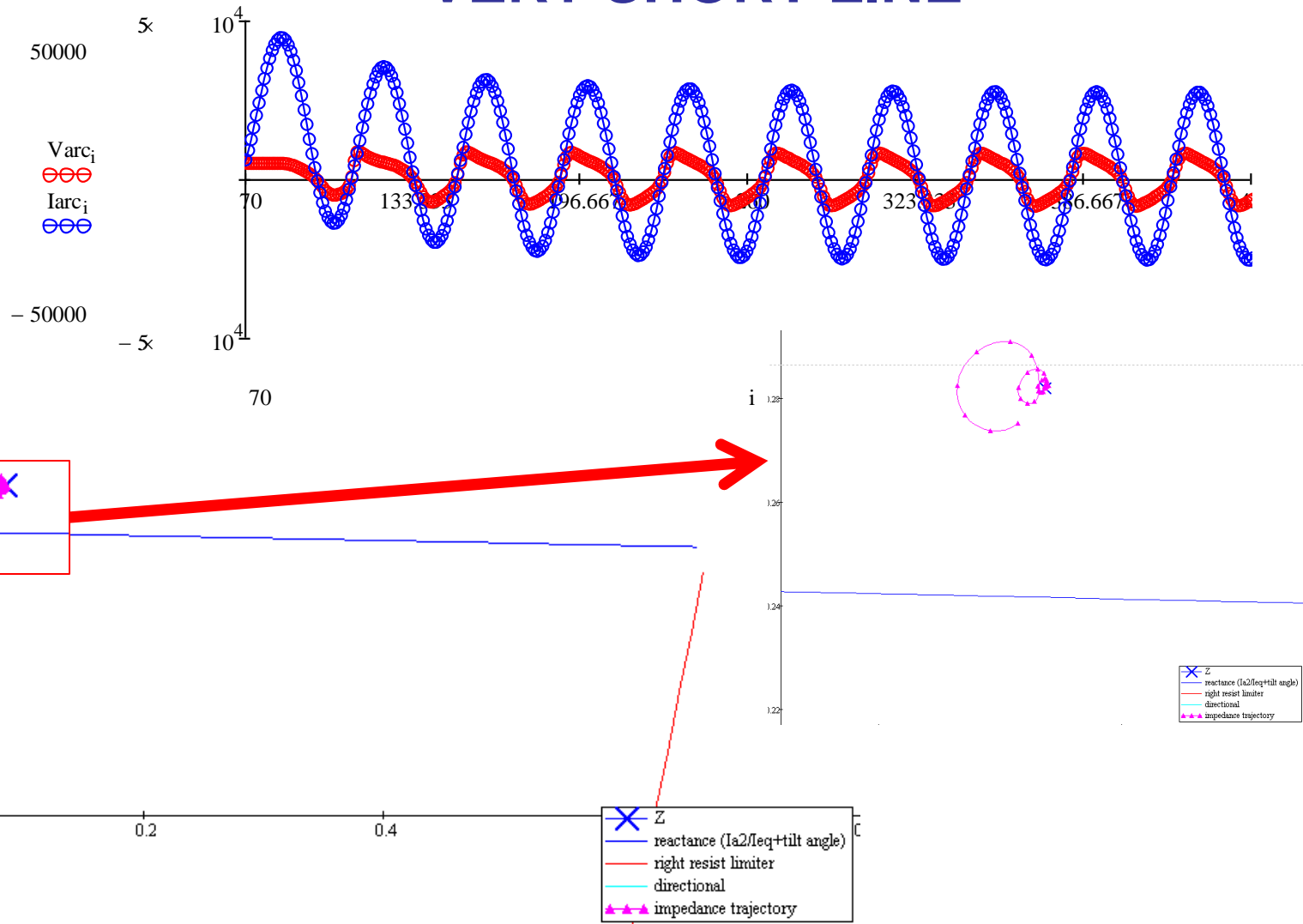
— $(I_a - I_{ap})/I_{eq}$

— I_a/I_{eq}

- - I_{a2}/I_{eq}

Fault with Arc Resistance at 90%

VERY SHORT LINE



Conclusions

- The Mho characteristic tends to underreach during resistive faults although its advanced polarization makes it expand and it automatically compensates the load flow effect
- The quadrilateral characteristic has a good resistive coverage, however the reactance line has to be adequately polarized in order to compensate the load flow and the system non-homogeneity
- The polarization phasors chosen are:
 - Ground units:
 - Negative-sequence current during normal single-phase-ground faults
 - Pure fault phase current during open-pole and phase-phase-ground faults
 - Phase units: pure fault phase-phase current

Conclusions

- The use of the ground units during simultaneous ground faults can complement the operation of the phase units, increasing the sensibility
- The system non-homogeneity can be compensated with a tilt angle
- The influence of the arc voltage on distance relays can be considered negligible
- It is important to limit the resistive reach as a function of the reactive reach

Thank you

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