

# Three Terminal Line Application of Distance and Differential Relays in the Entergy System



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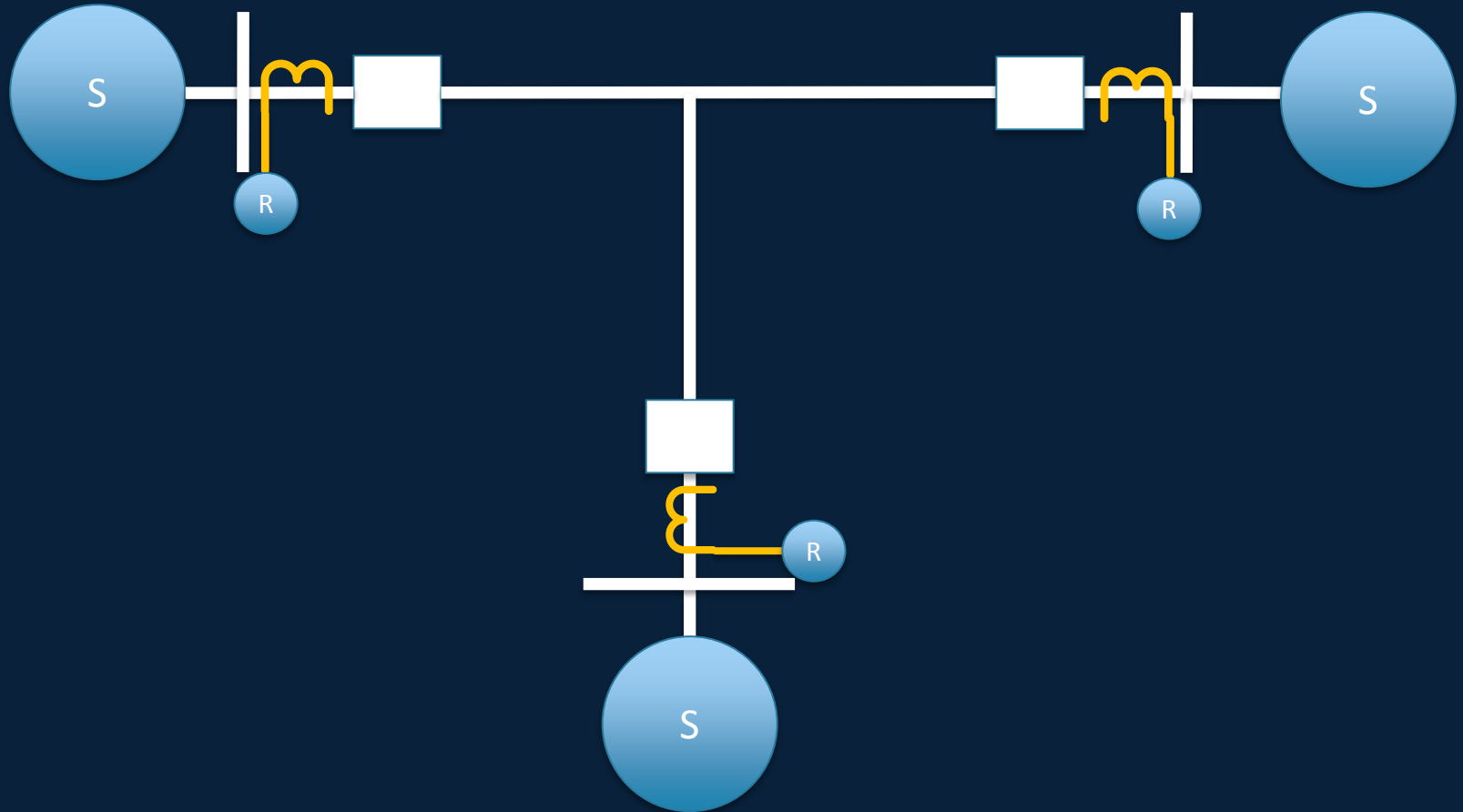
**Tu Nguyen, Entergy Transmission**

**Joe Perez, P.E. SynchroGrid Labs**

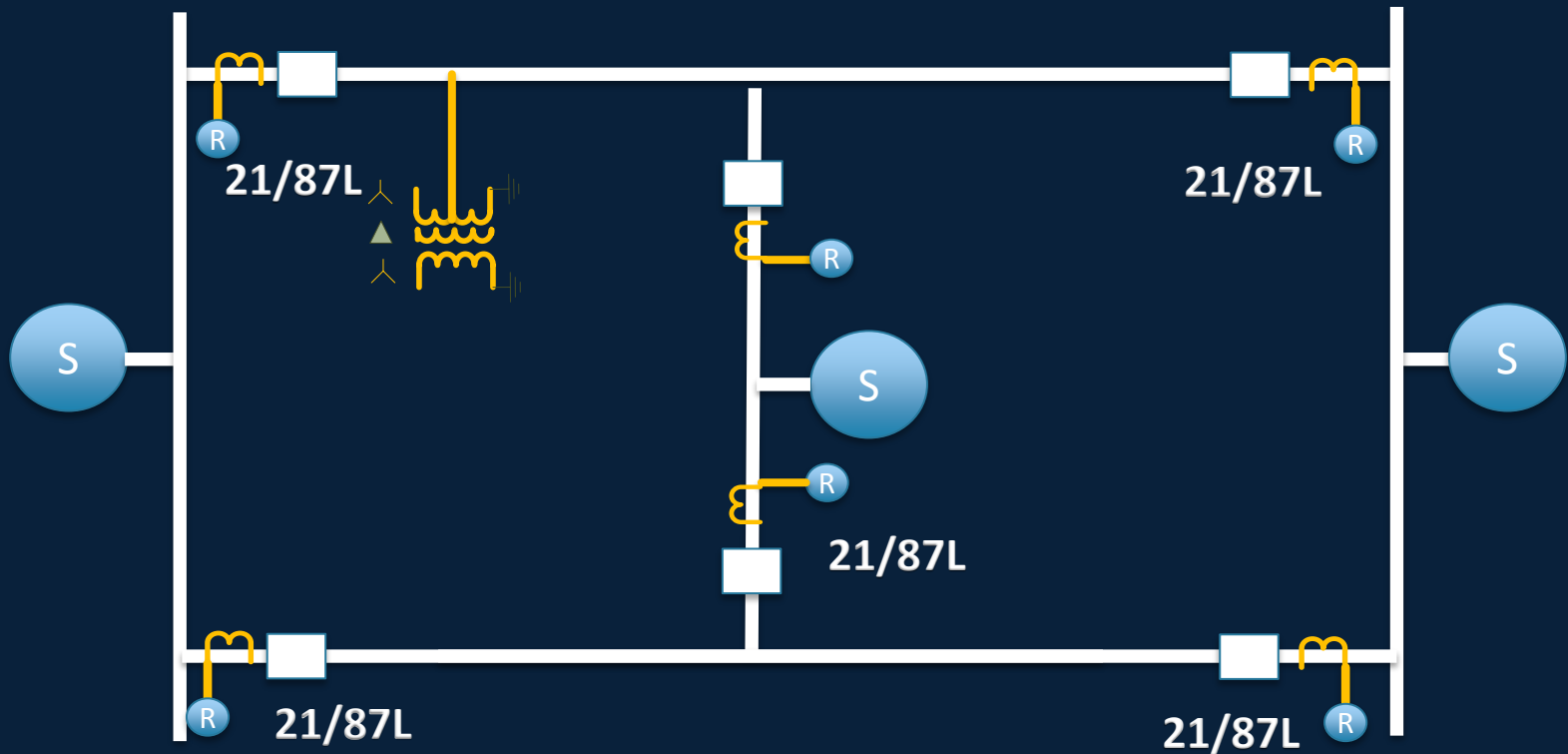
# Outline

- Definition of Terminals
- Project Background
- Three Terminal Line Protection Schemes
- Apparent Impedance
- Distance Relay Settings
- Communications
  - DUTT
  - POTT

# Types of Lines



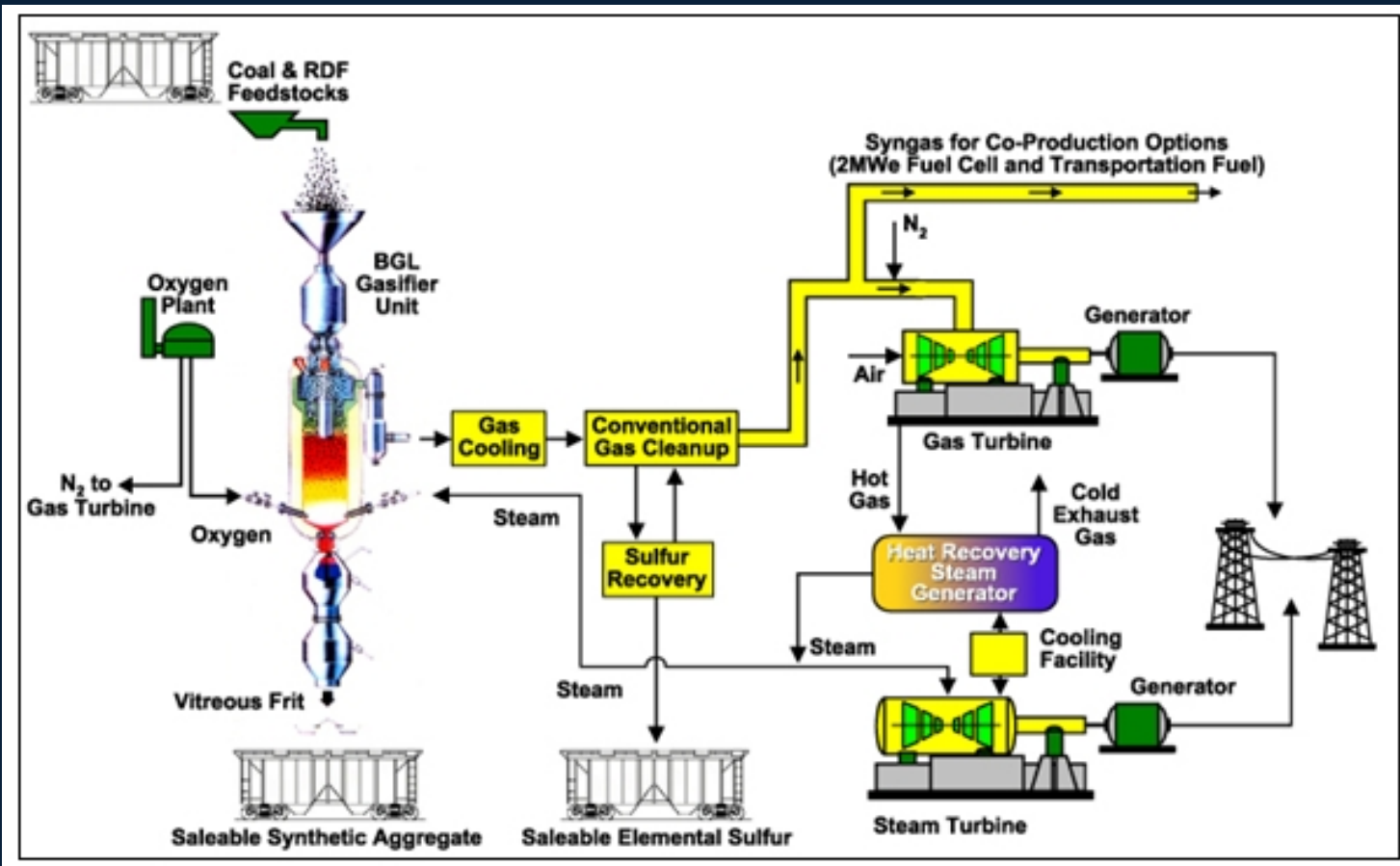
# Complex Three Terminal Lines



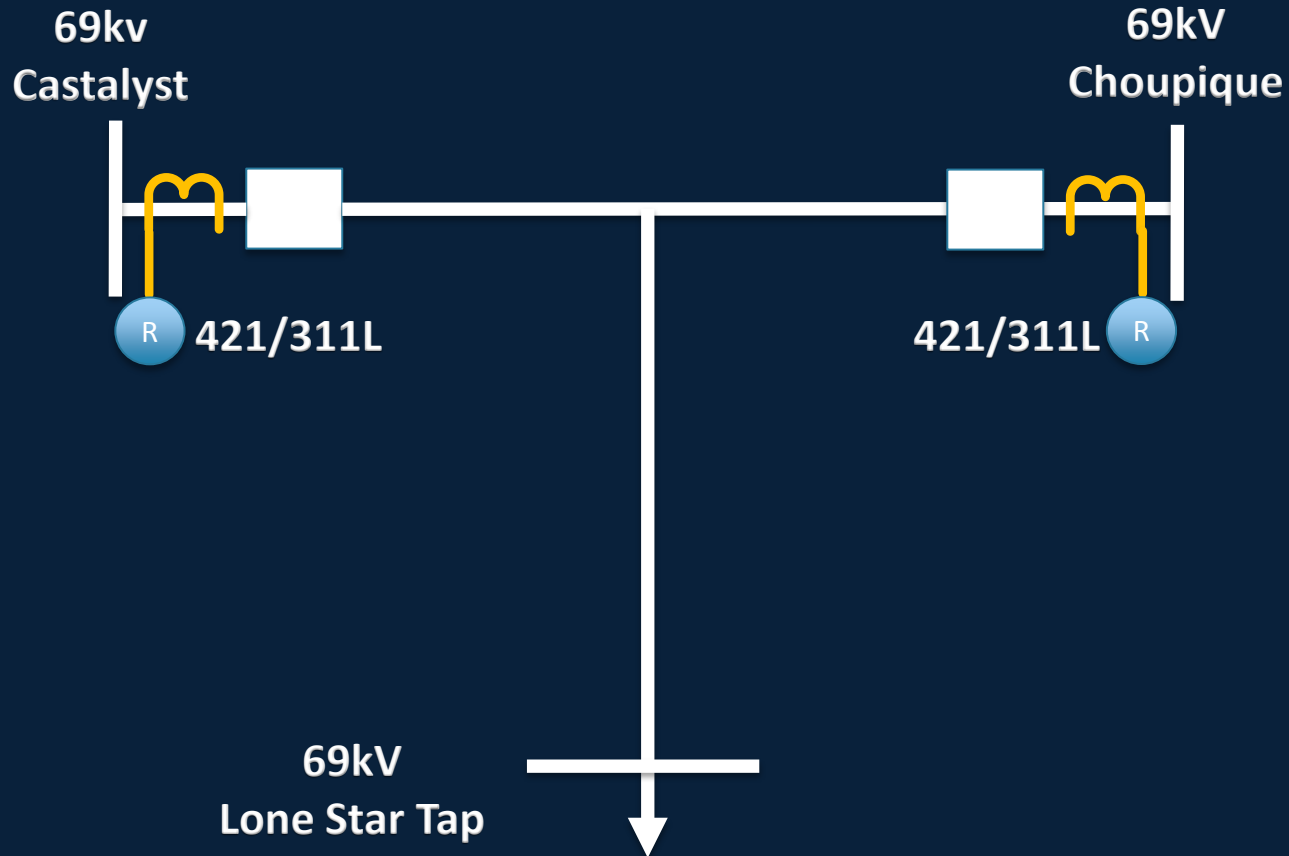
# Project Background

- Customer requested interconnection agreement for new generator.
- Customer's facility operates two high temperature rotary kilns to process petroleum coke.
- Exhausts of the rotary kilns are combined and exit to atmosphere through a refractory lined stack at temperatures ranging from 1800°F to 2100°F.
- Proposed project would capture lost energy and co-generate electricity for use at the facility and for sale to Entergy.
- A condensing steam-driven turbine generator would produce 36.4 MW of electricity.

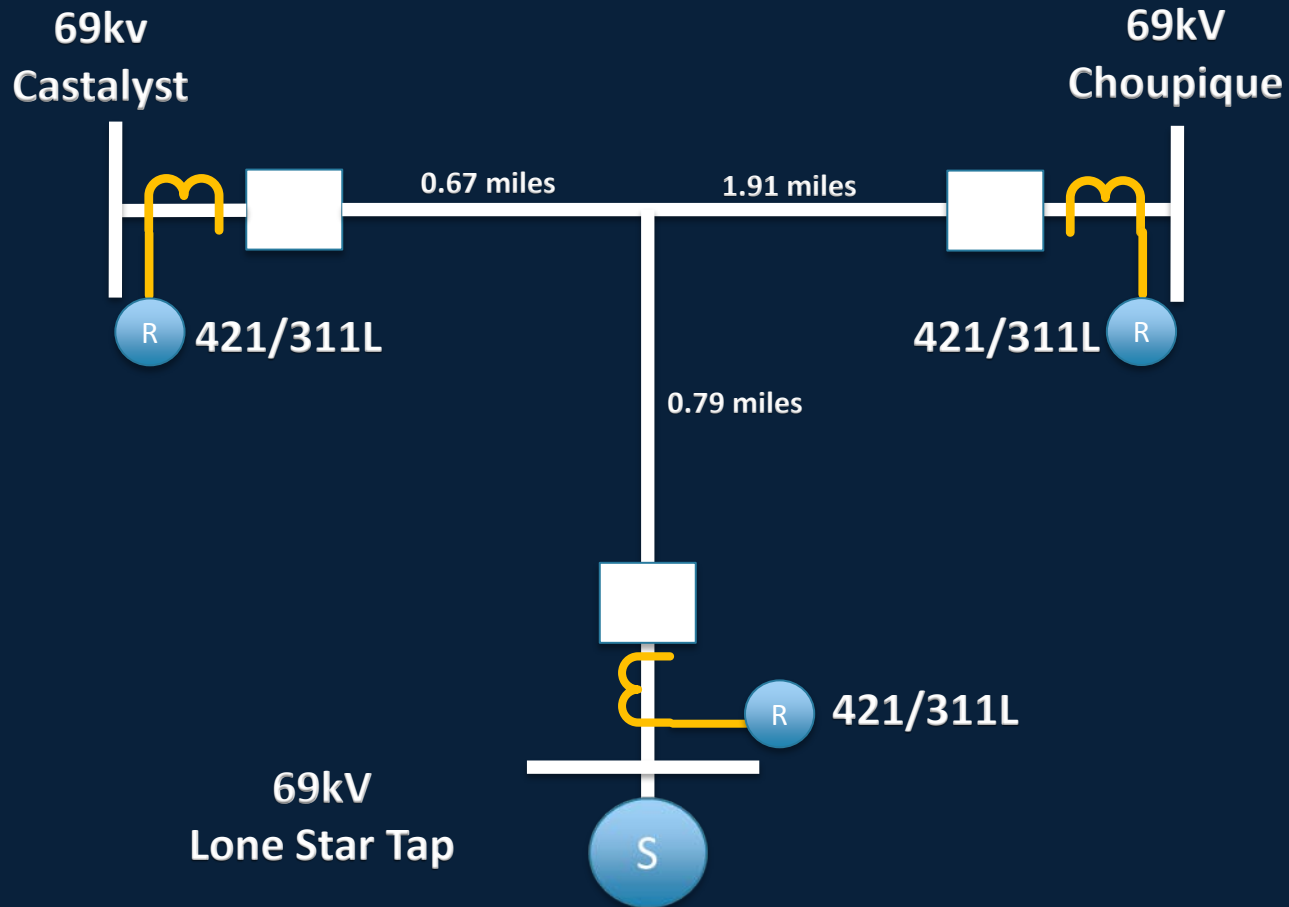
# Chemical Process



# Entergy Application



# Entergy Application





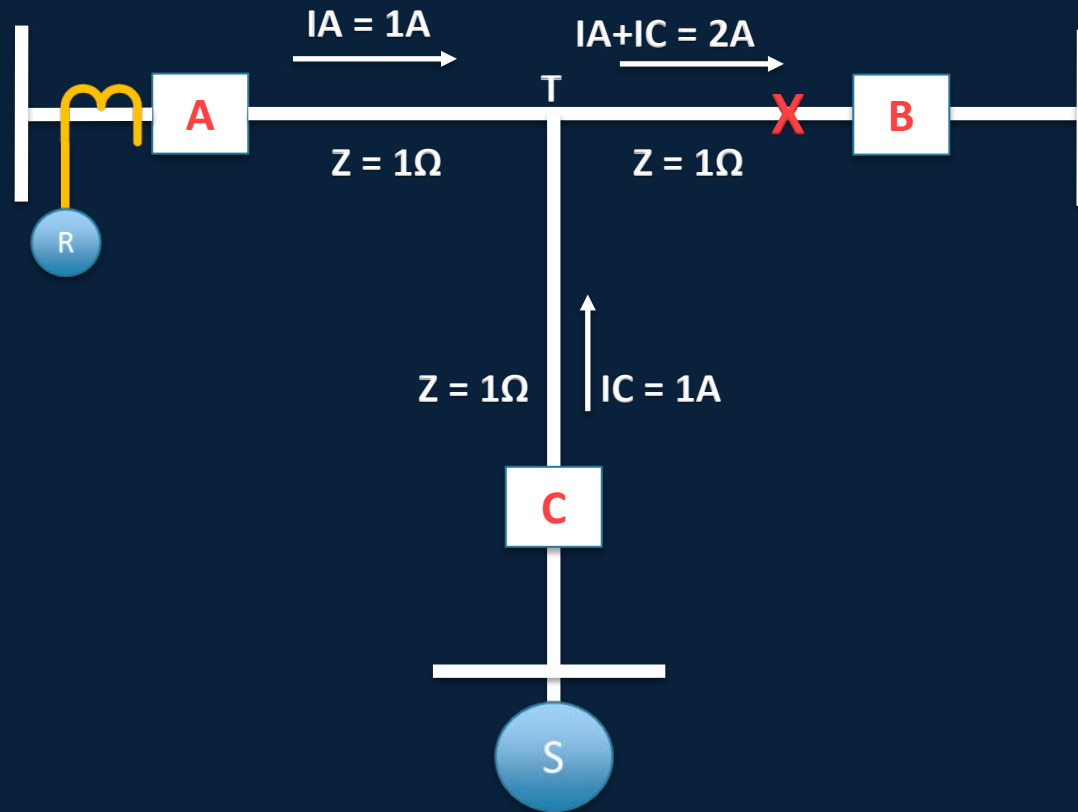
# Protection of Three Terminal Lines

- Not as simple as two terminal lines
- Infinite variety of
  - Tap locations
  - Line impedances
  - Source impedances
  - System loading
  - System operations
- Infeeds
- Outfeeds

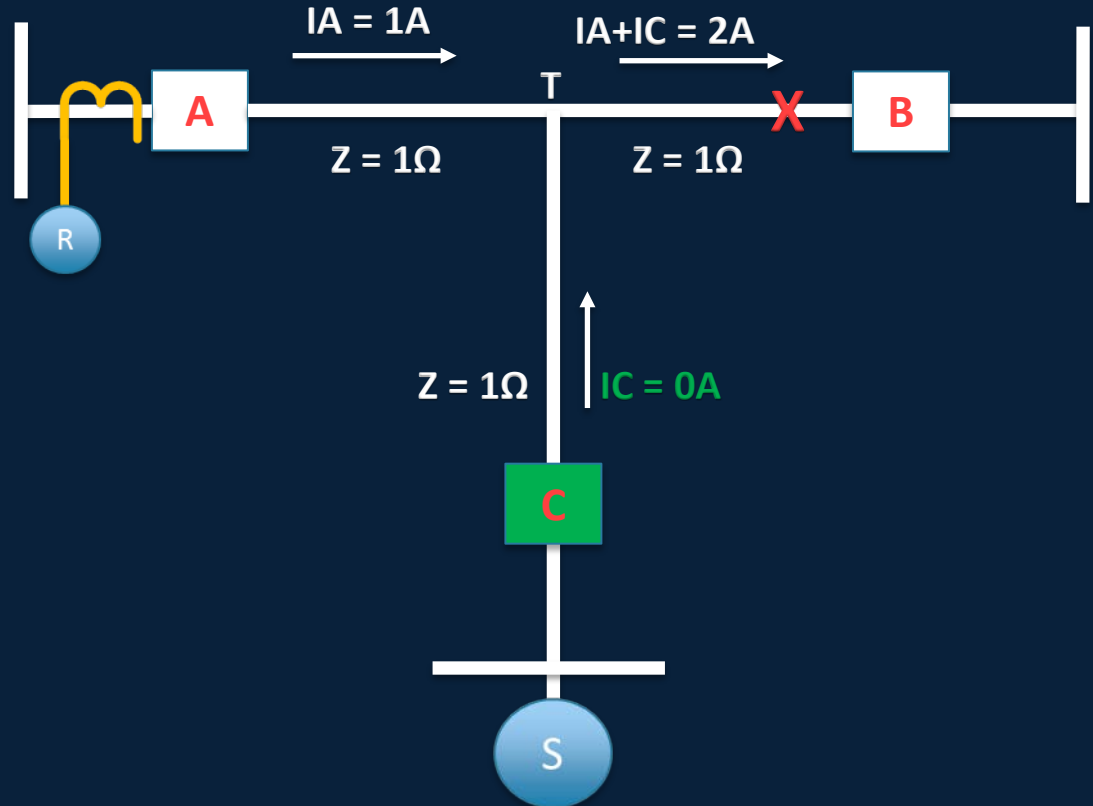
# Apparent Impedance

- Impedance seen by relay does not equal line impedance from the relay terminal to fault.
- Relay measures voltage drop between relay location and fault.
- Impedance seen by relay depends on contributions or infeed from other terminals.
- Let's review the infeed problem.

# Apparent Impedance and Infeed



# Apparent Impedance and Infeed

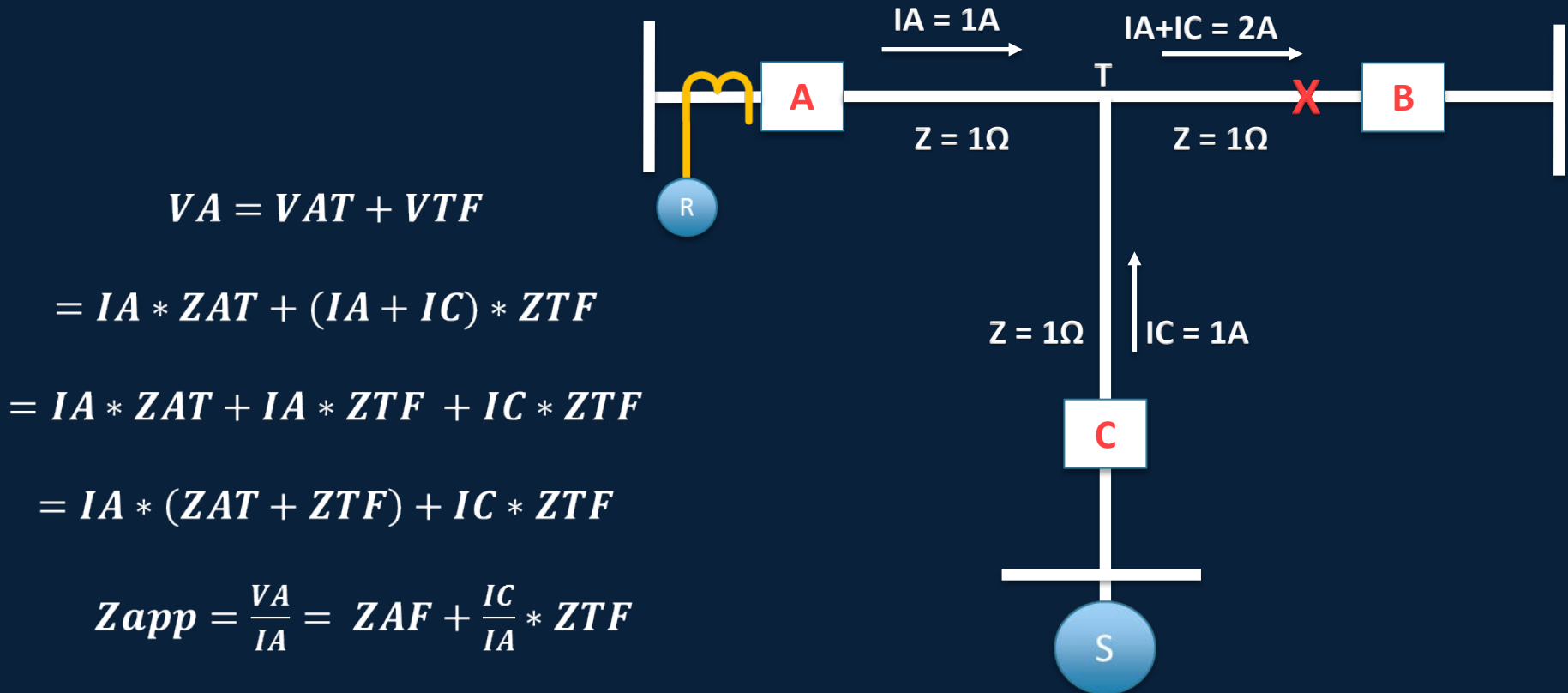


$$\begin{aligned} V_A &= V_{AT} + V_{TF} \\ &= I_A * Z_{AT} + I_A * Z_{TF} \\ &= I_A(Z_{AT} + Z_{TF}) \\ &= I_A * Z_{AF} \end{aligned}$$

The true impedance is:

$$Z_{AF} = \frac{V_A}{I_A} = 2\Omega$$

# Apparent Impedance and Infeed



$$V_A = V_{AT} + V_{TF}$$

$$= I_A * Z_{AT} + (I_A + I_C) * Z_{TF}$$

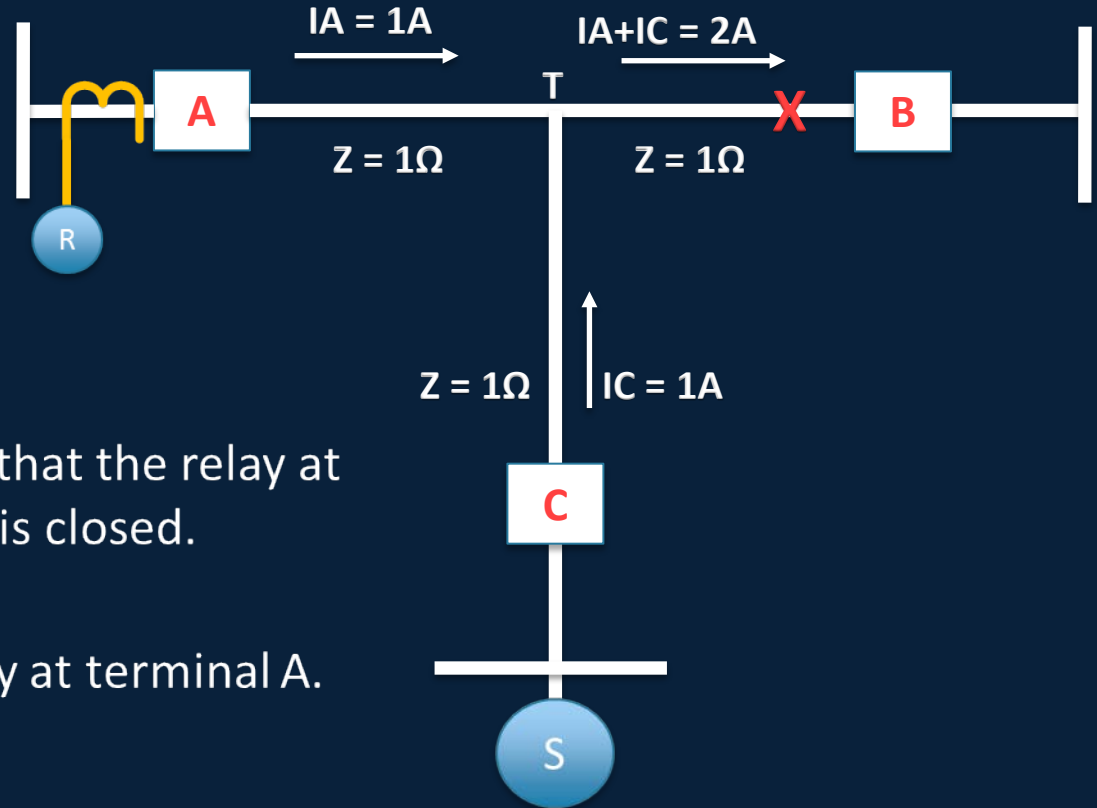
$$= I_A * Z_{AT} + I_A * Z_{TF} + I_C * Z_{TF}$$

$$= I_A * (Z_{AT} + Z_{TF}) + I_C * Z_{TF}$$

$$Z_{app} = \frac{V_A}{I_A} = Z_{AF} + \frac{I_C}{I_A} * Z_{TF}$$

$$Z_{app} = 2\Omega + \frac{1A}{1A} * 1\Omega = 3\Omega$$

# Apparent Impedance and Infeed



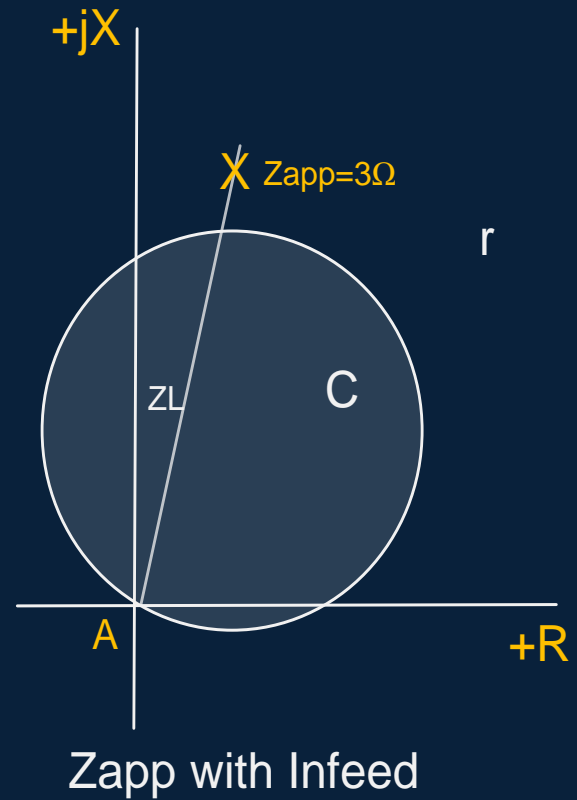
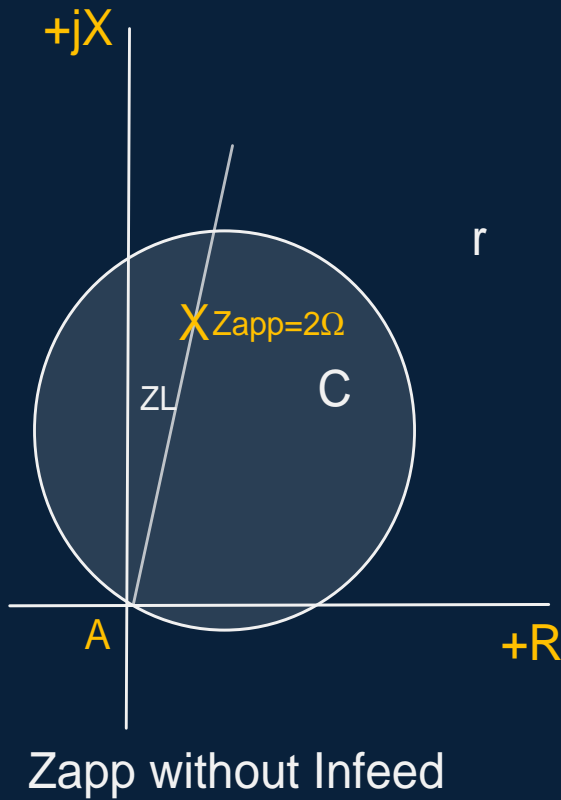
$$Z_{app} = \frac{VA}{IA} = Z_{AF} + \frac{IC}{IA} * Z_{TF}$$

$Z_{app}$  is the apparent impedance that the relay at terminal A sees when terminal C is closed.

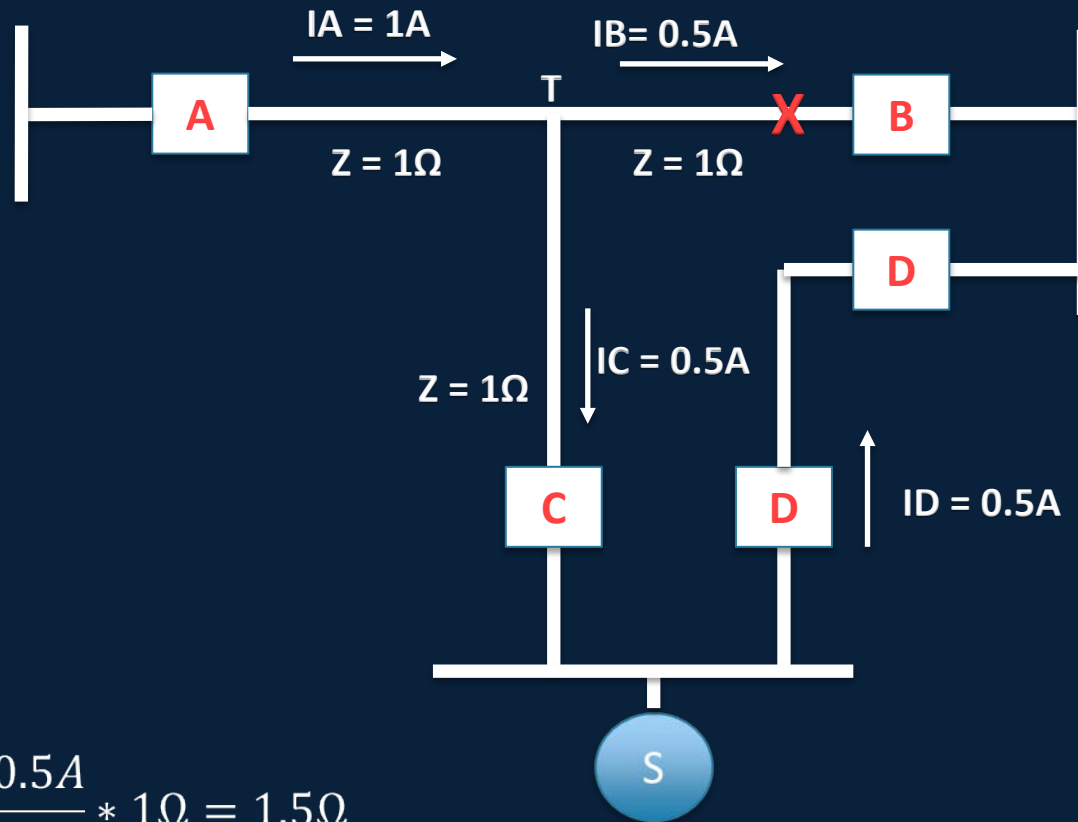
$\frac{IC}{IA}$  is the infeed factor for the relay at terminal A.

$\frac{IC}{IA} * Z_{TF}$  is the error factor as a result of the infeed.

# Apparent Impedance and Infeed



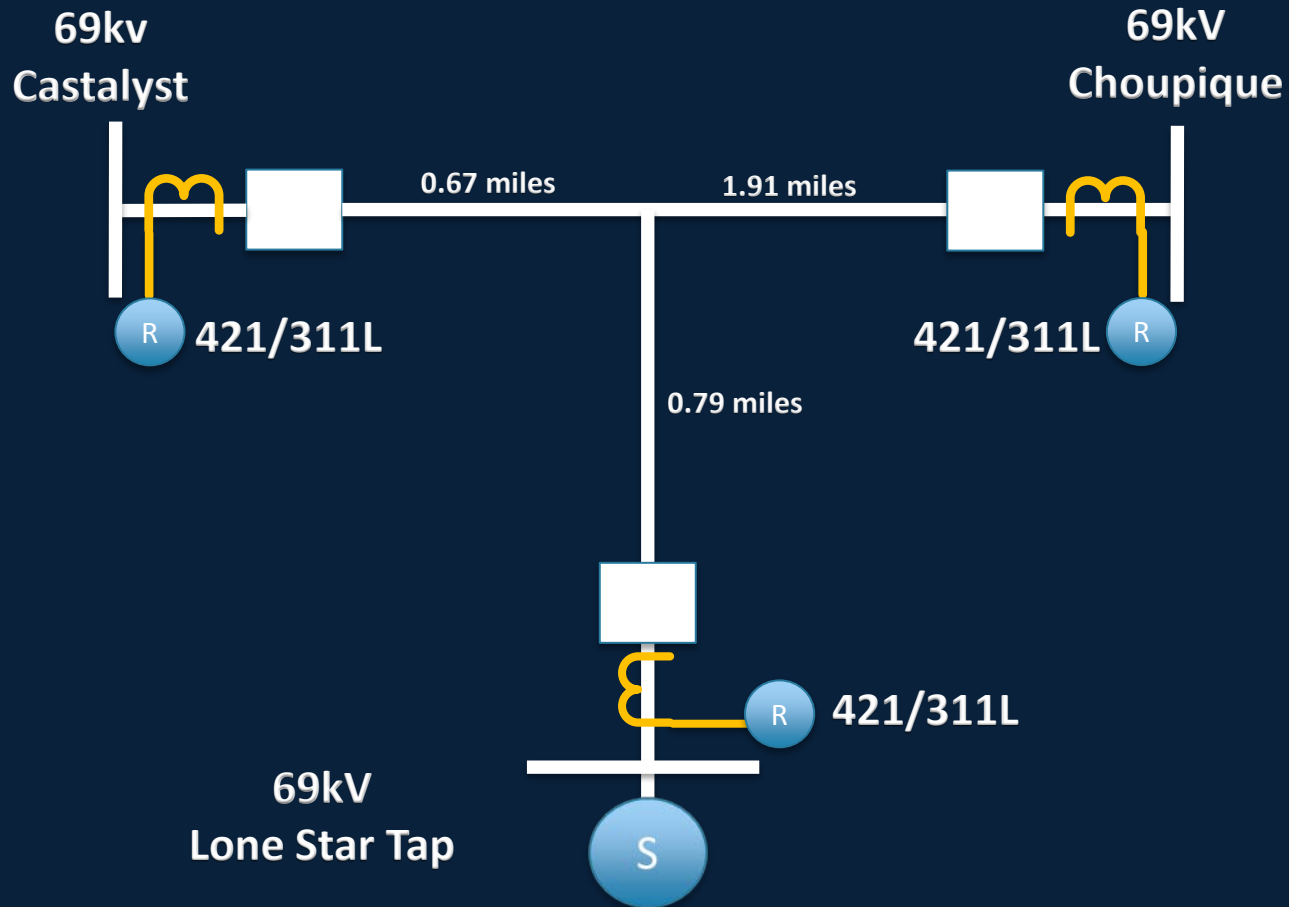
# Apparent Impedance and Outfeed



$$Z_{app} = 2\Omega - \frac{0.5A}{1A} * 1\Omega = 1.5\Omega$$



# 421-Relay Settings

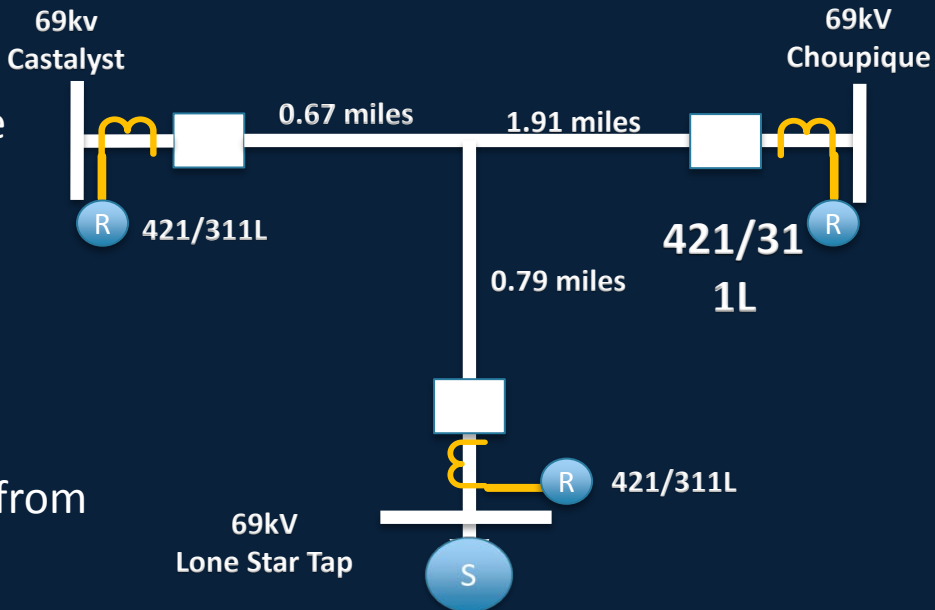


# 421-Directional Settings

Station R = Catalyst  
Station S = Choupique  
Station T = Lone Star

$$Z2F = 0.5 * \left( ZRTap + \frac{ZSTap * ZTTap}{ZSTap + ZTTap} \right)$$

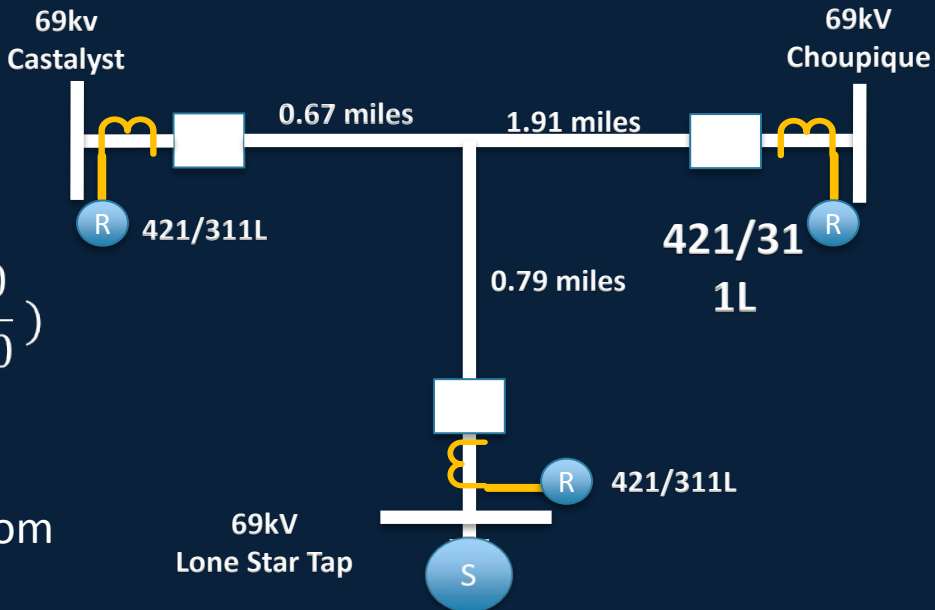
- ZRTap is the positive sequence impedance from station R to the Tap point.
- ZSTap is the positive sequence impedance from station S to the Tap point.
- ZTTap is the positive sequence impedance from station T to the Tap point.



# 421- Directional Settings

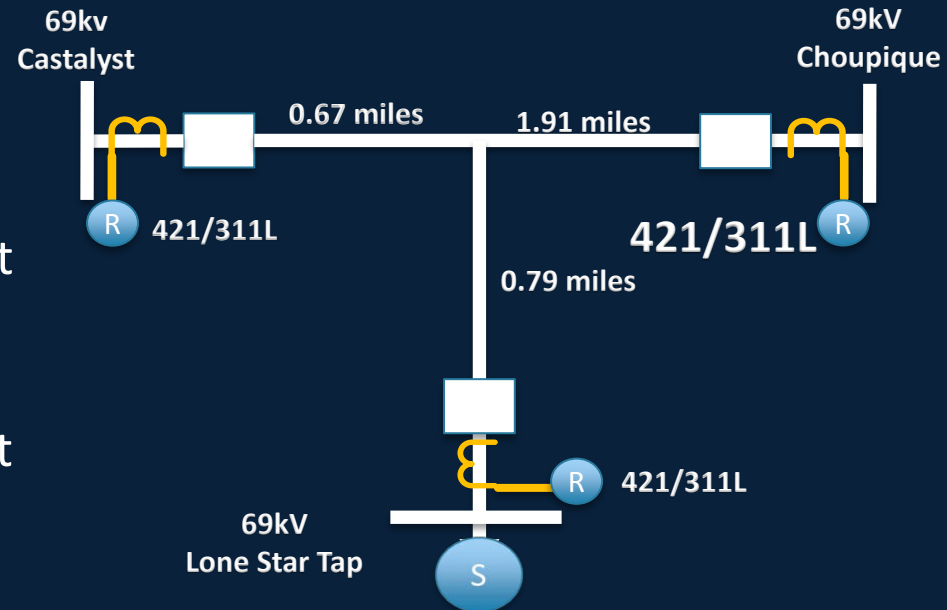
$$Z0F = 0.5 * (ZRTap0 + \frac{ZSTap0 * ZTTap0}{ZSTap0 + ZTTap0})$$

- ZRTap0 is the zero sequence impedance from station R to the Tap point.
- ZSTap0 is the zero sequence impedance from station S to the Tap point.
- ZTTap0 is the zero sequence impedance from station T to the Tap point.



# 421-Zone 1 Settings

- Zone 1 settings should be selected based on the shortest line to the next terminal.
- Zone 1 settings need to be set so that they do not overreach any of the remote terminals.
- Zone 1 settings should be 80% of the line.
- All Zone 1 elements work under a DUTT.



# 421-Zone 1 Settings

## Lone Star- Zone 1 Settings:

Lone Star-Choupique							
Line Length	=	2.70	mile	0.06313	+J	0.15293	(Pos)
				(Longest 2nd line)			
0.01410	+J	0.04011	(Pos)	Choup-Intracostal			
				(from infeed sheet)			
				0.13778	+J	0.49056	(Zero)
0.03395	+J	0.13064	(Zero)	0.00652	+J	0.03750	(Pos)
Lone Star-Catalyst				(Shortest 2nd line)			
Line Length	=	1.46	mile	Catalyst-Carlyss			
				(Zone 2 Bus)			
0.00938	+J	0.02198	(Pos)	0.02289	+J	0.10151	(Zero)
0.02015	+J	0.07111	(Zero)				

# 421-Zone 1 Settings

## Catalyst-Zone 1 Settings:

Catalyst-Choupique							
Line Length	=	2.58	mile	0.06313	+J	0.15293	(Pos)
				(Longest 2nd line)			
0.01334	+J	0.03829	(Pos)	Choup-Intracostal			
				(from infeed sheet)			
				0.13778	+J	0.49056	(Zero)
0.03230	+J	0.12479	(Zero)	0.00976	+J	0.05560	(Pos)
Catalyst-Lone Star				(Shortest 2nd line)			
Line Length	=	1.46	mile	Choupique-Carlyss			
				(Zone 2 Bus)			
0.00938	+J	0.02198	(Pos)	0.04248	+J	0.17876	(Zero)
0.02015	+J	0.07111	(Zero)				

# 421-Zone 1 Settings

## Choupique-Zone 1 Settings:

### Choupique-Lone Star

Line Length = 2.70 mile

0.00652 +J 0.03750 (Pos)

(Longest 2nd line)

Catalyst-Carlyss

0.01410 +J 0.0401 (Pos)

(from infeed sheet)

0.02289 +J 0.10151 (Zero)

0.03395 +J 0.13064 (Zero)

### Choupique-Catalyst

Line Length = 2.58 mile

0.00652 +J 0.03750 (Pos)

(Shortest 2nd line)

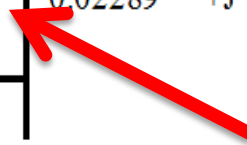
Catalyst-Carlyss

(Zone 2 Bus)

0.01334 +J 0.0382 (Pos)

0.02289 +J 0.10151 (Zero)

0.03230 +J 0.1247 (Zero)



# 421-Zone 2 Settings

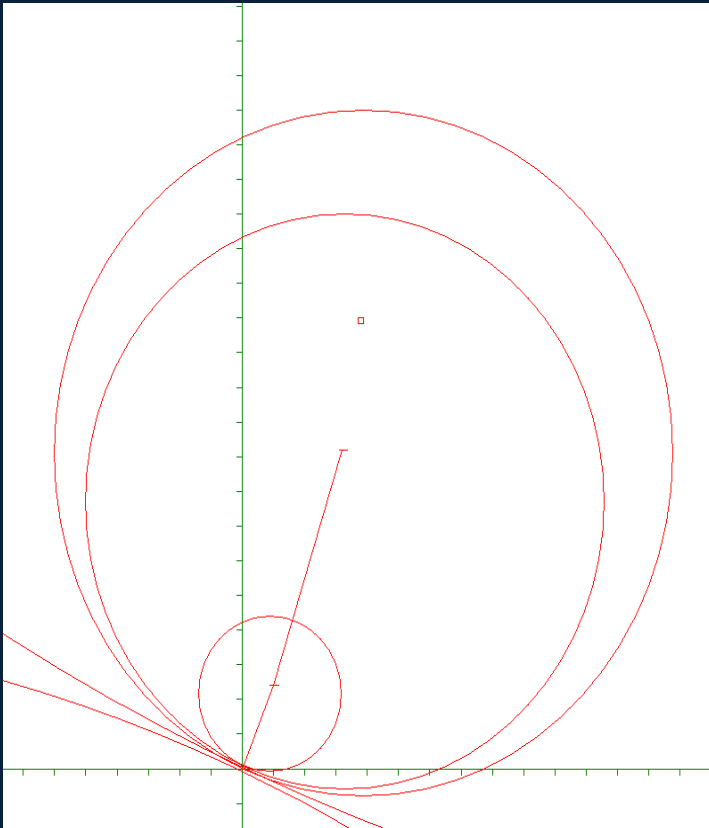
- Zone 2 is set between
  - 120% of the line impedance and
  - 100% of the secondary line impedance plus 50% of the secondary line impedance of the remote shortest line.
- Zone 2 elements must detect all internal faults.
- Zone 2 elements are used for the permissive trip elements with a POTT scheme.
- Zone 2 elements are affected by the infeed currents.
- Zone 2 elements must be verified using the Apparent Impedance through Aspen.



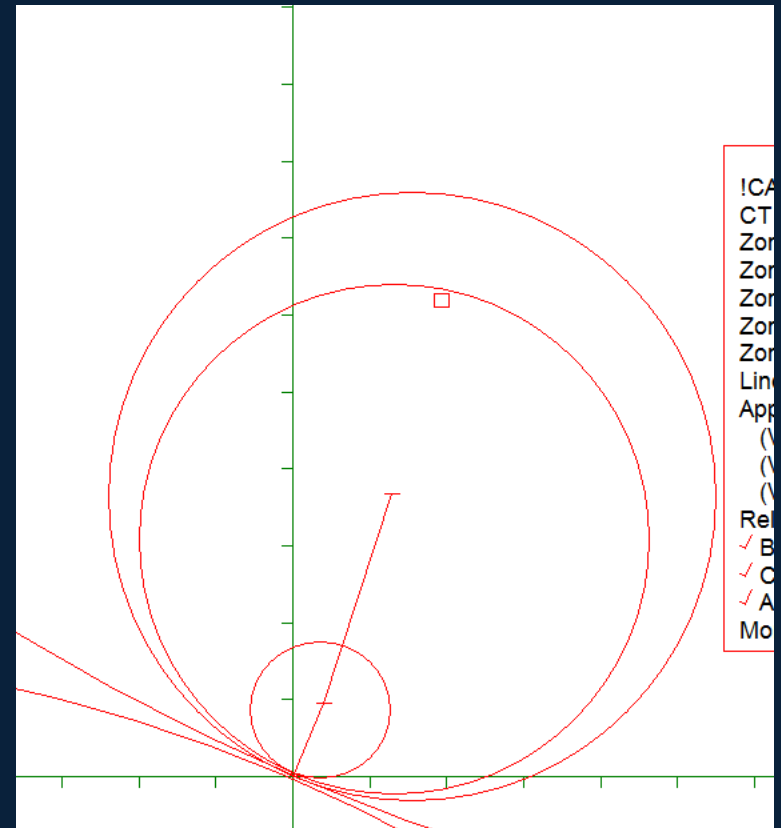
# 421-Zone 2 Settings

Zone 2 Settings Carlyss set at 2.19 ohms from calculation sheet

Apparent Impedance Lone Star  
Open, fault at 124% of the line: 1.77 ohms



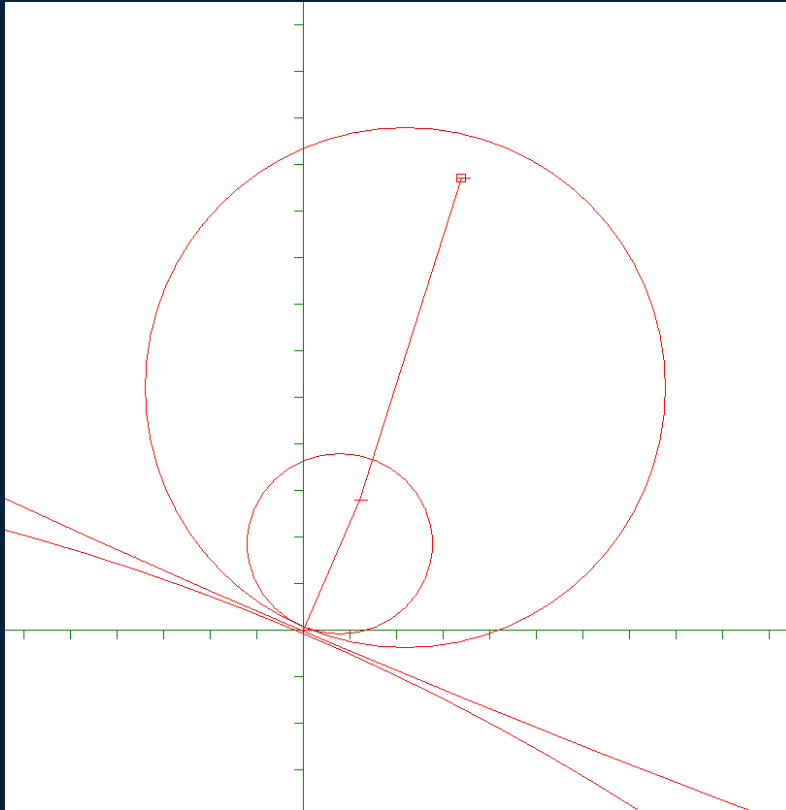
Apparent Impedance Lone Star  
Closed, fault at 124% of the line: 2.14 ohms



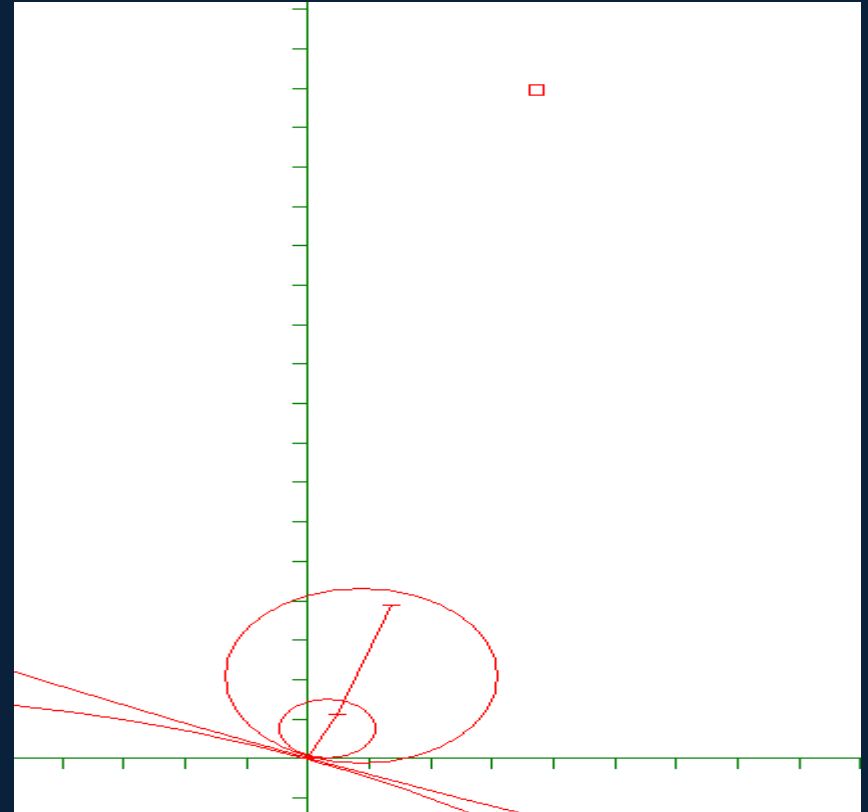
# 421-Zone 2 Settings

Zone 2 Settings Lone Star set at 1.48 ohms from calculation sheet

Apparent Impedance Carlyss Open,  
fault at 100 % of the line: 1.48 ohms

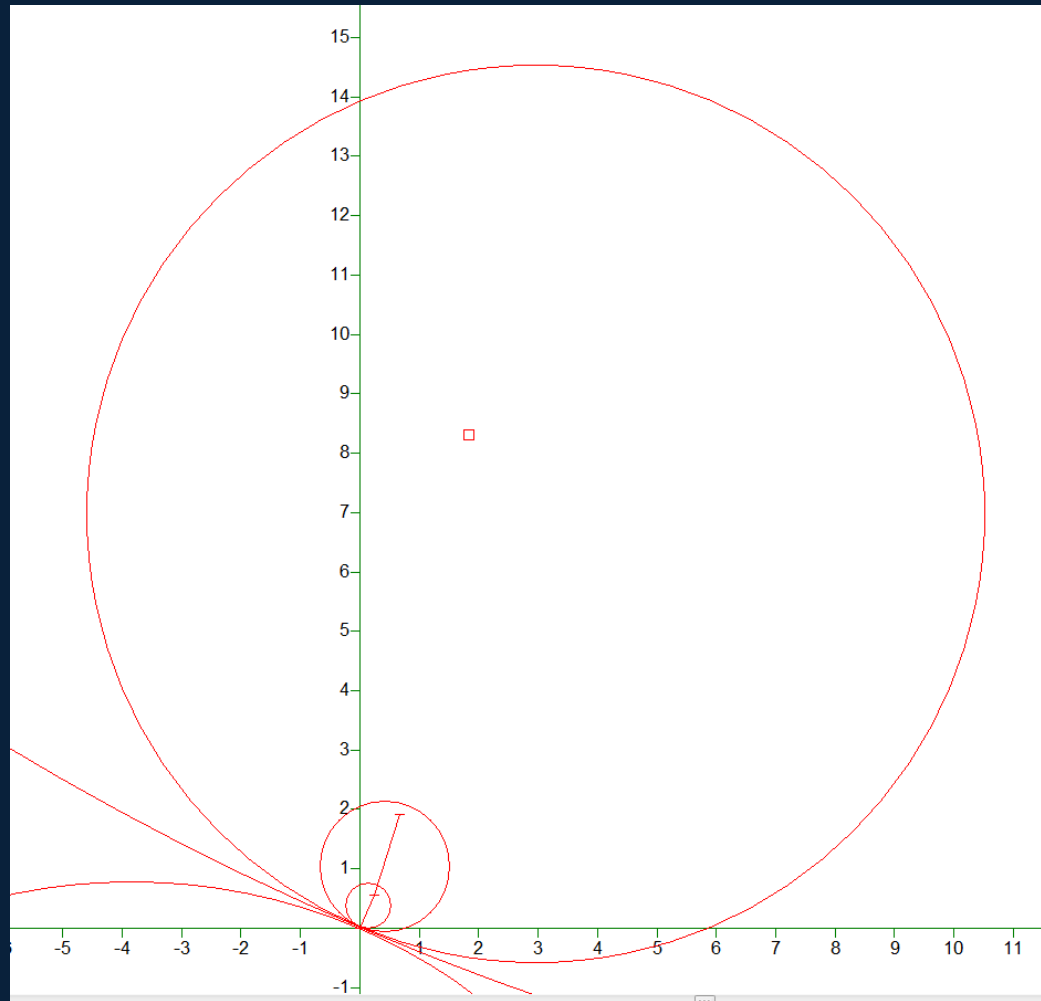


Apparent Impedance Carlyss Closed,  
fault at 100 % of the line: 5.68 ohms



# 421-Zone 2 Settings

Zone 2 Settings Lone Star set at 10.1 ohms from Zapp



# 421-Zone 3 FWD Settings

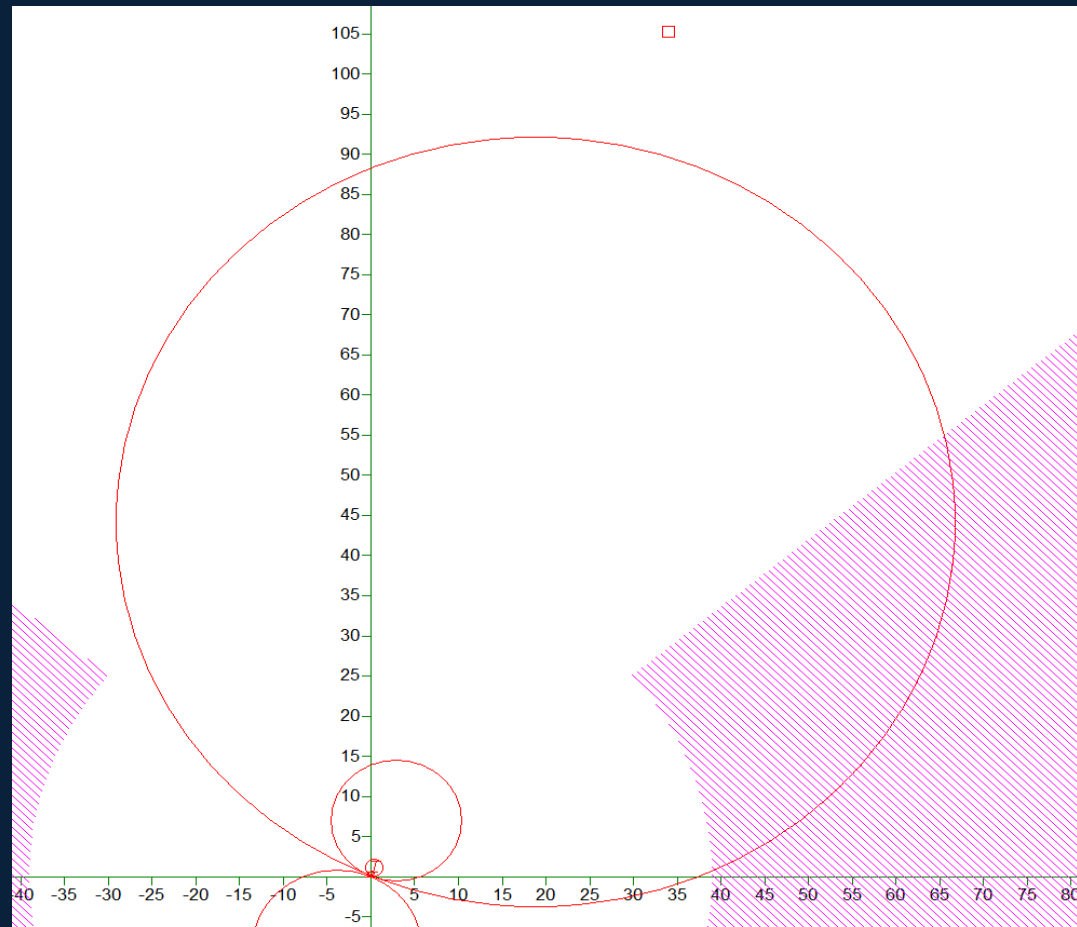
Set Zone 3 Forward to see a fault to the end of the second longest line with line end open

## Lone Star- Zone 1 Settings:

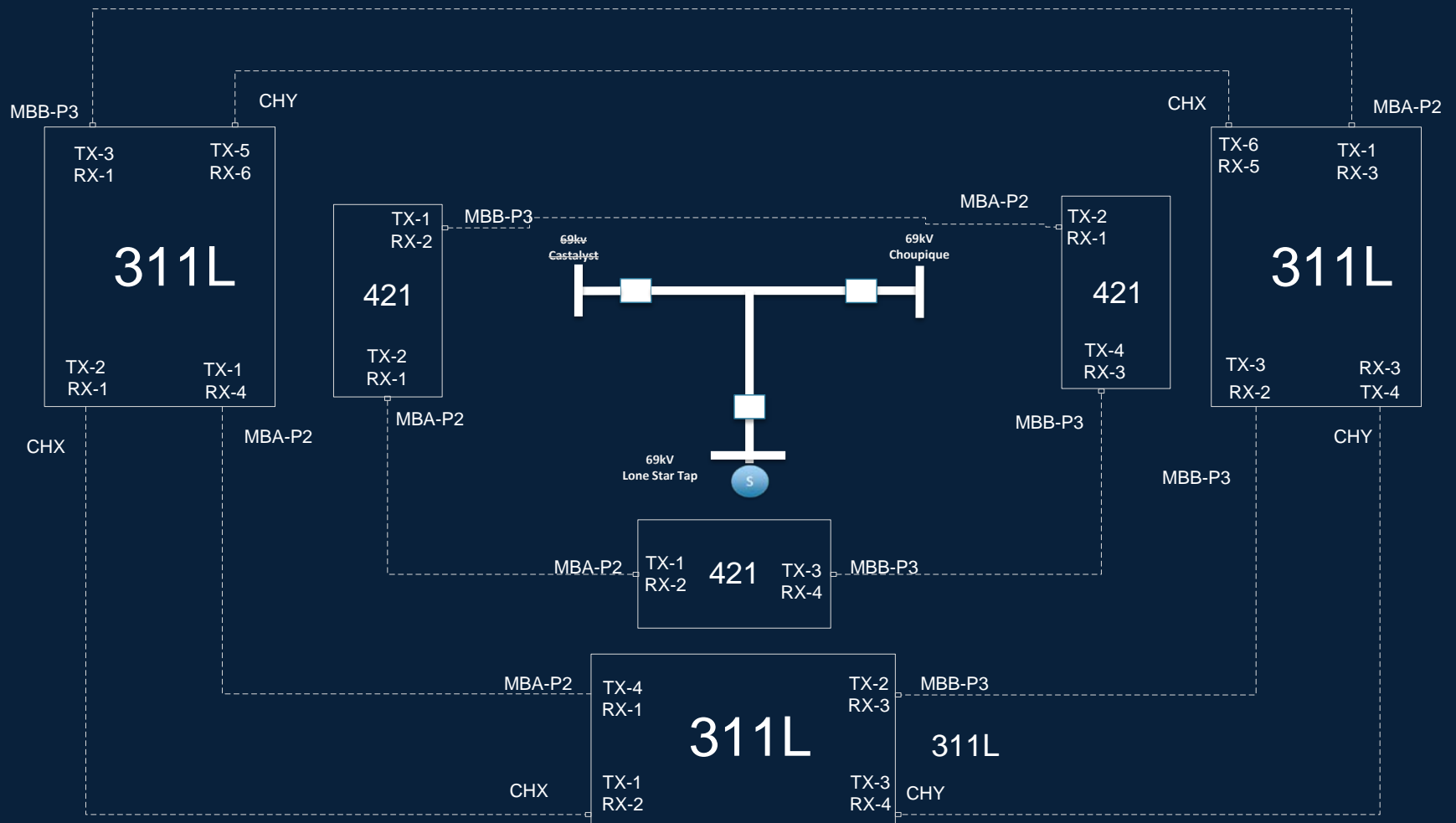
Lone Star-Choupique							
Line Length	=	2.70	mile	0.06313	+J	0.15293	(Pos)
				(Longest 2nd line)			
0.01410	+J	0.04011	(Pos)				
				Choup-Intracostal			
				(from infeed sheet)			
				0.13778	+J	0.49056	(Zero)
0.03395	+J	0.13064	(Zero)	0.00652	+J	0.03750	(Pos)
Lone Star-Catalyst							
				(Shortest 2nd line)			
Line Length	=	1.46	mile				
				Catalyst-Carlyss			
0.00938	+J	0.02198	(Pos)				
				(Zone 2 Bus)			
				0.02289	+J	0.10151	(Zero)
0.02015	+J	0.07111	(Zero)				

# 421-Zone 3 FWD Settings

- Zone 3 Settings Lone Star set at max 64 ohms
- Sequential tripping

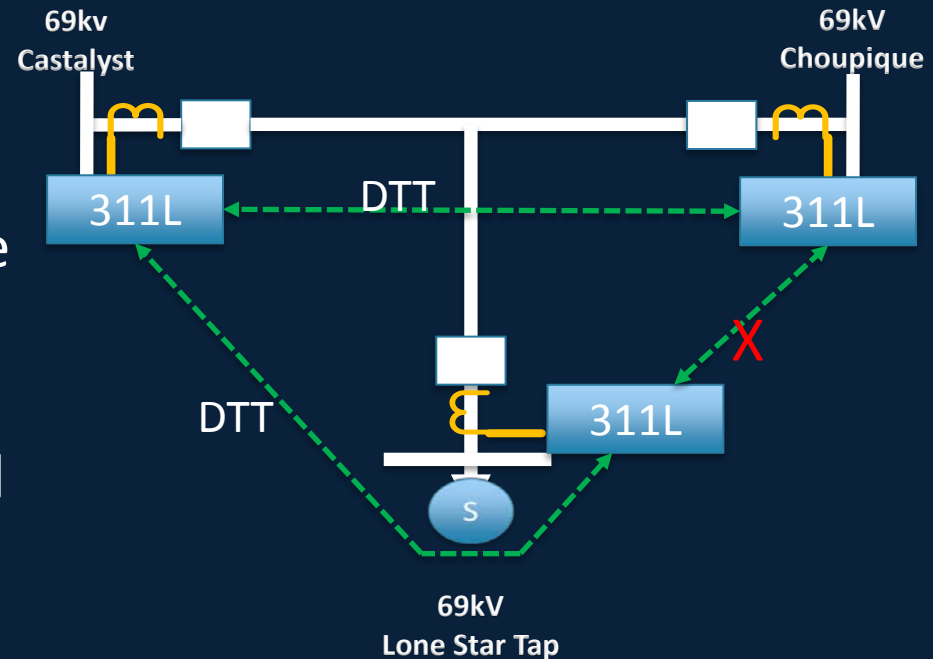


# Communications

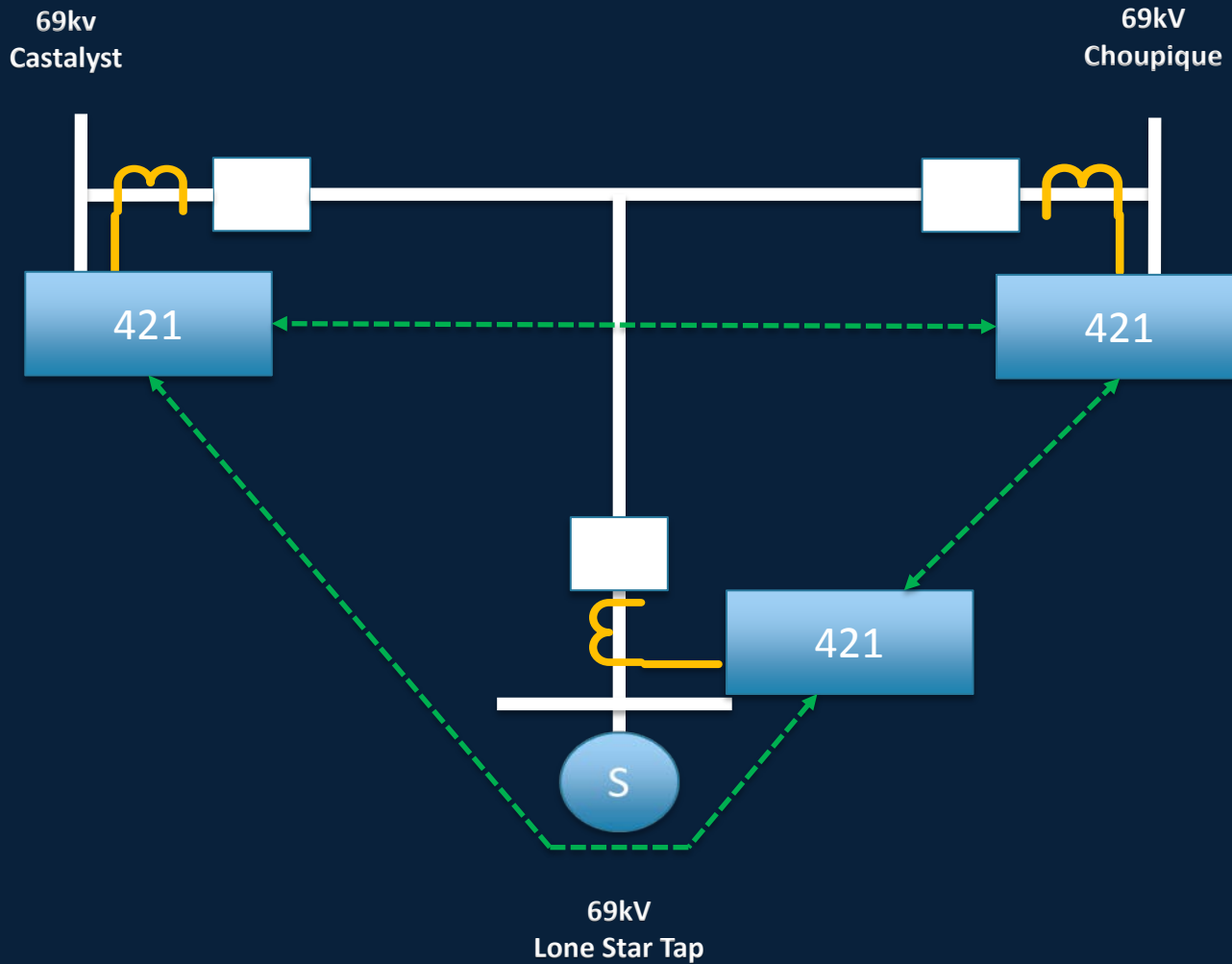


# Communications

- 311L combines two terminal line currents into single current.
- SEL 311L applies two terminal line algorithms to three terminal line applications.
- Loss of communication channel relay with two healthy channels protection still maintained.
- In addition, scheme changed into a DTT.



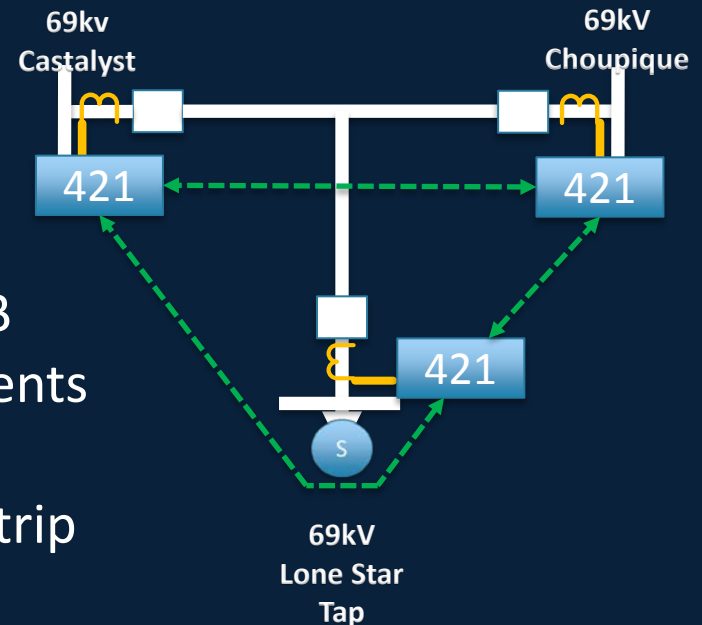
# Communications



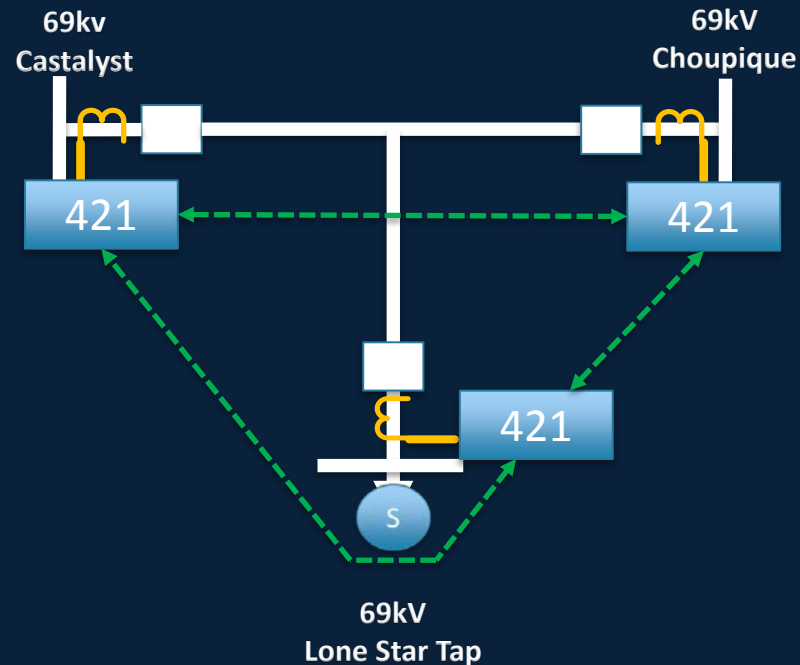


# Communications

- DUTT scheme for Zone 1 elements
  - Trips all terminals via MBA and MBB
- POTT scheme for all overreaching elements
  - PT sent via MBA and MBB
- Terminal must receive a PT to initiate a trip
- In case of communication loss, MBs are passed through each communication channel to reach second remote bus.
- Echo logic enabled



# Questions



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